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Clayey-sand filter for the pharmaceuticals removal from wastewater effluent: Percolation experiments

T. Thiebault,*^a M. Boussafir,^a R. Guégan,^a C. Le Milbeau^a and L. Le Forestier^a

The objective of the study was to evaluate the sorption of a pool of pharmaceutically active compounds (PhACs) onto a clay-sand filter in a dynamic sorption experiment. The chosen adsorbent should have suitable chemical properties for the removal of the targeted PhACs and also consistent hydrodynamic behavior regarding field application. In this aim, the impact of interfoliar cation (Ca^{2+} or Na^+) intercalated into natural montmorillonite (Swy2) was tested by using different clay-sand ratios (from 0% to 100% of clay minerals). Only Ca-Swy2 showed a consistent hydraulic conductivity for field application with a value of 4.78 x 10⁻⁸ m.s⁻¹ for 5%-95% clay-sand ratio. The sorption of PhACs onto this filter was investigated using œdometer cells by varying two parameters, the solution matrix (ultra-pure water or natural effluent) and the injection pressure (0.1 MPa and 0.2 MPa). PhACs were effectively adsorbed onto the filter for each experiment at different levels. The drop in injection pressure was a favorable factor for sorption whatever the matrix, with median global removal of ~45% at 0.2 MPa and ~75% at 0.1 Mpa. The effect of the matrix exhibited two different trends as a function of the molecular charge of each PhAC. While cationic compounds were more effectively sorbed in the ultra-pure water matrix than in effluent matrix the sorption of anionic PhACs was more effective in the effluent matrix than in ultra-pure water. This indicates that the charge of the pollutant is a key parameter controlling the efficiency of the adsorbent. Despite these removal variations, the filter exhibited a significant sorption capacity especially at 0.1 MPa. It can therefore be an efficient solution for the removal of PhACs by tertiary filtration.

1 Introduction

2 Emerging Pollutants (EPs) represent a common form of 3 pollution in numerous water compartments, from 4 effluents to drinking water. Pharmaceutically Active 5 Compounds (PhACs) account for more than 3,000 6 compounds among the most concentrated and 7 persistent ones in the environment.^{1,2} They constitute a 8 representative part of EPs due to their wide variety of chemical properties.^{3,4} 9

10 Ever since the study by Richardson and Bowron 11 highlighting the fate of pharmaceutical residues in the environment,⁵ several investigations have been 12 13 conducted in this field over the last thirty years. Studies have focused on the removal of PhACs in Waste-Water 14 Treatment Plants (WWTPs),^{6,7} and on improving the 15 sensitivity of analytical methods in order to better 16 17 characterize their occurrence in the environment.^{8,9}

- 18 There are three main types of WWTPs: activated sludge
- 19 treatment plants, phytoplanted filters or lagoon-based

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systems, but the removal of EPs remains insufficient for 20 all of them. ^{10–12} The main consequence of this lack of 21 22 efficiency is the constant discharge of PhACs into the 23 aquatic system. Even if PhACs are present in natural 24 waters at relatively low concentrations, from several ng.L⁻¹ to μ g.L⁻¹,^{14,13} their toxicity has been widely 25 proved,^{14,15} particularly for endocrine disruptors.^{16,17} 26 27 Moreover, some PhACs can be concentrated in natural beings,18 and contaminate the whole trophic chain 28 29 including humans with poorly-known consequences.¹⁹ 30 While this contamination goes beyond issues of human 31 health, it raises awareness of the hazards generated by 32 EPs and particularly PhACs.

Waste-water treatment is framed by two major factors,
purification capacity and cost. Numerous innovative
methods such as activated carbon or UV-oxidation
exhibit excellent results for the removal of EPs but are
often reserved for drinking water treatment due to
prohibitive costs.²⁰ In addition, oxidation creates
metabolites,²¹ whose toxicity is still unknown today.
Ali et al. showed by a simple calculation between several

Ali et al. showed by a simple calculation between several removal techniques that adsorption mechanisms are the most appropriate and easiest way to remove both inorganic and organic micro-pollutants,²² since the adsorbent material has a large specific surface and a good affinity with the targeted micro-pollutants.^{23,24}

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⁺ Footnotes relating to the title and/or authors should appear here.

