

Temporal evolution of age data under transient pumping conditions

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Sarah Leray, Jean-Raynald de Dreuzy, Luc Aquilina, Virginie Vergnaud-Ayraud, Thierry Labasque, et al.. Temporal evolution of age data under transient pumping conditions. Journal of Hydrology, 2014, 511, pp.555-566. 10.1016/j.jhydrol.2014.01.064 . insu-00952724

HAL Id: insu-00952724 https://insu.hal.science/insu-00952724

Submitted on 28 Feb 2014 $\,$

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12	Key words: groundwater age, residence time distribution, environmental tracers,

13 chlorofluorocarbons, heterogeneous aquifers, transient flow conditions

14

15 Abstract

While most age data derived from tracers have been analyzed in steady-state flow conditions, we determine their temporal evolution when starting a pumping. Our study is based on a model made up of a shallowly dipping aquifer overlain by a less permeable aquitard characteristic of the crystalline aquifer of Plœmeur (Brittany, France). Under a pseudo transient flow assumption (instantaneous shift between two steady-state flow fields), we solve the transport equation with a backward particle-tracking method and determine the temporal

22 evolution of the concentrations at the pumping well of CFC-11, CFC-12, CFC-113 and SF₆. 23 Apparent ages evolve because of the modifications of the flow pattern and because of the non-24 linear evolution of the tracer atmospheric concentrations. To identify the respective role of 25 these two causes, we propose two successive analyses. We first convolute residence time distributions initially arising at different times at the same sampling time. We secondly 26 27 convolute one residence time distribution at various sampling times. We show that flow pattern modifications control the apparent ages evolution in the first pumping year when the 28 29 residence time distribution is modified from a piston-like distribution to a much broader 30 distribution. In the first pumping year, the apparent age evolution contains transient information that can be used to better constrain hydrogeological systems and slightly 31 compensate for the small number of tracers. Later, the residence time distribution hardly 32 evolves and apparent ages only evolve because of the tracer atmospheric concentrations. In 33 34 this phase, apparent age time-series do not reflect any evolution in the flow pattern.

35 1. Introduction

Groundwater flow is by nature transient, because of the temporal variations of boundary 36 37 conditions such as the variations of recharge over different time scales (seasons, decades, centuries or more) and because of anthropogenic forcings such as pumping or artificial 38 39 recharge. Pumping has a significant impact on the flow pattern and on solute transport. They 40 induce more convergent flow pattern and, even in some cases, some extension of recharge 41 areas (Bredehoeft, 2002; Frind et al., 2005). It will as well speed up flows and modify the 42 relative role of structures, hydrodynamic properties and boundary conditions - increasing for 43 instance the effective recharge rate of unconfined aquifers in close connection to the surface 44 (Leray et al., 2012; Sophocleous, 2005).

Environmental tracers have been widely used for water sources identification, estimation of residence time distribution and model calibration amongst others (Castro et al., 1998; Cook et al., 2005; Long and Putnam, 2009; McMahon et al., 2010; Stichler et al., 2008). Because they integrate velocities along flow paths, they reflect flow conditions over various time scales in the past. They are sensitive to transient phenomena affecting the flow field. More precisely, they are sensitive to transient phenomena occurring over time scales comparable to their characteristic time (Zuber et al., 2011).

Yet, the influence of transient flow conditions on environmental tracer concentration has 52 53 hardly been addressed. Sanford et al. (2004) have reconstructed transient recharge rates using ¹⁴C data in the regional alluvial middle Rio Grande Basin. Schwartz et al. (2010) have noticed 54 that the interpretation of ¹⁴C age in transient flow models can be ambiguous in terms of flow 55 pattern as data distributed over the aquifer reflect different flow conditions. Long and Putnam 56 (2009) have incorporated CFCs and ³H data from a karstic system in binary mixing model 57 with dilution allowing parameters to vary with time. Fewer studies have analyzed the role of 58 transient flow conditions on residence time distribution. Using numerical simulations, 59 Troldborg et al. (2008) have showed the effect of recharge seasonality on residence time 60 distribution and have noticed distinct behaviors. In the shallowest part of the studied 61 heterogeneous aquifer, residence times tend to be smaller than in steady-state flow conditions 62 while they tend to be higher in the deepest part of the aquifer. The effect in a fully-penetrating 63 64 well is however negligible. Zinn and Konikow (2007) have analyzed the effect of the start of pumping on a synthetic configuration composed of an aquifer overlain by an aquitard. Their 65 study have revealed important changes of the mean residence time at the pumping well and of 66 the residence time distribution over long periods of time. Changes only come from the 67

modification of the flow pattern as they solely focused on the mean residence time and not onthe apparent ages obtained from tracers.

In this study, we determine the influence of the transient groundwater flow pattern induced by 70 anthropogenic forcing on environmental tracers concentrations (CFC-11, CFC-12, CFC-113) 71 and SF₆) interpreted in apparent ages. We consider that the transient flow pattern is induced 72 73 by the instantaneous start of a pumping well. Tracer concentrations are reported at the pumping well. Our study is based on the hydrogeological setting of Plœmeur, which is a well 74 documented aquifer where water has been produced for the last two decades for the water 75 76 supply of the nearby city (Le Borgne et al., 2004; Le Borgne et al., 2006; Ruelleu et al., 2010; Touchard, 1999). Although based on a specific site, the results of this study can be 77 generalized to shallowly dipping aquifers overlain by a leaking layer. Such condition has been 78 79 proved to be of importance for groundwater resources in hard-rock aquifers (Leray et al., 80 2013). While our objective is more methodological than targeted to a specific site, the Plœmeur aquifer still offers a complex and yet realistic hydrodynamic context. We use 81 hydrogeological models previously calibrated in steady-state flow conditions under pumping 82 (Leray et al., 2012) and determine the effect of transient flow conditions on apparent ages. We 83 84 first aim at determining the causes of the temporal evolution of the apparent ages and specifically when they rather come from the transient modifications of the flow pattern and 85 when they are more linked to the specificities of the tracers, especially their atmospheric 86 87 concentrations. We second aim at assessing the interest of age data time series for models 88 segregation. After recalling in section 2 the hydrogeological, flow and transport models, we 89 present the results in section 3 and discuss them in section 4.

2. Hydrogeological, flow and transport models 90

91 We successively describe the hydrogeological models of the Plœmeur site that will be used as a basis of this study, the flow and the transport models as well as the numerical methods used. 92 We finally comment in details the derivation of the tracer concentrations and the 93 94 corresponding apparent ages to highlight the possible causes of apparent age temporal S 95 variations.

Hydrogeological model 96 2.1.

97 The study of the effects of transient flow conditions, induced by pumping, on age data is 98 based on the Plœmeur aquifer, a highly heterogeneous hard-rock aquifer located on the south coast of Brittany near the city of Lorient (France). A previous study based on the inversion of 99 gravimetric data has established a geological conceptual model (Ruelleu et al., 2010). This 100 conceptual model is composed of two transmissive structures at large scale, the dipping 101 contact zone and a North 20° normal fault, besides the Plœmeur and Guidel granites and 102 overlying micaschists acting as a typical aquitard. Local heterogeneities are not represented in 103 104 the model. The supplying area to the pumping well which amounts to a few square kilometers 105 is limited in the North-South direction by these two granites. The pumping rate thus has a strong impact on flow pattern within this heterogeneous aquifer. 106

107 Because the shape and the dip of the contact zone are only partially known, the overall 108 thickness of the aquitard-aquifer system remains relatively uncertain. To account for this 109 uncertainty, a few structural models with distinct thickness have been built (Figure 1 and Table 1). The hydraulic properties of the different rocks have been set either to common 110 values as for the granites which are found almost impervious (10^{-11} m/s) , or to measured 111 values as for the micaschists $(10^{-7} \text{ m/s} - 5 \text{x} 10^{-6} \text{ m/s})$ and the contact zone $(1.9 \text{x} 10^{-3} \text{ m}^2/\text{s} - 10^{-6} \text{ m/s})$ 112

 $3 \times 10^{-3} \text{ m}^2/\text{s}$). In addition, the potential recharge rate R has been estimated at 200 mm per year 113 114 (Carn, 1990; Leray et al., 2012; Touchard, 1999). Following these constraints, each model has 115 been calibrated against the mean piezometric level measured at the pumping well (-5.5 masl) 116 in steady-state flow under pumping conditions (Leray et al., 2012) by slightly adjusting the 117 contact zone transmissivity previously estimated from long-term pumping tests (Le Borgne et al., 2006). Uniform porosity has also been calibrated against the CFC-12 age (30 years ± 1 118 year in 2009). Note that the overall volume of the system is about 1.5×10^9 m³ and the mean 119 120 residence time of the model -i.e. the first moment of the residence time distribution -is121 around 13 years in ambient conditions and 50 years in pumping conditions.

Our study has been carried out on about ten representative hydrogeological models differing by their structure, their micaschists permeability and their porosity. The interest of considering different models is to investigate the potential influence of the hydrogeological structure on the apparent ages and their evolution. We discuss further in section 4 how this sensitivity might be useful as an additional way to characterize the flow pattern. Among this set of models, only two are used here to illustrate the methodology as they all lead to the same conclusions. Table 1 synthesizes the parameters of the two chosen hydrogeological models.