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Drug	Abbreviatio n	CAS-Number	M _w	рКа	log K _{ow}	Sw	Charge	
Atenolol C ₁₄ H ₂₂ N ₂ O ₃	ATE	29122-68-7	266.34	9.6	0.16	300	+	
Codeine C ₁₈ H ₂₁ NO ₃	COD	76-57-3	299.36	8.21	1.2	79 x 10 ²	+	
Diazepam C ₁₆ H ₁₃ ClN ₂ O	DIA	439-14-5	284.74	3.4	2.82	50	0	
Diclofenac C ₁₄ H ₁₁ Cl ₂ NO ₂	DCF	15307-79-6	296.15	4.15	4.06	50 x 10 ³	-	
Doxepin C ₁₉ H ₂₁ NO	DOX	1229-29-4	279.38	8.96	3.86	32 x 10 ³	+	
Gemfibrozil C ₁₅ H ₂₂ O ₃	GEM	25812-30-0	250.33	4.8	4.33	4.97	-	
buprofen C ₁₃ H ₁₈ O ₂	IBU	15687-27-1	206.28	4.91	3.72	21	-	
Ketoprofen C ₁₆ H ₁₄ O ₃	KET	22071-15-4	254.28	4.45	2.81	51	-	
Vietoprolol C ₁₅ H ₂₅ NO ₃	MET	56392-17-7	267.36	9.6	1.79	47 x 10 ²	+	
Naproxen C ₁₄ H ₁₄ O ₃	NAP	22204-53-1	230.26	4.15	3	15.9	-	
Dxazepam $C_{15}H_{11}CIN_2O_2$	OXA	604-75-1	286.97	1.7- 11.6	2.31	20.71	0	
$C_{21}H_{30}O_2$	PRO	57-83-0	314.46	-	4.04	8.81	0	
C ₁₆ H ₂₅ NO ₂	TRA	27203-92-5	263.37	9.41	2.51	75 x 10 ³	+	
C ₁₄ H ₁₈ N ₄ O ₃	TRI	738-70-5	290.32	7.2	0.38	400	0	

With M_w, the molecular weight in g.mol⁻¹, pKa the acid dissociation constant, log K_{ow} the octanol/water partition coefficient, S_w the solubility in water at 25°C in mg.L⁻¹ and Charge, the dominant form at pH=7

Table 1: Selected pollutants and parameters used in this work

77 the feasibility of a clay-based filter for the removal of 78 PhACs.

46 Natural materials such as clays offer a good balance 47 between reactivity and cost for the treatment of 48 effluents.²⁵ The efficiency of clays CEC (Cationic

Exchange Capacity) in water is well documented. $^{\rm 26\mathcharmonic 26\$ 49 50 After all, numerous PhACs are not in cationic form but in

51 neutral or anionic form in environmental

52 conditions. Another key parameter is the influence of 53 the solid-liquid ratio, which is often very remote from realistic applications.^{29,30} The latter two studies sought 54 to gain a better understanding of sorption mechanisms 55 56 for which starting concentrations are often largely 57 overestimated compared to simulation approaching field 58 conditions. To our knowledge, no study has investigated 59 the sorption of PhACs at low starting concentrations (25 60 μ g.L⁻¹) onto natural clays. However sorption experiments 61 with PhAC concentrations that are as close as possible to 62 those found in natural environments and water 63 purification plants are necessary in order to estimate the 64 efficiency of sand and clay mixtures and the real 65 affinities between the tested materials and the targeted 66 pollutants.

67 A similar concern also frames the choice of the 68 geosorbents and their characteristics as interlayer 69 cation, which controls the sorption capacity and hydrodynamic behavior.^{31,32} 70

71 In view of the well-established capacity of clays to 72 remove numerous compounds from water, the present

73 study addressed three main issues: (i) the real capacity

74 of slightly modified clay to treat a complex solution in

75 pure water or effluent (ii) the impact of the kinetic

76 transfer and the matrix effect on the sorption and (iii)

79 Materials and Methods

80 Filter: clay minerals and sand

- 81 The sand used was uniformly fine-grained Fontainebleau
- 82 quartz sand (from the Paris basin, France) of analytical
- 83 grade, and with a granulometry of 100-150 MESH.
- 84 The clay mineral chosen was Swy2 Wyoming 85 montmorillonite (Crook County Wyoming, United 86 States), supplied by the Source Clays Repository of the 87
- Clay Minerals Society. After <2 µm fractionation by 88 gravity sedimentation, the Swy2 sample was Na-
- exchanged by well-established procedures.33 This Na-89
- 90 Swy2 was the starting material for the production of Ca-
- 91 Swy2 with the same procedure, by replacing NaCl with
- 92 CaCl₂. These two interlayer cations were chosen because
- 93 of their predominance in the environment.
- 94 Different proportions of sand and clay were tested to
- 95 estimate the hydrodynamic properties of the resulting
- 96 mix, with clay percentage in the filter of 5%, 10%, 50%
- 97 and 100% (i.e. pure clay) and with a constant total mass
- 98 of 8.0 ± 0.4g. For percolation tests with PhACs, a 5% clay 99 filter was used.

100 PhACs and chemical reagents

101 The 14 PhAC standards (purity grade > 98%; see Table 1

102 for details) were obtained from Sigma-Aldrich for ATE,

- 103 COD, DIA, DOX (Doxepin Hydrochloride), GEM, KET, MET
- 104 (Metoprolol Tartrate salt), NAP, OXA, PRO, TRA
- 105 (Tramadol Hydrochloride), TRI, and from Acros Organics
- 106 for DCF (Diclofenac Sodium) and IBU.

- 107 Chemical reagents of analytical grade, methanol (MeOH)
- 108 and pyridine were purchased from Fisher Scientific. N-
- 109 tert-Butyldimethylsilyl-N-methyltrifluoroacetamide
- 110 (MTBSTFA, >95%) was supplied by Sigma-Aldrich.

111 Percolation Experiments

112 Percolation experiments were carried out in œdometer
113 cells. This specific equipment was developed to
114 understand the hydrodynamic behavior of a solid sample
115 under different conditions.³⁴

116 The œdometer cell (internal diameter = 0.04 m) and the 117 injection syringe were both connected to a distinct 118 compressed-air system in order to apply respectively the 119 mechanical pressure on the sorbent material and the 120 injection pressure on the leaching solution. The 121 equipment scheme and further details are given in 122 Figure S1 and in Gautier et al.³⁵

123 For each experiment, 8 g of material (clay-sand mix) was 124 gradually compacted on the bottom side up to 0.5 MPa, 125 then totally unloaded, and compacted again at a 126 mechanical pressure of 0.3 MPa. The solution was 127 injected at the upper side into this compacted sample at 128 a constant pressure during experiments. The injection 129 pressure is the variable which controls the interaction 130 kinetic between the solution and the material. Indeed, 131 œdometer cells enable physical and hydraulic properties 132 to be jointly controlled. Two different injection pressures 133 were used in this study, 0.1 and 0.2 MPa.

134 In order to control impact of the matrix on the 135 adsorption of PhACs, two solutions were used in the 136 experiments: (i) a mix, hereafter called S, of each of the 137 14 selected PhACs at concentrations around 25 µg.L⁻¹ in 138 ultra-pure water, and (ii) a mix between the 14 PhACs 139 and an effluent of a French rural WWTP, called N. 140 Although PhACs were present in this effluent their 141 maximum concentration around 200 ng.L⁻¹ did not affect 142 our results by modifying starting concentrations 143 noticeably (Table S1 for details, and Table S2 for the 144 chemical parameters of the chosen effluent).

145 The choice of the starting concentration at 25 μ g.L⁻¹ for 146 each PhAC corresponds to the maximum PhAC 147 concentrations in some effluents.¹³

148 During percolation experiments, leachate samples were 149 collected each time that a volume of 100 mL solution

- 150 passed through the filter. A total of 1 L (10 x 100 mL) was
- 151 therefore used for each percolation experiment.

152 Leachate and clay analyses

153 Leachate analysis

154 Leachate solutions were concentrated by Solid-Phase155 Extraction (SPE) and analyzed by Gas Chromatography156 coupled to Mass Spectrometry (GC-MS).

PhAC extraction was carried out on a 6mL glass cartridge
filled with HR-X phase (Macherey-Nagel). Cartridges
were conditioned with 5 mL of MeOH then with 5mL of
ultra-pure water. Columns were filled with 100 mL of
sample and then rinsed with 5 mL of ultra-pure water
before drying for 30 minutes under vacuum. Finally,

elution was performed with 3 x 5 mL of MeOH.
Thereafter, internal standard was added to organic
layers, which were evaporated under reduced pressure.
Residues were derivatized with MTBSTFA according to
Schummer et al.³⁶

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168 Analyses were performed on a Trace GC Ultra gas
169 chromatograph (GC) coupled to a TSQ Quantum XLS
170 mass spectrometer equipped with an AS 3000
171 autosampler (both from Thermo Scientific). The GC was
172 fitted with a Thermo Trace Gold TG-5 MS capillary
173 column (60 m, 0.25 mm i.d., 0.25 µm film thickness).

174 The temperature of the column was held at 50°C for 3 175 min, increased from 50 to 120°C at 30°C.min⁻¹, and from 120 to 310°C at 3°C.min⁻¹ with a final isothermal hold at 310°C for 21 min. 2 μ L of sample was injected in splitless 178 mode at 280°C. Helium was the carrier gas (1 mL.min⁻¹). 179 The mass spectrometer was operated in EI mode at 70 180 eV, from m/z 50 to 500.

181 Clay characterization and global carbon analysis

182X-ray diffraction (XRD) patterns were recorded between1832 and 64° (20) using a Thermo Electron ARL'XTRA184diffractometer equipped with a Cu anode (Cu K α 1,2 =1851.5418 Å) coupled with a Si(Li) solid detector.186Experimental measurement parameters were 10s187counting time per 0.04°20 step. The diffractograms were188performed with dry powder samples (100 °C for 24 h).

189 Fourier transform infrared (FTIR) measurements were
190 recorded in the range 650-4000 cm⁻¹, using a Thermo
191 Nicolet 6700 FT spectrometer equipped with a
192 Deuterated Triglycine Sulfate (DTGS) detector and a
193 Nicolet Continuum microscope. The analyses were
194 performed in transmission mode and each spectrum was
195 the average of 256 scans collected at 2 cm⁻¹ resolution.