129 2.2. Flow model

130 Transient flow conditions are induced by starting a pumping well. The transient pumping rate 131 $Q_w(t)$ is a step function going from zero before the starting date t_{switch} , to a positive value Q_p :

$$Q_w(t) = \begin{cases} 0 & t \le t_{switch} \\ Q_p & t > t_{switch} \end{cases}$$
(1)

6

In the particular case of the site of Plœmeur, Q_p is set at 3.36×10^{-2} m³/s. Pumping started in 132 133 1991 and the most part of the evolution of the piezometric levels occurred only in a few years 134 after the start of pumping. t_{switch} has thus been set at 1994. We solve the 3D diffusivity 135 equation for the hydraulic head $h(\mathbf{x}, t)$ with free surface boundary conditions under a pseudo transient flow approximation: 136

$$\nabla . \left(K(\mathbf{x}) \nabla h(\mathbf{x}, t) \right) = 0$$

$$\nabla . (K(\mathbf{x})\nabla h(\mathbf{x},t)) = 0$$

$$K(\mathbf{x})\nabla h(\mathbf{x},t) \cdot \mathbf{n} = -R \quad \& \quad h(\mathbf{x},t) = z(\mathbf{x}) \quad \text{where } h < z_{\text{ground}}$$

$$h = z_{\text{ground}} \quad \text{anywhere else} \quad \} \quad \text{on } \Gamma_{\mathfrak{s}}(3)$$

$$\nabla h(\mathbf{x}) \cdot \mathbf{n} = 0$$
 on Γ_{west} and Γ_{east} (4)

$$h(\mathbf{x}) = z_{\text{ground}} - z_0 \text{ on } \Gamma_{\text{north}} \text{ and } \Gamma_{\text{south}}$$
 (5)

$$\int_{\Gamma_{W}} K(\boldsymbol{x}) \nabla h(\boldsymbol{x}, t) \cdot \boldsymbol{n}_{\boldsymbol{w}} \, d\Gamma_{\boldsymbol{w}} = Q_{W}(t) \quad \text{sink term}$$
(6)

where K(x) is the hydraulic conductivity; *n* is the outgoing normal to the saturated domain; *R* 137 is the potential recharge rate; z_{ground} is the ground surface elevation; Γ_{s} is the top of the 138 139 saturated domain; Γ_{west} , Γ_{east} , Γ_{north} and Γ_{south} are respectively the West, East, North and South 140 sides of the domain; z_0 is a reference height; n_w is the ingoing normal to the well screen; Γ_w is 141 the well screen surface and $Q_{w}(t)$ is the transient pumping rate defined in equation 1 and 142 located at x_{w} . The pseudo transient approximation intervenes in equation 6 and consists in 143 assuming that steady-state flow conditions are quickly established compared to the solute 7

transport evolution. This is a reasonable approximation of transient flow conditions valid at low specific storage and with the advantage of being less costly numerically. Practically, it consists in ignoring the transition between the two steady-state velocity fields under ambient and pumping conditions.

Equation 2 is solved in unconfined conditions since seepage conditions are a priori not 148 149 known. Unconfined conditions are satisfied through both conditions at the free surface 150 boundary of equation 3. When the free surface level is below the ground surface level, the 151 effective recharge rate is equal to the potential recharge rate R; anywhere else, the free surface 152 level is set at z_{ground} and the effective recharge rate continuously evolves from negative values 153 in the discharge zone to positive potential recharge rate R. The model has been built to 154 include the nearest watersheds both in ambient and pumping conditions in order to minimize the potential effects of the boundary conditions. No-flow conditions applied on the West and 155 156 East boundaries (Equation 4, Figure 2) do not have any impact on the recharge areas captured 157 by the pumping zone located at depth in the pumping well. Imposed heads, set at depth z_0 (5) meters below the ground surface level), are applied to the South and the North boundaries 158 159 without any significant influence on the system because of the almost impervious granites 160 (Equation 5, Figure 2).

161 2.3. Transport model

Transport is considered only advective as the macro-scale dispersion from local dispersion
and diffusion is assumed to have a much smaller effect compared to the macro-scale
dispersion induced by structural heterogeneity and sampling (LaBolle and Fogg, 2001).
Transport is modeled by the advection equation (Bear, 1991; de Marsily, 1986):

$$\frac{\partial C(\mathbf{x},t)}{\partial t} + \nabla \cdot \left(\frac{q(\mathbf{x},t)}{\theta}C(\mathbf{x},t)\right) + \frac{Q_{W}(t)C_{W}(t)}{\theta} = 0 \qquad (7)$$

$$C(\mathbf{x},t=0) = C_{0}(\mathbf{x}) \qquad (8)$$

$$C(\mathbf{x},t) = C_{1}(t) \quad \text{on } \Gamma_{1} \qquad (9)$$

with $C(\mathbf{x},t)$ the solute concentration at the position \mathbf{x} and at the time t; θ the effective porosity; $Q_{w}(t)$ the rate of the pumping well; $C_{w}(t)$ the solute concentration at the pumping well; $C_{0}(\mathbf{x})$ the initial condition; $C_{1}(t)$ is the boundary condition on a first-type boundary (Γ_{1}) - such as the tracer atmospheric concentration at the free surface boundary - and $q(\mathbf{x},t)$ the pseudo transient Darcy's flux derived from the head field $h(\mathbf{x},t)$:

$$\boldsymbol{q}(\boldsymbol{x},t) = -K(\boldsymbol{x})\nabla h(\boldsymbol{x},t). \tag{10}$$

171 2.4. Numerical methods

The unconfined flow equations are solved using a computationally effective finite-volume 172 approach with a local adaptation scheme (Bresciani et al., 2011). The advection equation is 173 174 solved in backward-time that consists in reversing the flow field and adapting the boundary 175 conditions (Neupauer and Wilson, 1999; Neupauer and Wilson, 2001; Neupauer and Wilson, 176 2002). To solve the transport equation, we use a Lagrangian random walk method well-suited to purely advective transport (de Dreuzy et al., 2007; Kinzelbach, 1988) and adapted to the 177 178 unconfined conditions and to the backward-time resolution. We inject particles proportionally 179 to flow (Kreft and Zuber, 1978) at the pumping well cell and tracked them to the aquifer free

surface. The chosen number of injected particles (5×10^6) is determined through a convergence test of the mean and the variance of the residence time distribution. Flow and transport simulations are carried out using the H2OLAB platform (Bresciani et al., 2011; Erhel et al., 2008; Erhel et al., 2009).

184 2.5. Computation and temporal evolution of apparent age

We derive the residence time distribution p(t) from the equally likely residence times given by the particles. The mean concentration C_w of a tracer at the pumping well and at the sampling date t_w is determined by the convolution of the residence time distribution p(t) with the atmospheric concentration $C_{in}(t_w - t)$ of the tracer (Kreft and Zuber, 1978; Maloszewski and Zuber, 1982):

$$C_{\rm w} = \int_0^{+\infty} C_{\rm in}(t_{\rm w} - t)p(t)dt = \int_{-\infty}^{t_{\rm w}} C_{\rm in}(t)p(t_{\rm w} - t)dt.$$
(11)

Note that, to highlight that the residence time distribution p(t) is highly dependent on a given sampling date t_w , we later use it as $p(t_w - t)$ where $t_w - t$ represents the date at which water recharged, rather than as a function of the residence time "t" alone. Throughout the paper, $p(t_w - t)$ is named recharge date distribution. The apparent age A (Nir, 1964) of a tracer at the pumping well x_w and at the sampling date t_w is then obtained from the difference between t_w and the date at which the concentration C_w is equal to the atmospheric concentration:

$$A(t_w) = t_w - C_{\rm in}^{-1}(C_w) = t_w - C_{\rm in}^{-1} \left(\int_{-\infty}^{t_w} C_{\rm in}(t) p(t_w - t) dt \right), \tag{12}$$

196 with C_{in}^{-1} the reciprocal function of the atmospheric concentration.

Equation 12 shows the two possible causes of the variation of age *A* with the sampling date t_w . The first cause is the evolution of the recharge date distribution $p(t_w - t)$ because of the modification of flow conditions that can be traced back to equation 1 through equations 2-11. The shift from ambient to pumping conditions does not only change the flow magnitude but also the flow pattern, the recharge and discharge locations as well as the water mixing within the radius of action of the well (Bredehoeft, 2002). This first cause is solely linked to the flow conditions and does not depend on the tracer characteristics.