196 Carbon and nitrogen analyses were performed on197 powdered samples by using a Thermo Scientific Flash2000 organic analyzer assuming an analytical error of199 0.05%.

201 Data analysis

200

202 To characterize the distribution of a compound between 203 a potential sorbent and the dissolved phase, the Log K_d 204 parameter is often used.³⁷ The computation 205 corresponding to its calculation is expressed as follows: 206 $\log(K_d) = \log(\frac{q_s}{q_a})$ (1)

207 with K_d the solid-liquid distribution coefficient (L.kg⁻¹), q_s 208 the sorbed concentration (mg.kg⁻¹) and q_e the 209 equilibrium concentration (mg.L⁻¹).

Statistical tests were performed to verify the significanceof some hypothesis using the Student test with a chosen

212 statistical threshold of 0.01 for the resulting *p*-values.

213 To estimate the link between time and sorption capacity 214 and to describe the sorption dynamic, the first-order

- 215 Lagergren equation, the second-order kinetics model
- and the Bangham equations are often used.³⁸217

218	These	equations	are	expressed	in	linear	form	by
219	equation	ons (2)-(4) re	espec	tively:				

220
$$\log(q_m - q_t) = \log q_m - \frac{k_1}{2.303}t$$
 (2)

$$221 \quad \frac{1}{q_t} = \frac{1}{k_2 q_m^2} + \frac{1}{q_m} t \tag{3}$$

222 $\log q_t = \log k_b + \frac{1}{n} \log t$ (4)

223 with q_t the sorbed concentration in µg.mg⁻¹ at the time t (min), q_m the pseudo-equilibrium sorbed concentration 224 (μ g.mg⁻¹), k_1 (min⁻¹), k_2 (g.g⁻¹.min⁻¹) and k_b (g.g⁻¹.min⁻¹) 225 respectively the first-order, the second-order and the 226 227 Bangham sorption rate constants.

228 Each equation is based on different assumptions:

229	(i)	the first-order Lagergren model considers
230		that the quantity of unoccupied adsorption
231		sites is proportional to the adsorption rate
232		of adsorbate onto adsorption sites

233 (ii) the second-order kinetic model assumes 234 that the adsorption is chemically 235 accomplished

236 The Bangham equation considers a fast (iii) 237 velocity of adsorption and a slow 238 attainment of sorption equilibrium

239 These equations were applied to the experimental 240 results.

241 **Results and discussion**

242 Hydrodynamic properties

243 Percolation experiments were first performed with 244 water solution in order to determine the hydraulic 245 conductivity (K) of the different clay-sand materials. K, expressed in m.s⁻¹, was calculated from Darcy's law, 246 247 using the expression developed for a saturated 248 medium:³⁹ 0

$$249 \quad K = \frac{Q}{i.S}$$

250 where Q is the measured volumetric flow rate $(m^3.s^{-1})$ at 251 the steady state, *i* is the hydraulic gradient and *S* is the 252 cross-sectional area of the œdometer cell (m²).

253 For a potential environmental application, the clay-sand 254 filter should have hydrodynamic properties that 255 correspond to the hydraulic conductivities operable in 256 actual treatment installations, whereas clays are a 257 natural barrier used for example to trap nuclear wastes.40 258

Clays	SSA	CEC	ε _{max}	Θ _{max}
Na-Swy2	45.4 ^ª	85.0±2.7 ^ª	37% ^a	75%
Ca-Swy2	46.0 ^b	85.1±0.01 ^b	1.5%	62%

With SSA, Specific Surface Area (m^2, q^{-1}) ; CEC, Cationic Exchange Capacity (meq.100g⁻¹ of clays); ε_{max} the maximum axial swelling strain for 100% clay $\int 1000^{-1} of clays$; ε_{max} the maximum axial swelling strain for 100% clay sample; Θ_{max} , the maximum water content for 100% clay sample and $^{\circ}$

<u>28</u>9 259 Table 2: Main properties of the selected clays saturated with Na⁺ and Ca²⁺ as 290 260 interfoliar cations

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288

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Figure 1: Hydraulic Conductivity as a function of the clay percentage in the claysand filter with circle: pure sand, triangles: clay-sand filters with Na-Swy2 and squares: clay-sand filters with Ca-Swy2

261 This specific application should find a good balance 262 between high permeable Fontainebleau sand and Na- or 263 Ca-Swy2 clay with a low permeability.

264 Different clay-sand ratios were tested for both Na- and 265 Ca-SWy2 in order to simulate and calculate the 266 maximum flow of solution that can pass through the 267 filter.

268 In accordance with the aim of this work, the ideal clay-269 sand ratio should include a low proportion of clay. As 270 expected, the decrease in K was correlated with the finer 271 texture related to the increase in clay percentage. 272 Nevertheless, this evolution differed between the two 273 clay materials tested (Figure 1):

- The NaSwy2-Sand mix can be considered as a waterproof material with K values between 1.35e⁻⁹ m.s⁻¹ (5% clays) and 1.5e⁻¹² m.s⁻¹ (50% 276 clays)
 - The CaSwy2-Sand mix allowed a better percolation at a low clay proportion with K between $4.76e^{-8}$ m.s⁻¹ (5% clays) and $1.11e^{-9}$ m.s⁻¹ (50% clays)

282 This permeability gap between the two materials can be 283 explained by the differences in physico-chemical clay 284 properties. Whereas the specific surface area and the 285 cationic exchange capacity were similar for both Na- and 286 Ca-Swy2 (Table 2), their macroscopic swelling 287 performance varied greatly impacting their Θ_{max} value.

Injection Pressure	0.1	MPa	0.2 1	0.2 MPa		
Matrix	S	S N		N		
Abbreviation	\$1	N1	S2	N2		
Q	9	9.1	17.9	18		
Filter						
thickness (mm)	4.39	4.24	4.05	3.95		
pН	6.5	6.7	6.5	6.7		

Table 3 Experimental conditions for percolation experiments with PhACs in solution through a filter composed of 5% of Ca-Swy2 and 95% of Fontainebleau sand

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292 The maximum axial swelling strain ε_{max} , deduced from 293 the measured axial displacements of the piston, 294 revealed a high degree of swelling for the Na-Swy2 295 smectite compared to Ca-Swy2, 37% and 1.5% 296 respectively (Table 2).

297 The high swelling capacity of Na-Swy2 influenced the
298 decrease in *K* especially at a low clay percentage (5%).
299 Conversely the extremely low macroscopic swelling for
300 Ca-Swy2 indicates a textural and crystalline swelling
301 control on the decrease in *K*. 5% was the clay proportion
302 selected for the percolation experiments with PhACs in
303 solution.

304 Ca-Swy2 presents another advantage compared to Na-305 Swy2 for a field use: the high macroscopic swelling 306 capacity of Na-Swy2 under wet conditions could damage 307 installations which are subjected to dry/wet cycles. 308 While the mechanical behavior of the Ca-Swy2 smectite 309 in association with sand was very similar to non-swelling 310 clay (such as kaolinites) with a low impact of dry/wet 311 cycles, this adsorbent was characterized by a high 312 specific surface area, making it suitable for interaction 313 experiments with emerging organic pollutants.

In view of the very low permeability of the NaSwy2-sand
mix, percolation experiments with the PhACs in solution
were carried out only with CaSwy2-sand materials as

317 filter. The experimental conditions for the percolation 318 tests with a 5-95% CaSwy2-sand mix are presented in

319 Table 3.

320 Drug Removal

321 The global removal of the PhAC pool can be used to 322 estimate the efficiency of the filter in different

323 experimental conditions.

 $324 \quad \text{The term } C_0 \text{ was calculated by the addition of the initial} \\$

325 concentrations of the 14 PhACs and C corresponds to the

addition of the 14 PhAC concentrations for one collectedsample.



Figure 3: Additive sorption (C/C_0) of all the pharmaceuticals for each experiment: boxes were computed from the removal values added for the 14 pollutants for 10 independent measurements. The line within the box marks the median, boundaries indicate the 25th and 75th percentiles, and error bars indicate the maximum and the minimum removal measurements

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328 The spread of the ten values is around 10% of the total 329 removal (Figure 2) indicating a good regularity in the 330 sorption capacity of the tested material. The adsorption 331 capacity was significant (i.e. > 40%) for all the 332 experimental conditions and the total removal reached 333 was between the extreme values of 35 and 85%. No 334 significant differences in total C/C_0 in the global removal 335 were observed for the two matrices at the same 336 pressure (p = .04 and .06 at 0.1 and 0.2 MPa 337 respectively). The median removal was around 75% at 338 0.1 MPa and 50% at 0.2 MPa whatever the matrix. The 339 enrichment of the matrix with natural organic matter 340 (NOM) and electrolytes (matrix N) appeared to have no 341 impact on global removal whereas the drop in injection 342 pressure significantly enhanced removal (p<.01 between 343 N1 and N2 and between S1 and S2).

344 Partition and removal efficiency of targeted PhACs

345 The solid-liquid distribution coefficient (K_d) is often used 346 to determine the ability of a material to sorb compounds 347 from a solution. This parameter was used to calculate 348 the partition between the solution and the sorbent for 349 each collected sample and estimate its variability 350 between the ten samples for each percolation 351 experiment. Unlike modeling equations of sorption 352 kinetic, the K_d value does not directly depend on the 353 duration of the experiment.

354 Due to the chosen solid-liquid ratio, PhACs were half-355 sorbed (50:50) if, Log $K_d = 3.40 \text{ L.kg}^{-1}$, and the starting 356 concentration is precisely 25 µg.L⁻¹.