The second cause of the age variation directly comes from the tracer atmospheric 204 concentration $C_{in}(t)$ through the convolution of equation 11. The non-linear temporal 205 206 evolution of $C_{in}(t)$ modifies the sampling of the recharge date distribution $p(t_w - t)$. Monotonic 207 and steep evolutions of $C_{in}(t)$ characteristic of the SF₆ and CFCs approximately between the 208 1970s and 1990s results in a large range of weights of the residence times in this period. 209 Flatter evolutions characteristic of the CFCs after the early 1990s give a higher but more equilibrated contribution of the shorter residence times. Depending on the sampling date t_{w} , 210 211 this equilibrated contribution is more or less significant. This effect occurs both in transient 212 and steady-state flow conditions (Troldborg et al., 2008; Waugh et al., 2003; Zhang, 2004). 213 Even under steady-state flow conditions, the non-linear evolution of the atmospheric 214 concentration $C_{in}(t)$ lets the sampled concentration evolve. Under simpler terms, the evolution 215 of the sampled concentration does not only come from the evolution of the system but also 216 from the modification of the "observation device" (C_{in}).

It should be noted that this second effect is irrelevant when mixing is minimal like within the framework of the piston-flow model. In such cases, the residence time distribution resumes to a Dirac and the dependency to the tracer atmospheric concentration vanishes in equation 12 because of the direct transformation of $C_{\rm in}$ by $C_{\rm in}^{-1}$. This effect is, however, very relevant

close to the aquifer discharge zones (springs, wells) where the mixing of flow paths is maximal. The mixing of sampled flow lines enhances the importance of the non-linear evolution of $C_{in}(t)$. The case studied here pertains more to this second situation, in which, finally, both the temporal evolutions of the recharge date distributions $p(t_w - t)$ and the tracer atmospheric concentration $C_{in}(t)$ can modify the sampled concentration and the derived age $A(t_w)$ (equation 12).

To analyze the temporal evolution of the apparent ages, we have determined them using equation 12 by convoluting the recharge date distributions $p(t_w - t)$ obtained under the pseudo transient conditions with the CFC-11, CFC-12, CFC-113 and SF₆ atmospheric concentrations at the evolving sampling dates t_w^i from 1994 to 2009 (Table 2). These dates correspond to sampling 0 to 15 years after the change of flow conditions from ambient to pumping conditions occurring at $t_{switch} = 1994$.

233 **3.** Results

This section first reports the temporal evolution of the apparent ages at the pumping well for the hydrogeological model numbered 1 of the site of Plœmeur described in section 1 and in Table 1. It then analyses the respective effects of the modification of the flow pattern and of the evolution of the tracer atmospheric concentration. The implication of the temporal evolution of the apparent ages for models segregation is further discussed in section 4.1 by comparing the results of the models numbered 1 and numbered 2.

240 3.1. Temporal evolution of apparent age

Figure 3 shows the evolution of the apparent ages from CFC-11, CFC-12, CFC-113 and SF₆ concentrations with the sampling date t_w ranging from 1994 (ambient conditions) to 2009 12

243 (Table 2). At first sight, the apparent ages increase first sharply after the start of pumping and 244 then more smoothly whatever the tracer. We indeed expect that the modifications of flow are 245 maximal just after the start of the pumping and later decrease. Though similar, the apparent 246 ages derived from the CFCs and SF_6 still exhibit some differences induced by the tracer atmospheric concentration $C_{in}(t)$. The temporal evolution is minimal for SF₆ because of the 247 almost linear increase of its atmospheric concentration and maximal for the CFC-11 and 248 CFC-12 because of the strong and non-monotonic variations of their atmospheric 249 250 concentration (IAEA, 2006). CFC-11 and CFC-12 display similar variations because of the similar shapes of their atmospheric concentration chronicles. 251

252 The increase of the apparent ages in the models considered here is somehow counterintuitive. Indeed, in the exponential model (Haitjema, 1995), the residence time distribution is 253 254 independent of the pumping rate. Besides, in the piston-flow model, as said in section 2.5, 255 apparent ages remain constant whatever the sampling dates due to minimal mixing. When 256 starting a pumping in those conditions, one would expect an increase of velocity that would 257 directly reduce the residence time and then the apparent ages. In the more complex system modeled here, pumping has a nontrivial effect on the apparent ages. Further insight is given 258 by the analysis of the recharge date distribution $p(t_w - t)$ and its temporal evolution. Figure 4 259 shows the recharge date distribution sampled at three different dates : (a) at $t_w^1 = 1994$ under 260

ambient flow conditions, (b) at
$$t_w^2 = 1994.1$$
 approximately one month after the pumping

started and (c) at $t_w^3 = 1995$ one year after the pumping started. At later dates ($t_w \ge 1995$),

263 distributions stop to evolve. Therefore, only the distribution at $t_w^3 = 1995$ is displayed.

For 1994 $\leq t_{w} \leq$ 1995, the system is strongly transient (Figure 4a and b). The start of 264 265 pumping induces a modification of the recharge date distribution from a narrow piston-like distribution at ambient conditions (t_w^1) (Figure 4a) to a much broader, more exponential-like, 266 267 later (Figure 4c). Intermediary distribution shapes occur in the first pumping year (Figure 4b). 268 The broadening of the distribution comes from the shift of status of the sampling zone. Under 269 ambient flow conditions, it is a standard zone within the aquifer broken through by just a few 270 flow lines. The different tracers then lead to very close ages (Figure 3). Under pumping 271 conditions, it becomes the major discharge zone of the aquifer focusing a dense net of flow 272 lines that initially discharged in much larger areas such as wetlands (Figure 2) and apparent ages from the different tracers spread out. For $t_w \ge 1994.1$, the recharge date distribution 273 274 broadens including both shorter and larger residence times than the ambient distribution. In 275 the case of the Plœmeur site, shorter residence times eventually control the apparent ages. 276 This is also consistent with the increase of the mean effective recharge rate and the induced 277 circulation speed up (from 160 mm/year in ambient conditions to 200mm/year in pumping 278 conditions). As previously noted, the distributions sampled in 1995 and later are almost identical. Thus, for $t_w \ge 1995$, sampled concentrations are likely to be more influenced by 279 the temporal evolution of the tracer atmospheric concentrations $C_{in}(t)$ and less by the 280 281 evolution of the recharge date distribution. 3.2. Effect of the temporal evolution of the recharge date 282 distribution

283

284 *3.2.1. Methodology*

To assess the role of the temporal evolution of the recharge date distribution $(p(t_w - t))$ in equation 12), we filter out the evolution of the tracer atmospheric concentration $(C_{in}(t))$ in equation 12). To this end, we translate the distributions $p_i(t_w^i - t)$ (Table 2) to the same

288 sampling date t_w^t , the exponent "t" standing for translated. The recharge date distributions

289 $p_i(t_w^i - t)$ are shifted along the date axis by a translation of $t_w^t - t_w^i$ without any

290 modification of their shape. The shifted distributions are noted $p_i(t_w^t - t)$:

$$p_{i}(t_{w}^{t}-t) = p_{i}\left(\underbrace{t_{w}^{i}-t}_{recharge time} + \underbrace{t_{w}^{t}-t_{w}^{i}}_{translation}\right).$$
(13)

291 This is illustrated on Figure 5 for the three recharge date distributions of Figure 4 translated 292 to $t_w^t = 2009$. The apparent age determination is modified accordingly:

$$A(t_{w}^{t}) = t_{w}^{t} - C_{in}^{-1} \left(\int_{-\infty}^{t_{w}^{t}} C_{in}(t) p_{i}(t_{w}^{t} - t) dt \right).$$
(14)

Equation 14 replaces equation 12 and filters out most of the effect of the tracer atmospheric concentration $C_{in}(t)$ to highlight that of the evolution of the flow pattern. The apparent ages

are noted $A(t_w^t)$ recalling that they are obtained after the translation of the recharge date distributions.

297 *3.2.2. Results*

298 Figure 6 compares the apparent ages obtained with the various recharge date distributions

- translated to the same sampling date $t_w^6 = 2009$ for the model numbered 1. The apparent ages
- 300 are derived from equation 14 and are noted $A(t_w^6)$. As for the apparent ages from equation 12,
- 301 the apparent ages $A(t_w^t)$ from equation 14 are first almost identical for the four tracers
- because of the piston-like shape of the ambient distribution. Because of the broadening of the
 recharge date distributions after the start of pumping, they diverge from each other to finally
 reach fixed values spreading over almost 15 years (four last points of Figure 6). The apparent
- 305 ages $A(t_w^t)$ from the distribution initially sampled at $t_w^i = 1994.1$ (*i.e.* one month after the
- 306 pumping started) constitute an intermediate case. Indeed, unlike the ages from the ambient 307 distribution, they significantly diverge for the four tracers. However, their spreading is not as 308 broad as for the distributions sampled at later dates ($t_w^i \ge 1995$). We will discuss in section
- 4.1 the interest of these differences for model segregation. We have checked that theconclusions were the same for the other sampling dates of Table 2.