Figure 2: Additive sorption (C/C₀) of the cationic pharmaceuticals for each
experiment: boxes were computed from the removal values added for the 14
pollutants for 10 independent measurements. The line within the box marks the
median, boundaries indicate the 25th and 75th percentiles, and error bars indicate
the maximum and the minimum removal measurements

362 Cationic Species

363 Two major trends emerged from the analysis of the total 364 C/C_0 values for the cationic species (Figure 3).

365 The decrease in the injection pressure, corresponding to 366 a slowdown of the flux was a favorable factor for 367 sorption. For all the compounds, the transition from S2 368 to S1 was accompanied by a significant increase in the 369 Log K_d (*p*<.01 for the whole cationic compounds) 370 together with an increase in the total removal (Figure 3).

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	S1		N1		\$2		N2		onto Sludge
	Log K _d	MRv	Log K _d	MRv	Log K _d	MRv	Log K _d	MRv	Log K _d
Cationic Specie	s								
ATE	4.99 ±0.03	97.0 ± 0.04	4.34 ±0.04	87.6 ± 0.09	3.43 ±0.05	46.2 ± 0.41	3.31 ±0.04	37.2± 0.39	1.58 ^a
COD	4.74 ±0.02	95.2 ± 0.03	4.31 ±0.04	88.6 ± 0.11	4.03 ±0.06	73.2 ± 0.24	4.26 ±0.02	86.4± 0.09	1.15 ^{a,b}
DOX	5.79 ±0.01	99.6 ± 0.01	4.86 ±0.02	96.2 ± 0.03	5.38 ±0.01	98.9 ± 0.01	4.57 ±0.02	93.2 ± 0.03	2.14 ^b
MET	5.09 ±0.03	96.9 ± 0.03	4.34 ±0.03	89.0 ± 0.08	4.01 ±0.03	77.2 ± 0.16	3.96 ±0.01	75.8 ± 0.12	1.81 ^b
TRA	4.63 ±0.03	94.3 ± 0.04	3.96 ±0.04	74.6 ± 0.24	3.94 ±0.02	77.2 ± 0.14	3.65 ±0.02	60.4 ± 0.19	1.67 ^b
TRI	4.76 ±0.02	95.3 ± 0.06	4.90 ±0.04	96.4 ± 0.03	4.87 ±0.05	95.0 ± 0.04	4.36 ±0.02	91.4 ± 0.07	1.15 ^b
Neutral Species									
DIA	4.20 ±0.03	86.5 ± 0.07	4.19 ±0.03	86.1 ± 0.09	3.45 ±0.04	44.4 ± 0.46	4.33 ±0.04	90.1 ± 0.59	1.72 ^b
OXA	3.78 ±0.01	71.6 ± 0.09	3.84 ±0.01	74.4 ± 0.12	2.01 ±0.13	2.0 ± 0.56	3.17 ±0.01	34.4 ± 0.19	1.11 ^b
PRO	4.92 ±0.01	97.4 ± 0.01	4.76 ±0.02	96.1 ± 0.03	5.80 ±0.03	99.5 ± 0.01	5.77 ±0.03	99.6 ± 0.01	3.28 ^a
Anionic Species									
DCF	3.45 ±0.02	55.3 ± 0.12	3.60 ±0.02	59.8 ± 0.19	2.99 ±0.02	26.2 ± 0.35	3.01 ±0.02	28.9 ± 0.36	1.2 ^c
GEM	3.76 ±0.02	71.6 ± 0.09	3.72 ±0.02	67.2 ± 0.18	2.71 ±0.05	13.9 ± 0.72	3.48 ±0.01	52.6 ± 0.16	0.95 ^a
IBU	3.07 ±0.02	34.2 ± 0.35	3.35 ±0.01	48.3 ± 0.22	2.08 ±0.04	5.1 ± 0.58	2.61 ±0.04	12.5 ± 0.93	2.23 ^a
KET	4.11 ±0.04	81.9 ± 0.03	4.12 ±0.02	84.5 ± 0.09	3.44 ±0.04	40.0 ± 0.56	3.99 ±0.01	79.8 ± 0.05	-
NAP	3.12 ±0.02	40.4 ± 0.29	3.55 ±0.02	53.7 ± 0.41	2.26 ±0.12	6.1 ± 0.86	2.96 ±0.01	24.5 ± 0.27	2.08 ^a
with Log K_d in L kg ⁻¹ , MRv in %, Relative Standard Deviation values equal to Average/Standard Deviation for n=8 (clipped for the two extreme samples) and values onto sludge from a ⁴² , b ⁴³ and c ⁴⁴									

Table 4: Log K_d values and Mean Removal values (in %) for selected pollutants

372 \pm Relative Standard Deviation for each experiment, compared to Log K_d values

373 found for PhACs onto sludge in the literature

374 Whereas for the S2 experiment, Log K_d values varied 375 between ATE (3.43) and DOX (5.38), Log K_d values were

376 more homogeneous for the S1 experiment (Table 4).

Whatever the injection pressure, the retention of
cationic PhACs was generally favored in the case of ultrapure water (S), except for TRI at 0.1 MPa and COD at 0.2
MPa for which the opposite was recorded. The cationic
PhACs were probably in competition with other
components (organic or inorganic) contained in the

383 wastewater effluent. As a result, the adsorption of

cationic PhACs was lower in matrix N than S (*p*<.01 forthe two injection pressures).