311 3.3. Effect of the temporal evolution of the atmospheric312 concentration

313 *3.3.1. Methodology*

To assess the influence of the tracer atmospheric concentration $C_{in}(t)$ independently of the 314 flow pattern modifications, we compute the apparent ages at six translated sampling dates t_w^t 315 316 (Table 2) for a fixed recharge date distribution. Figure 7 illustrates this analysis for the pseudo transient distribution initially sampled at $t_w^3 = 1995$ and translated to 2004 and 2009. This 317 318 transformation should not be confounded with the previous one in which we studied the influence of the recharge date distributions at fixed atmospheric concentration $C_{in}(t)$. 319 320 3.3.2. Results Figure 8a, b and c display the results for the three distributions of Figure 4a, b and c. For the 321 ambient distribution (initially arising at $t_w^i = t_w^1 = 1994$), the evolution of $A(t_w^t)$ with t_w^t 322 remains very small (Figure 8a) because of the restricted dispersion of the recharge date 323 distribution (blue curve of Figure 4a). It would be strictly equal to zero for a pure piston-flow 324 model. For broader recharge date distributions corresponding to the pseudo transient case 325 sampled at $t_w^i = t_w^3 = 1995$ (Figure 8c), the apparent ages strongly evolve with t_w^t . The 326 weighting of the recharge date distribution progressively evolves with date and yields 327 328 different ages consistently with Figure 3. Similar results have been found for the pseudo transient distributions sampled after t_w^3 (>1995). For the distribution initially sampled one 329

month after the pumping started (at $t_w^i = 1994.1$), the apparent age variation with t_w^t is still

331 significant though less important than the age variation from the posterior distributions.

332 In conclusion, the two previous analyses highlight the respective effects of the recharge date 333 distribution (3.2) and of the tracer atmospheric concentration (3.3). They show two well-334 differentiated regimes of apparent age evolution. The first regime occurs within the first few months after starting the pumping. Note that it is fast in comparison to the mean residence 335 336 time (50 years). The recharge date distribution shifts from a restricted distribution to an 337 extended one with major consequences on apparent ages. Relatively parallel flow lines under ambient conditions become convergent under pumping inducing the broadening of the 338 339 recharge date distribution. By comparison, on these short durations (some months), the 340 evolution of the atmospheric concentration has a negligible effect. The second regime occurs after the first year of pumping and lasts for longer period of times. The recharge date 341 distribution marginally changes without any marked effect on the apparent ages. The 342 dominant source of age variation is the non-linear evolution of the tracer atmospheric 343 344 concentration. This reveals that apparent ages can significantly evolve even if fluid flows and transport are at steady-state. If the second regime is smoother than the first one, it still leads to 345 significant variation of ages (Figure 3). 346

347 4. Discussion

We first discuss the potential interest of the two successive evolutions of apparent ages, *i.e.* a first phase dominated by the transient flow pattern and a second one by the transient atmospheric concentration for flow pattern characterization and models segregation. We secondly compare these modeling results to the available data on the site of Plœmeur.

4.1. Information contained in the temporal evolution of apparent
 ages

354 The temporal evolution of apparent ages contains information on the hydrogeological system, 355 in addition to information contained in the tracer concentrations analyzed at a single time. 356 Yet, information is largely different between the two evolutions identified in sections 3.2 and 3.3. The first evolution is the rapid shift when starting pumping from a restricted recharge 357 358 date distribution to an extended one. The restricted recharge date distribution can be typically fitted by an inverse Gaussian model characterizing mainly the length of the flow paths from 359 the recharge zone divided by the recharge rate (Ginn et al., 2009; Woolfenden and Ginn, 360 361 2009). The broader recharge date distribution characterizes more globally the aquifer volume 362 and the overall recharge rate (Leray et al., 2012), so does typically the exponential model (Haitjema, 1995). Therefore, almost independent and useful pieces of information, such as a 363 characteristic length vs. a volume, can be obtained using the same well before and after the 364 start of pumping. Using equation 12 as an illustration, it comes down to use the temporal 365 366 evolution of apparent ages to estimate the transient controlling parameters of the function 367 $p(t_{\rm w} - t)$.

Figure 9 compares the temporal evolution of the CFC-12 age for the models numbered 1 and 368 369 numbered 2 (Table 1) at sampling dates ranging from 1994 to 2009 (Table 2). It shows that 370 the two models give distinct apparent ages before 1995 *i.e.* when the recharge date distribution is transient. Later, once the recharge date distribution is broad and reaches a 371 372 steady-state, and because the two models have been calibrated on CFC-12 age in 2009, the 373 apparent ages are identical for both models. Differences only occur at short term after the 374 pumping started and result from different transient evolutions of the residence time 375 distribution. This underlines the interest of a continuous sampling of environmental tracer concentrations, particularly at the early times of pumping, to characterize the transient 376 377 behavior of the system. In that case, apparent age time series can be used as an additional tool

to segregate hydrogeological models. Using equation 12 as an illustration, it comes down to use the temporal signal in apparent ages to segregate two functions $p(t_w - t)$ that exhibit distinct transient behaviors.

Comparison to field observations on the site of Plœmeur 4.2. 381 382 Apparent ages obtained from CFC-11, CFC-12, CFC-113 and SF₆ data have been determined 383 on the site of Plœmeur since 2006 and recorded in the Plœmeur site database (Ayraud et al., 384 2008; de Dreuzy et al., 2006). In the pumping well, data are available in 2006 and 2009. CFC-385 12 age increases from 27.5 in 2006 to 30 years in 2009 and CFC-113 age decreases from 28.5 386 to 26.5 years. CFC-11 ages are close to 45 years and remain constant with time. Still, they 387 should be very close to CFC-12 apparent ages because of the similar normalized atmospheric 388 concentrations of the two tracers. As already reported in Leray et al. (2012), degradation of 389 CFC-11 under anaerobic conditions may explain these differences (Cook and Solomon, 1995). SF₆ apparent ages are less than 10 years. Such discrepancies cannot be explained by 390 391 hydrodynamic mixing alone even at the pumping well (Leray et al., 2012) but are rather 392 coming some geogenic production from the neighboring granites (Busenberg and Plummer, 2000; Koh et al., 2007). 393

The results of the models in section 3 suggest that with negligible temporal change of the recharge date distribution, the apparent age should continuously increase whatever the tracer and within the date interval 2000-2010. The CFC-12 age increase at the Plœmeur site is similar in terms of magnitude to that of the models. CFC-12 data thus suggest that the tracer age evolution in that discharge area mainly comes from the temporal evolution of the atmospheric concentration weighting and that the flow pattern and the resulting recharge date distribution in the pumping zone are in turn not expected to vary significantly after 2006.

401 Still, CFC-113 exhibits an opposite age variation in comparison with CFC-12. Considering
402 the age uncertainty due to analytical and sampling errors (Leray et al., 2012), the acquisition
403 of additional concentration data over the next few years would help to confirm the age trends
404 and eventually conclude about the flow pattern stabilization.

Earlier flow conditions, and particularly initial ones *i.e.* just before the pumping started, are 405 406 more difficult to constrain on the site of Plœmeur because of the lack of environmental tracers 407 monitoring before 2006. Contrary to CFCs and SF₆ data, chloride and nitrate concentrations 408 have been monitored on a longer date range starting at 1991. Because of reactivity processes and their evolution with time, the nitrate concentration chronicle can only give partial 409 410 information on the flow pattern and on mixing processes. However, its non-negligible initial 411 concentration (roughly 15 mg/l) before the start of pumping indicates short residence times 412 consistent with the local recharge area and the short flow paths obtained in the models. Chloride has the advantage of being conservative and being characteristic of deeper waters 413 and thus a good indicator of the flow pattern and its evolution. Figure 10 represents the 414 temporal evolution of chloride concentration at the pumping well. It displays a sharp increase 415 416 during the first two years of pumping (1st phase of Figure 10), a very slight increase for the next ten years (2nd phase of Figure 10) and finally stabilizes after 2005 (3rd phase of Figure 417 418 10). The first phase is consistent with the previous modeling result of a quick transition from 419 the piston-like recharge date distribution to the more extended one. The short duration of the 420 first phase is consistent with the fast temporal evolution of the recharge area (Figure 11). 421 Before pumping, the recharge area is a small zone upstream of the well (blue line). It quickly 422 expands to a much larger area around the well only after one year of pumping (green line). 423 Actually, the pumping well collects water that naturally discharged in wetlands next to it and 424 transforms a wide discharge zone to a point-like one.

The 2nd phase corresponds to a slight increase of the chloride concentration (Figure 10). This 425 426 increase does not come from the changes of the recharge area induced by the evolution of the 427 flow pattern, in this case marginal (from orange to purple curves in Figure 11). It more likely comes from the modification of the deep water fraction coming from the main aquifer - *i.e.* 428 429 the contact zone - that dips quasi-vertically at about 1,500m from the pumping well (Figure 11, (Ruelleu et al., 2010)). Its evolution only affects recharge dates earlier than 1940 and 430 cannot consequently be detected by atmospheric gases. Finally, the stabilization of the 431 chloride concentration (3rd phase of Figure 10) agrees with the apparition of a new steady-432 A 433 state regime.