Figure 4: Additive sorption (C/C_0) of the anionic pharmaceuticals for each experiment: boxes were computed from the removal values added for the 14 pollutants for 10 independent measurements. The line within the box marks the median, boundaries indicate the 25th and 75th percentiles, and error bars indicate the maximum and the minimum removal measurements

386 Anionic species

For anionic PhACs, the shift to a lower injection pressure
was also favorable for sorption (Figure 4), especially for
IBU in ultra-pure water (S2 vs S1) (Table 4). These results
indicated that the interaction kinetic is an important
component of the sorption, as for cationic PhACs.

392 The complexation of the matrix, especially at 0.2 MPa, 393 significantly increased the sorption of all the anionic 394 PhACs (p<.01 at 0.1 and 0.2 MPa). Between S1 and N1, 395 except for IBU, DCF and NAP (e.g. 3.10 to 3.54 396 respectively), the variations in Log K_d values were not 397 statistically significant (p = .44 and .36 for GEM and KET 398 respectively).

400 Neutral Species

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401 The solid-liquid distribution variations for the three 402 neutral PhACs did not follow a trend. It was therefore 403 difficult to evaluate the impact of the matrix or of the 404 injection pressure. Whereas PRO was well sorbed 405 whatever the experimental conditions, for DIA and OXA, 406 variations in the Log K_d values were closer to the 407 behavior of anionic species (Table 4).

408 Partition control factors

409 The effect of ionic strength or of the presence of organic 410 matter in water, which can favor the sorption of anionic 411 species, was confirmed by the experimental results as 412 suggested in other studies.⁴⁵ This assumption can be 413 explained by the adsorption of organic compounds or 414 electrolytes which could enhance the anionic sorption 415 capacities of the clay material.⁴⁶

416 Kinetic transfer is the second major influence on the
417 sorption capacity. The sorption improvement is
418 particularly strong on anionic species, whose sorption
419 kinetic is known to be slower to reach equilibrium,⁴⁷
420 than that of cationic species (Figure 4).²⁷

421 Measurements of Log K_d values are generally performed 422 onto sludge to better understand the partition of PhACs 423 during waste-water treatment.^{42–44} Thus, sorption on 424 sludge can be considered as a removal despite the 425 variable further use of sludge. If we compare the Log K_d 426 values onto secondary sludge in the literature for each 427 compound (Table 4), there is no link between the charge 428 of the pollutant and the Log K_d . IBU or NAP are well 429 sorbed onto sludge whereas other anionic compounds 430 have a Log K_d < 2. These compounds were also among 431 the three anionic compounds to be significantly better 432 sorbed in N matrix than S (Table 4) at 0.1 MPa. The 433 combination of these two factors demonstrated the 434 NOM impact on the sorption of some anionic PhACs.

435 For cationic species, only one value (for DOX) exceeds 2436 and only the neutral compound PRO is well sorbed by437 sludge.

438 The affinity of our material with PhACs was far greater 439 than that of sludge, with Log K_d values up to at least for 440 the N1 experiment, indicating that the chosen material 441 has better trapping properties than sludge.

The greater complexity of sludge in terms of chemical
reactivity results in a variable affinity with the targeted
PhACs that does not depend only on the charge of the
pollutants,⁴⁸ whereas with clay material, the charge
seems to play the most important role in the control of
sorption.

448 Sorption kinetics modeling

449 Based on the obtained correlation coefficients of the 450 three models tested that spread out from 0.90 to 0.999 451 (Tables S3, S4 and S5), it appears that the experimental 452 data are better adjusted with Bangham equation (r² 453 comprised between 0.970 and 0.999). Nevertheless, the 454 whole models used here provide similar trends. The 455 efficiency of the adsorption is enhanced at high pressure 456 as shown by k_1 constants (first-order Lagergen). Figures 457 5 and 6 confirm and highlights the sorption rate was 458 higher at 0.2 MPa than at 0.1 MPa indicating a better 459 sorption efficiency at higher kinetic percolation.

460 The second-order Lagergren (Table S4) and Bangham 461 (Table S5) equations suggested a good regularity of the 462 removal quality of the material as Log K_d standard 463 deviation values expressed.

464 For the best sorbed compounds DOX, PRO and TRI, the 465 comparison of k_2 and q_m values indicated the same 466 trends as those observed with the Log K_d analysis on the 467 matrix effect. An increase in log k_2 corresponding with a 468 drop in q_m between respectively S and N (for each 469 injection pressure) indicated a matrix effect that was

470 unfavorable for the adsorption of cationic compounds.



Figure 5: Bangham fits (solid lines) for (a) Tramadol (cationic) and (b) Ketoprofen (anionic) for each experiment



473 The exact opposite was observed for IBU, OXA and NAP, 474 with a lower log k_2 and a higher q_m for N than S. For the 475 other compounds, the data can be interpreted as shown 476 in Figure 5. For cationic species, there was a slight 477 unfavorable effect of the N matrix whereas the opposite 478 was observed for anionic species.