5. Conclusion 434

We have analyzed the temporal evolution of apparent ages in a complex aquifer under 435 pumping based on CFCs and SF₆ concentrations measured at the pumping well. The evolution 436 437 of apparent ages at the pumping well with time can come from (1) the transient nature of flow conditions and (2) the transient evolution of the tracer atmospheric concentrations. To identify 438 the respective role of these two sources, we proposed two successive analyses of the residence 439 440 time distributions: (1) convolution at the same sampling date (*i.e.* with the same atmospheric concentration chronicle) of residence time distributions initially arising at different dates to 441 442 assess the effect of the distributions, (2) convolution of one residence time distribution at 443 various sampling dates (*i.e.* with various atmospheric concentration chronicles) to assess the 444 effect of the atmospheric concentration.

445 We identify two well-differentiated phases in the evolution of apparent ages. Apparent ages first evolve because of the pumping-induced modifications of flows. At this stage, the 446 temporal evolution of apparent ages is distinct between two hydrogeological models and may 447

be advantageously used to segregate them using for instance a classical least square comparison procedure of data with modeling results. The transient measure of the tracer concentrations contain some additional information and slightly compensate for the small number of available tracers. After one year of pumping, residence time distributions hardly evolve and apparent ages become solely modified by the transient evolution of the atmospheric concentrations. Apparent ages still significantly evolve but do not contain any additional information on the flow patterns beyond those contained in the steady-state data.

455 Acknowledgments

CCK

Funding was provided by the French National Research Agency ANR through the H2MNO4 project for the development of parallel simulation methods (ANR-11-MN). Research and monitoring on the site of Plœmeur is funded by the Environmental research Observatory H+ (Network of hydrogeological sites) and by the European Interreg IV project Climawat. J.-R. de Dreuzy acknowledges the European Union for its additional funding through the IEF Marie-Curie fellowship (PIEF-GA-2009-251710). The authors acknowledge Arash Massoudieh and an anonymous reviewer for their fruitful reviews.

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Tables 605

Table 1: Parameters of the two hydrogeological models of the site of Plœmeur used in this 606 607 study with their reference work. H_{TOT} represents the mean thickness of the aquifer system composed of the micaschists and of the contact zone (Figure 1). The two models have been 608 609 calibrated on the piezometric level at the pumping well and on CFC-12 apparent age at the 610 pumping well.

Table 2 : Sampling dates t_{w}^{i} where the apparent ages are determined. 611 n

612

613 Figures

Figure 1: 3D diagram of the hydrogeological conceptual model composed of the contact zone, the North 20° normal fault, the micaschists and the two granites. The North 20° normal fault is underlined by black stripes. The red triangle locates the sampled pumping well. H(x)represents the thickness of the aquifer system composed of the micaschists and the contact zone. Its mean, noted H_{TOT} , is taken as a proxy for the characterization of its structure. As a convention, all positions are given in meters and vertical positions are negative below the sea level and positive above. Adapted from Leray et al. (2012).

Figure 2: Boundary conditions applied to the model *i.e.* no flow on the East and the West boundaries (black lines) and head imposed on the North and South boundaries (red lines). The limits with the impervious granites are represented by black dashed lines. Discharge zones in ambient conditions (green) are partly dried with starting the pumping. Specifically, the wetland in the pumping zone entirely disappears. Figure 3: Apparent ages derived from CFCs and SF₆ concentrations as functions of the sampling date t_w for the model numbered 1 (Table 1).

Figure 4: Recharge date distributions $p(t_w - t)$ of the model numbered 1 (solid curves, left axis) superimposed on CFC-12 atmospheric concentration $C_{in}(t)$ (grey dashed line, right axis). Recharge date distributions are sampled at: a) t_w^1 (1994 – ambient flow, blue curve), b) t_w^2 (1994.1, wine curve), and c) t_w^3 (1995, green curve). Superposition of the curves shows the sampling of the tracer atmospheric concentration performed by the recharge date

633 distributions.

634 Figure 5: CFC-12 atmospheric concentration $C_{in}(t)$ (grey dashes) superimposed on some translated distributions $p_i(t_w^t - t)$ to the sampling date $t_w^t = 2009$ for the model numbered 1 635 636 (Table 1). The translated distributions are the ambient distribution (initially sampled at $t_w^1 = 1994$, blue curve) and two pseudo transient distributions initially sampled at 637 $t_w^2 = 1994.1$ (wine curve) and at $t_w^3 = 1995$ (green curve). Note that the ordinate axis has 638 639 been broken between 0.05 and 0.19 to display the peak of the ambient distribution. Figure 6: Apparent ages derived from CFCs and SF₆ concentrations for the translated 640 recharge date distributions $p_i(t_w^6 - t)$ with *i* from 1 to 6 for the model numbered 1 (Table 2). 641 p_1 corresponds to the blue curve of the Figure 5 (translated ambient distribution), p_2 to the 642 wine curve of the Figure 5 and p_3 to the green curve of the Figure 5. 643 Figure 7: Recharge date distribution p_3 at its initial sampling date $t_w^3 = 1995$ (green solid 644 curve) and translated to $t_w^t = 2004$ (green dash dots) and translated to $t_w^t = 2009$ (green 645 646 short dashes) for the model numbered 1 (left axis) superimposed on the CFC-12 atmospheric concentration $C_{in}(t)$ (grey dashed line, right axis) 647 Figure 8: Apparent ages derived from CFCs and SF₆ concentrations as functions of the 648 649 translated sampling date t_w^t for the model numbered 1. Apparent ages are obtained for (a) the

650 translated ambient distribution $p_1(t_w^t - t)$ (blue curve of Figure 4a), (b) the translated

pseudo transient distribution $p_2(t_w^t - t)$ (wine curve of Figure 4b) and (c) the translated 651 pseudo transient distribution $p_3(t_w^t - t)$ (green curve of Figure 4c). 652 653 Figure 9: CFC-12 ages of the model numbered 2 (blue crosses) as a function of CFC-12 ages 654 of the model numbered 1 (Table 1). CFC-12 ages are computed at the pumping well and at sampling dates between 1994 and 2009 (Table 2). Labels next to the crosses stand for the 655 656 corresponding sampling dates. We recall that the two models have both been calibrated on the CFC-12 age in 2009. Results for the tracers CFC-11, CFC-113 and SF₆ are similar and thus 657 are not shown. 658 Figure 10: Chloride concentration as a function of the sampling date t_w measured at the 659 pumping well of the site of Plœmeur (updated from Ayraud (2005)). The first phase consists 660 in a sharp and fast increase of the chloride concentration, the second phase in a slight increase 661

of the chloride concentration and the third phase in the stabilization of the chlorideconcentration.

Figure 11: Surface origin of the CFCs and SF6 (corresponding to recharge dates posterior to 1940) for the model numbered 1 (Table 1) under pseudo transient conditions sampled at t_w^1

666 (1994 – ambient flow, blue line), at t_w^2 (1994.1, wine line), at t_w^3 (1995, green line), at t_w^4 667 (1999, orange line), at t_w^5 (2004, red line) and at t_w^6 (2009, purple wine).

	Values		References
Common parameters			
Potential recharge rate R (mm/year)		200	(Carn, 1990; Touchard, 1999)
Granites conductivity $K_{\rm G}({\rm m/s})$		10-11	
Specific parameters for selected models			
	Model n°1	Model n°2	
Mean thickness H_{TOT} (m) – structure name	180 - shallow	280 - deep	(Ruelleu et al., 2010)
Micaschists permeability K_{MS} (m/s)	10 ⁻⁶	5x10 ⁻⁶	(Leray et al., 2012)
Contact zone transmissivity T_{CZ} (x10 ⁻³ m ² /s)	2.27	2.2	(Le Borgne et al., 2004; Le Borgne et al., 2006)
North20° fault transmissivity $(x10^{-3} m^2/s)$	1.14	1.1	(Le Borgne et al., 2004; Le Borgne et al., 2006)
Porosity φ (%)	5	2.7	(Leray et al., 2012)

Sampling dates t_w	Acronym	Name and color for corresponding $p(t_w - t)$	
1994	$t_{\rm w}^{-1}$	$p_{1=}p(t_{w}^{1}-t)$, blue	
1994.1	$t_{\rm w}^{2}$	$P_{2=}p(t_{w}^{2}-t)$, wine	
1995	$t_{\rm w}^{3}$	$P_{3=}p(t_{w}^{3}-t)$, green	
1999	$t_{\rm w}^{4}$	$p_{4=}p(t_w^4-t)$, not displayed	
2004	$t_{\rm w}^{5}$	$p_{5} = p (t_w^{5} - t)$, not displayed	
2009	$t_{\rm w}^{6}$	$p_{6} = p (t_w^6 - t)$, not displayed	2

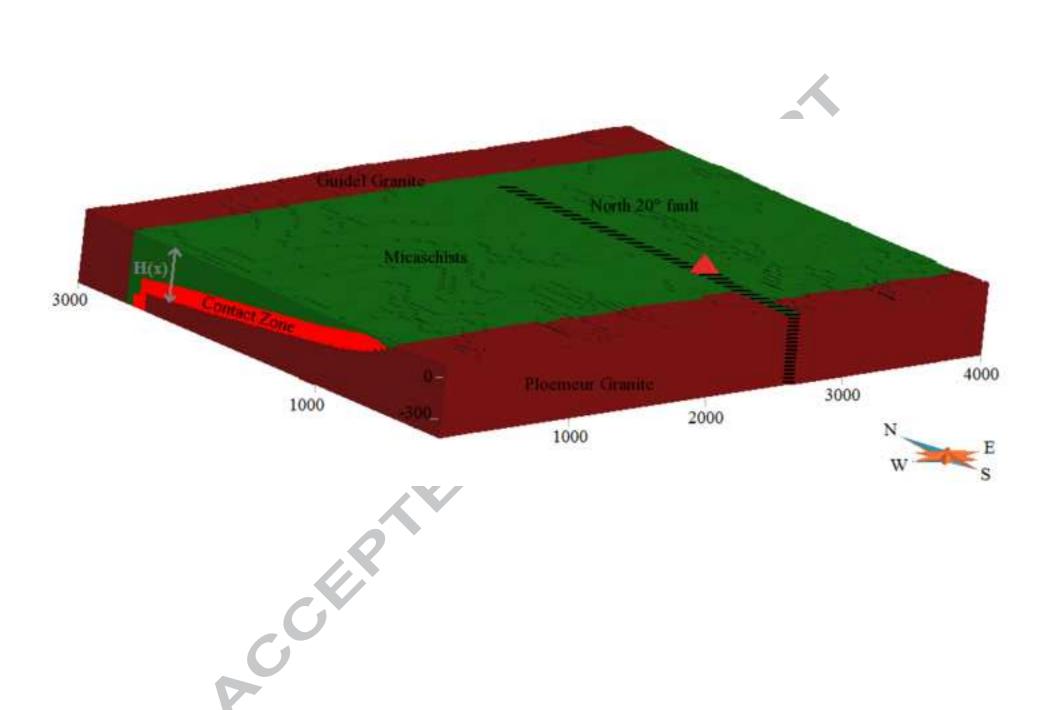
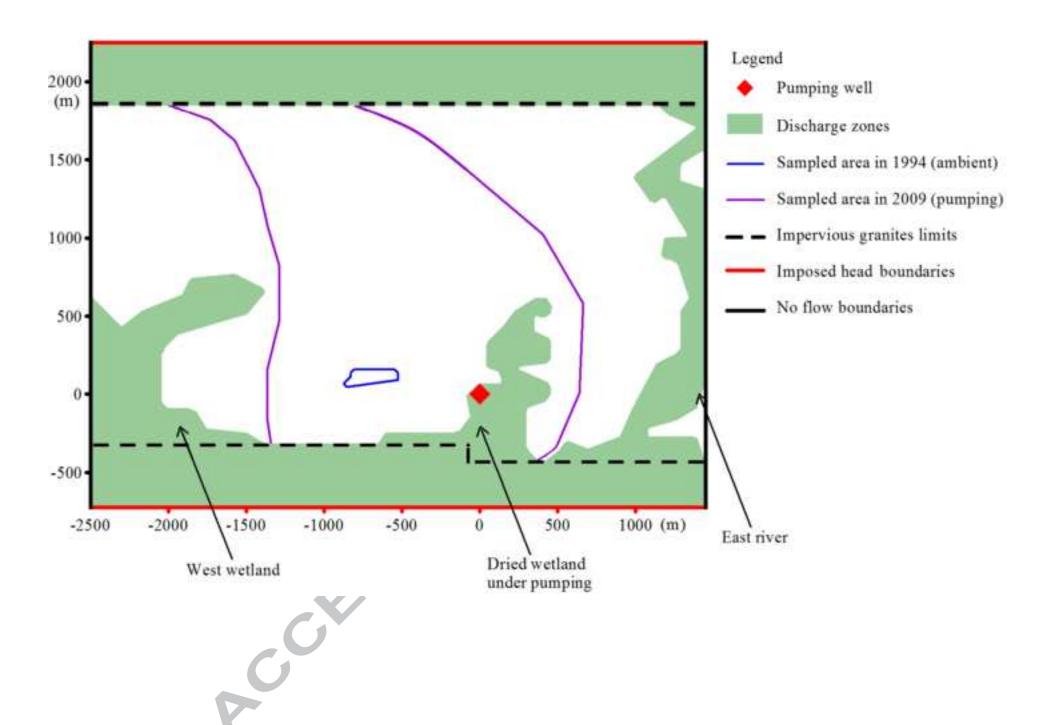
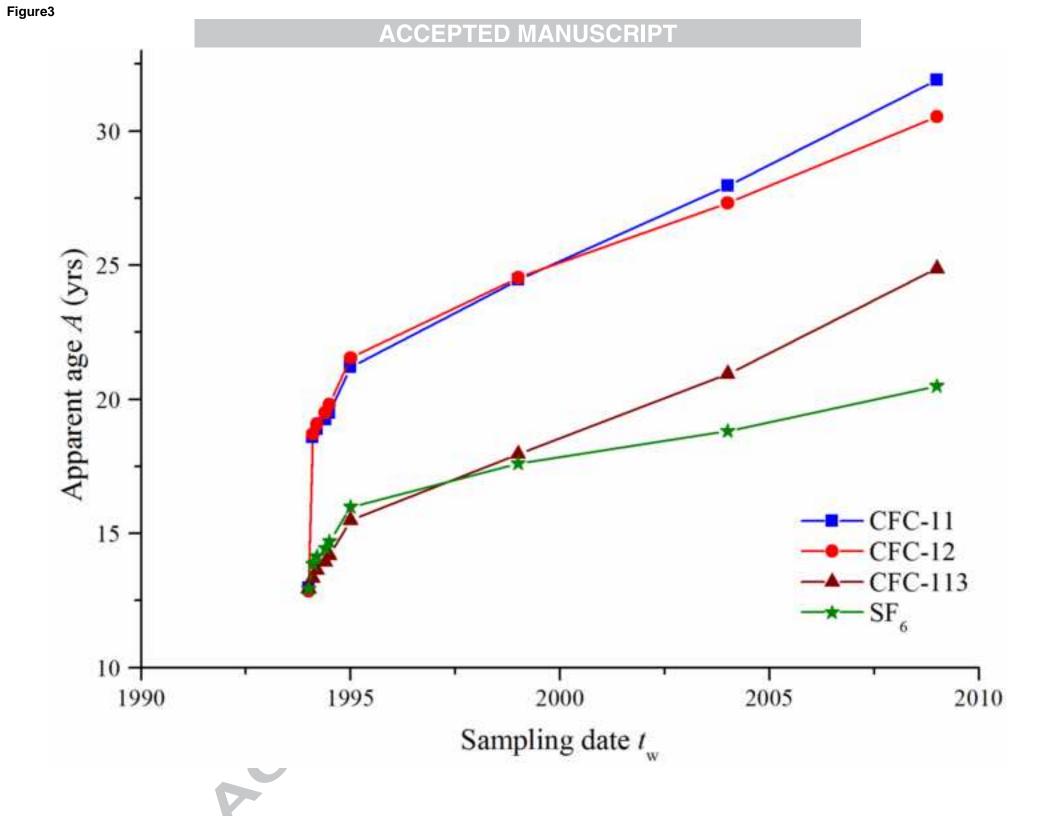
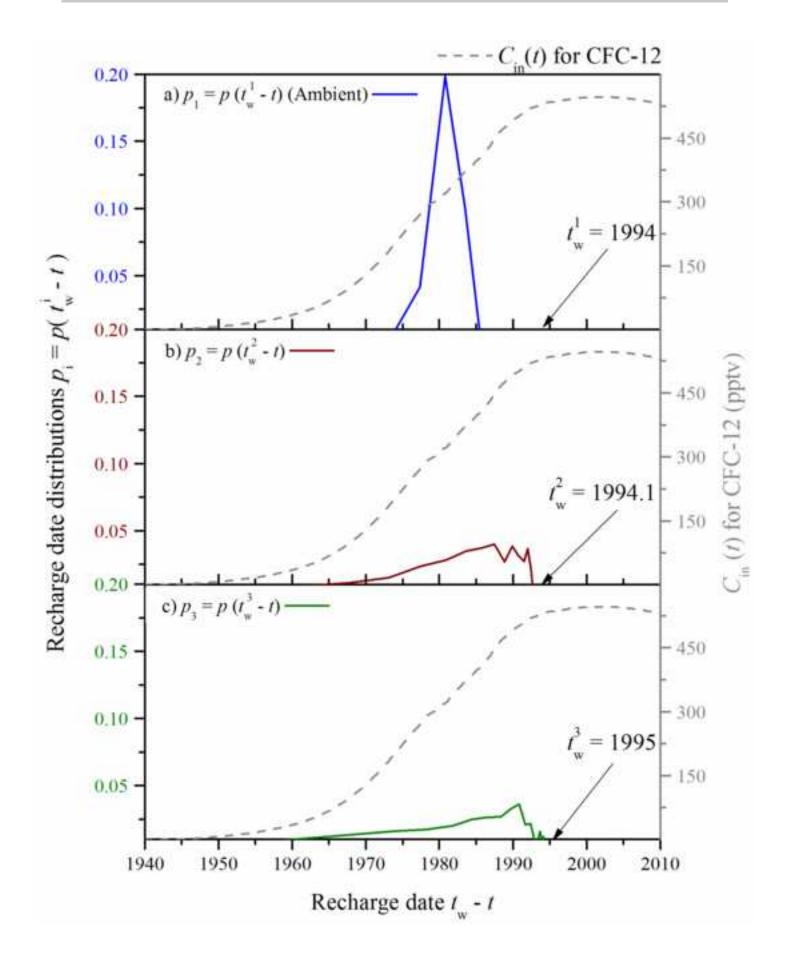
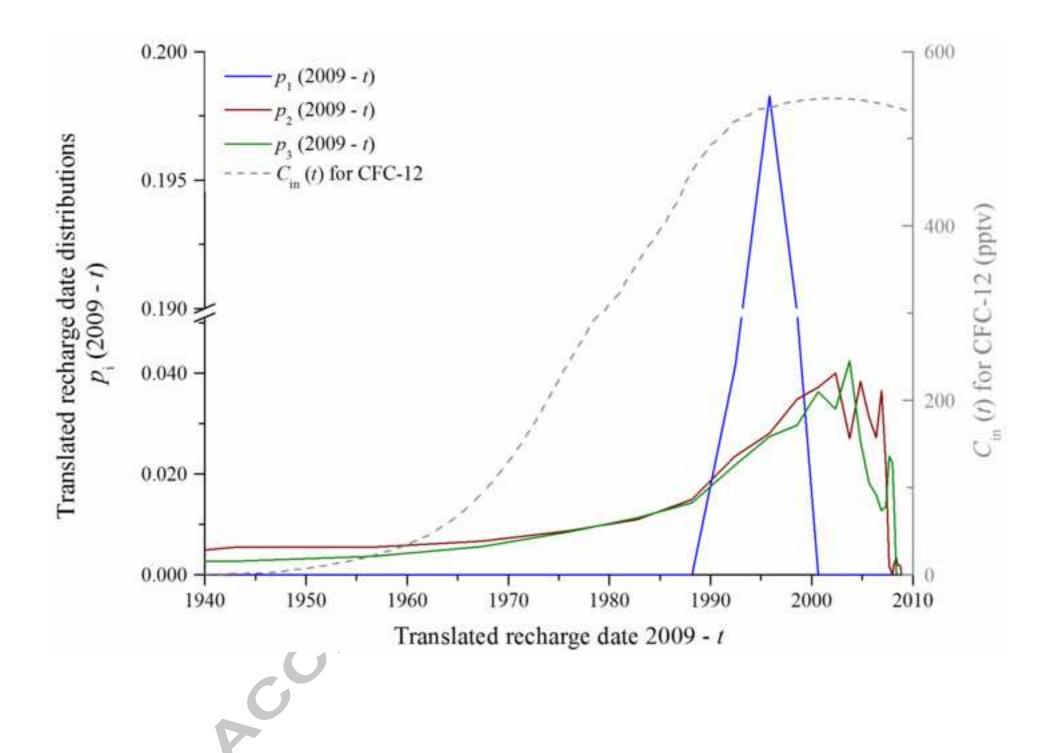


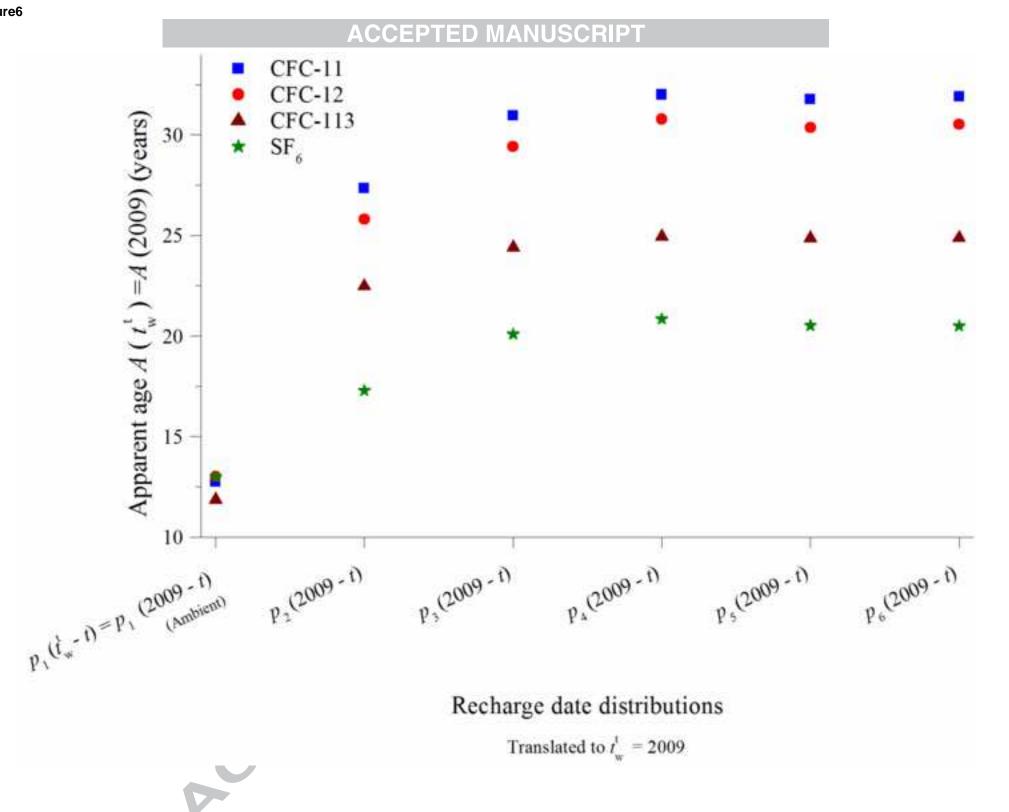
Figure2

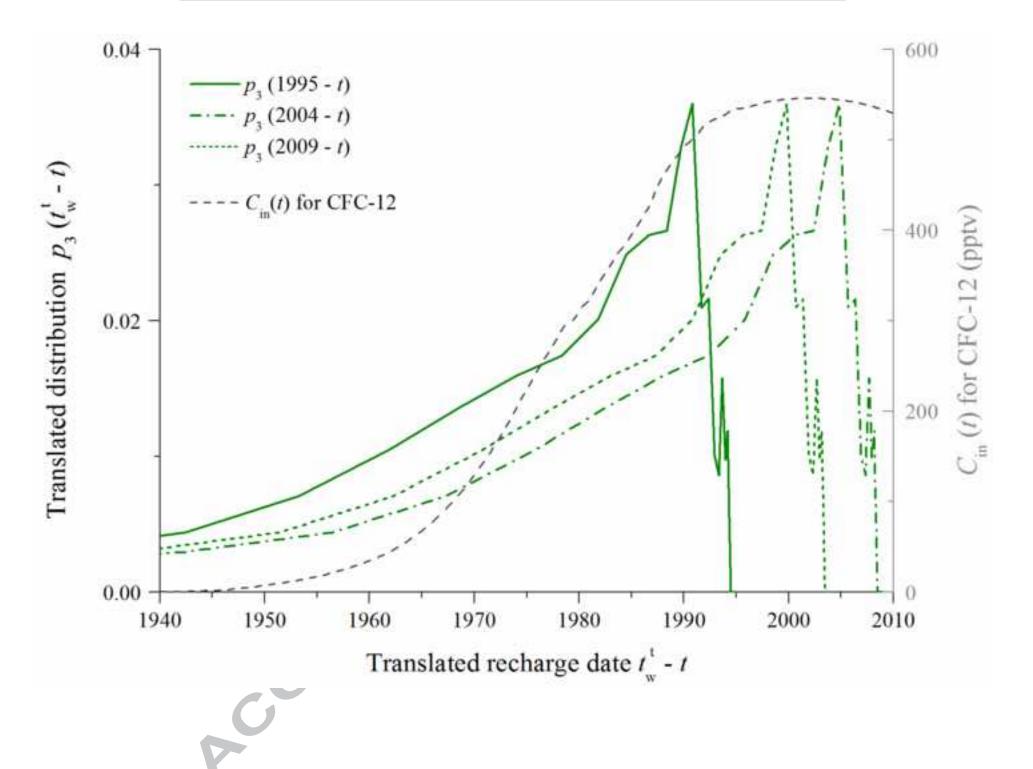












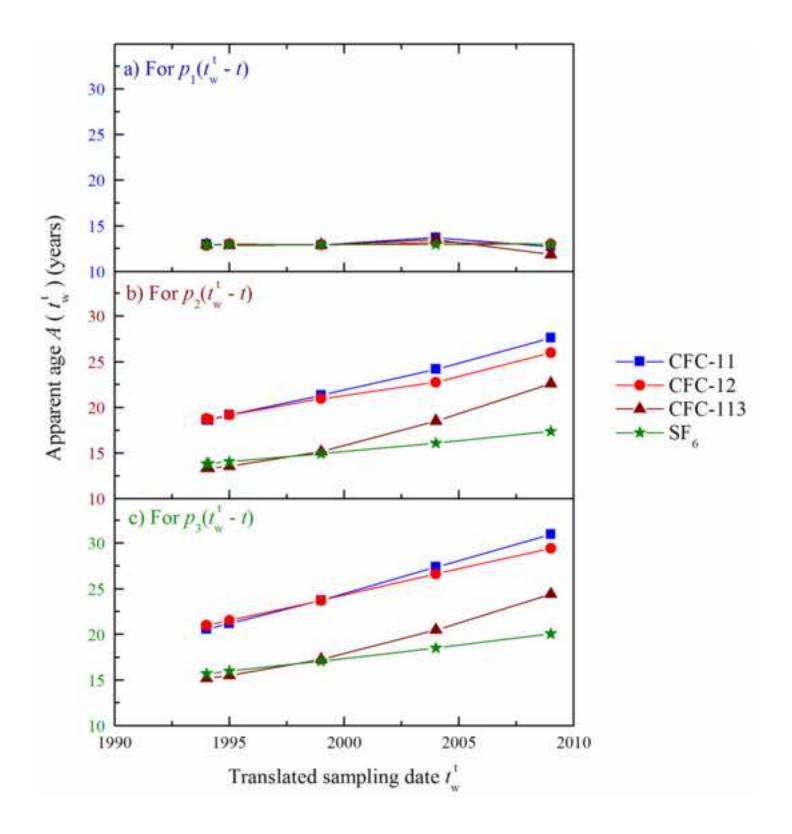
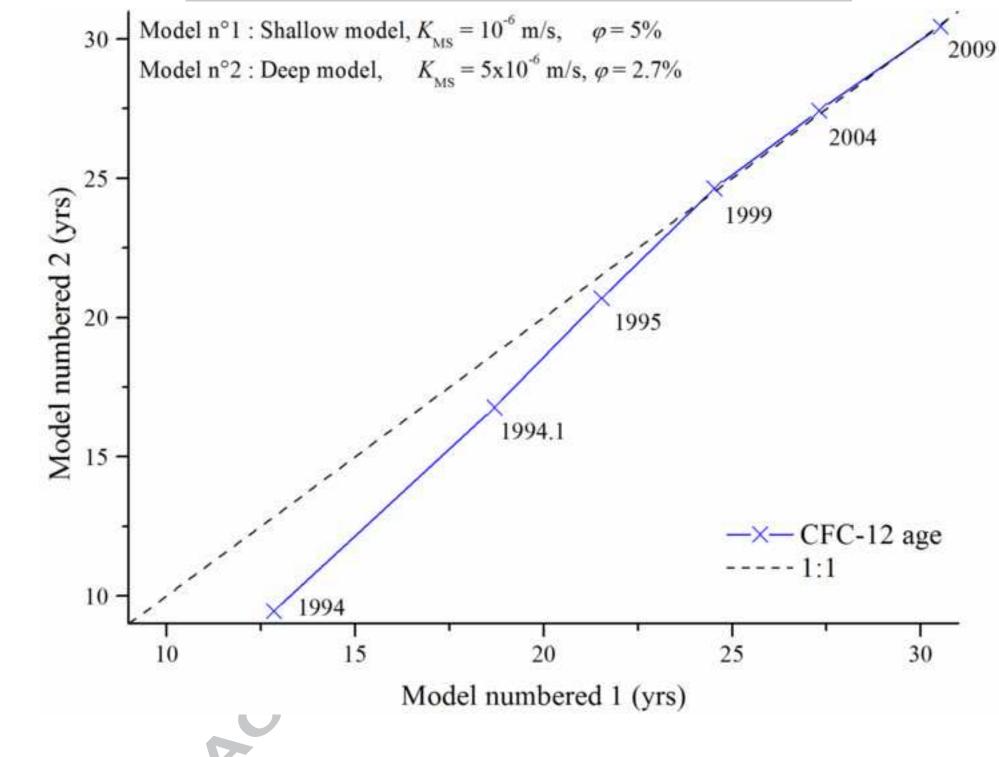
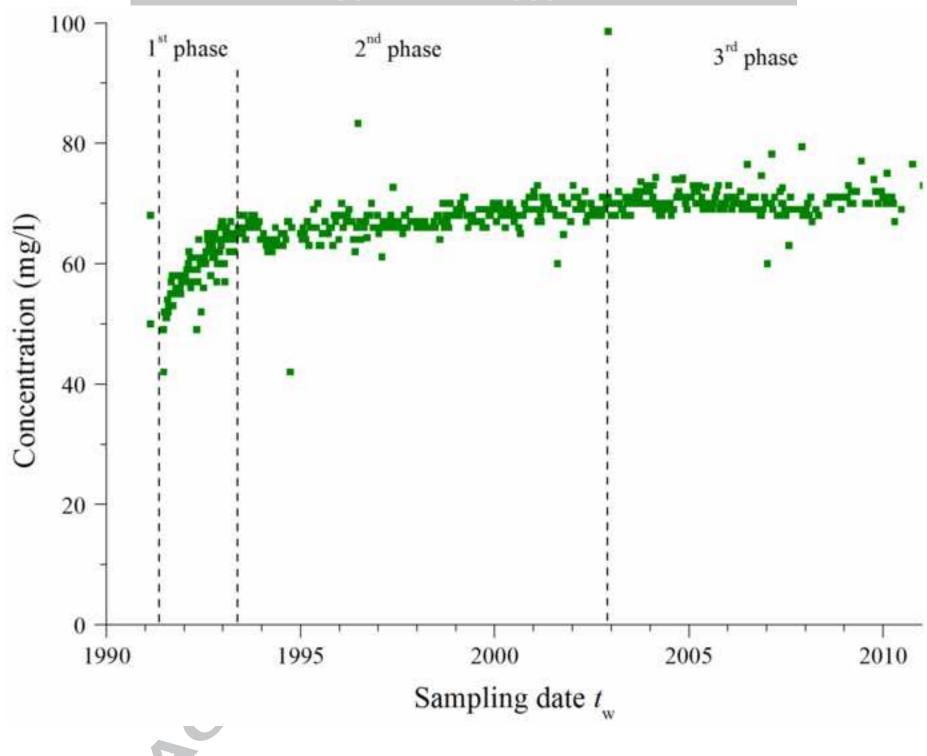


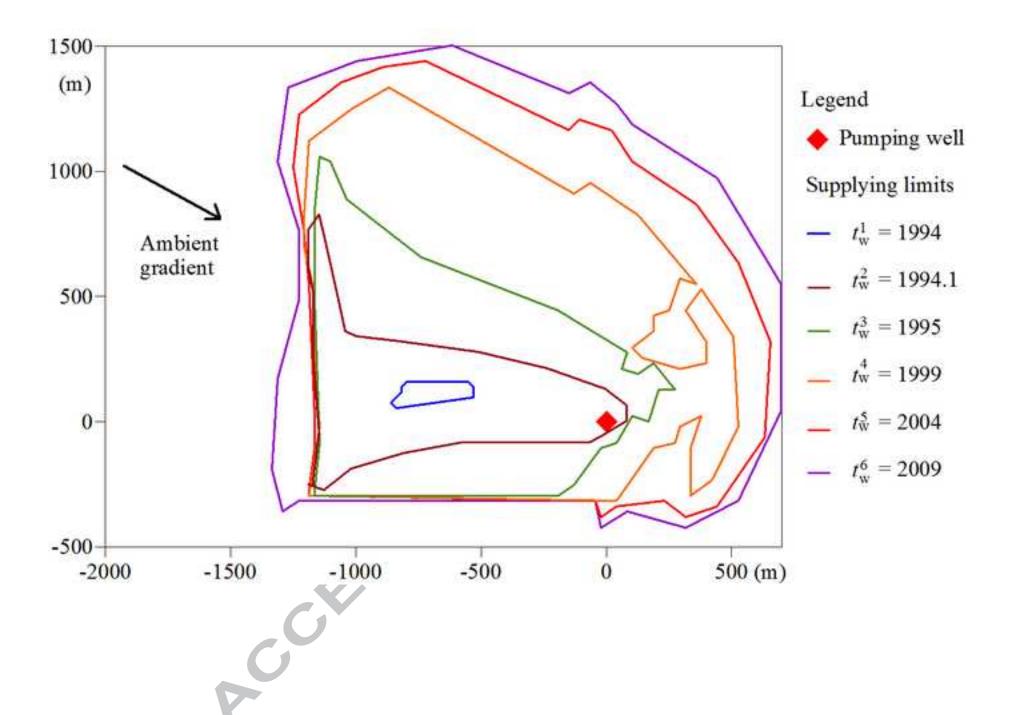
Figure9





ACCEPTED MANUSCRIPT





Highlights:

- Pumping start is modeled by an immediate shift between two steady-state flow fields •
- Ages deduced from CFCs and SF₆ concentrations evolve in two distinct phases •
- Transient flow patterns affect ages just after the pumping start but quickly vanish •
- Atmospheric concentrations then transiently weight the residence time distribution •
- Similar in terms of magnitude, these two regimes are helpful for models segregation •

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