479 Unlike the Log K_d values, the modeling and resulting 480 sorption efficiency values gave contrasting results. The 481 main controlling factor for the sorption capacity of Ca-482 Swy2 towards PhACs is the chemical properties of the 483 molecule. As this material has a greater cationic than 484 anionic exchange capacity, cationic compounds were 485 strongly favored for sorption.

486 Otherwise, the sorption of anionic compounds was 487 slightly better in effluent matrix than in ultra-pure water 488 but it remained significantly lower than for cationic 489 compounds. This enhancement of anionic species 490 adsorption by the addition of NOM or electrolytes has 491 already been reported for IBU alone onto 492 montmorillonite, indicating that without a saturation 493 effect, the behavior of a pool of PhACs with Ca-Swy2 is 494 similar to that of a single PhAC.

495 Model fittings demonstrated that Ca-Swy2 has a large496 sorption capacity spectrum even if the molecular charge497 remained a key factor for the removal ratio.

498 While the better removal efficiency at a lower injection 499 pressure seemed to improve sorption, modeling results 500 showed that the sorption rate was higher for higher 501 injection pressures. With a view to optimizing the kinetic 502 transfer through the filter, further data need to be 503 obtained to combine the best removal efficiency with 504 the best sorption rate constant.

505 Clays characterization

506 Clays were separated from sand after the leachate test
507 for further characterization. Two methods were applied
508 to investigate the adsorbent reaction to the leachate,
509 XRD and FTIR analysis.

510 XRD and FTIR exhibited no significant layer expansion or511 band stretching respectively after experiments.

512 Elemental analyses were carried out on the clay minerals 513 after the percolation of 1 liter in order to estimate the 514 total sorbed concentration based on the carbon 515 percentage of the clays (Figure 7).

516 The comparison between elemental analyses on clays 517 and leachate sample analyses exhibited similar results 518 for the ultra-pure water matrix. This is consistent with 519 the assumption that clays are responsible for most of 520 the sorption in comparison with sand. Similar results 521 between clays and water samples also indicated that 522 PhACs are effectively adsorbed onto Ca-Swy2 and not 523 degraded furthermore.

524 In accordance with previous results obtained from
525 solution analyses, the total sorbed concentration was
526 higher for S1 than S2, with a total removal of 65.7% and
527 48.2% respectively.

528 For N matrices, the elemental analysis results are
529 significantly higher than those of the leachate samples.
530 This indicates that the material adsorbed more than
531 PhACs from the effluent matrix. The additional organic
532 compounds that were adsorbed may possibly explain the
534 Sorption Mechanisms

535 Despite the excellent removal efficiency of the prepared 536 mineral mixture in this study, sorbed PhACs amounts 537 remain low due to the selected starting concentrations that were 25 $\mu g.L^{\text{-1}}.$ Since the sorbed amounts for the 538 539 whole PhACs were rather low, it was rather hard to 540 probe any changes through the use of classical analytical 541 techniques such as FTIR or XRD, which may acknowledge us about conformation of molecules and their 542 543 localization for a proper description of the adsorption 544 processes.



Figure 7: Comparison between the total sorbed concentrations calculated by elemental analysis of clays (white bars) and from the leachate samples (gray bars) for each percolation test. The dotted line corresponds to the total injected concentration of PhACs

545 Nevertheless, it appears that the sorption of anionic 546 PhACs is particularly enhanced for clay mineral with Ca²⁺ as compensating cations. Indeed, $\mathrm{Ca}^{^{2+}}$ is divalent and 547 showed its ability to sorb anionic species by cationic 548 bridges.⁵⁰ Here, the results suggest a better sorption 549 efficiency of anionic species in contrast to previous 550 studies using sodium exchanged Na-Swy2.49,51 However 551 552 electrostatic interactions or even hydrogen bonds cannot 553 be excluded that may play also as driving forces for the 554 adsorption. Further experiments need to be carried out to better point out the sorption mechanisms. 555

556 Cationic species are usually adsorbed on clay mineral 557 through cation exchanges and it may also the case for 558 PhACs here. This mechanism is thermodynamically 559 spontaneous,²⁷ but only compensating cations on the 560 external surfaces are involved since no changes in the 561 diffraction patterns were observed.

562 Conclusions

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563 From the results of this study, the following conclusions 564 can be drawn:

- Natural Ca-saturated smectite (Ca-Swy2) incorporated into a sand-filter allowed a flow consistent with *in-situ* applications whereas Nasaturated smectite (Na-Swy2) is a waterproof material that is not adapted to the sorption of pollutants in a simulation of dynamic sorption close to field reality
 - Ca-Swy2 exhibited a large adsorption capacity even for cationic, neutral and anionic PhACs at similar wastewater pH. With the values of the relative standard deviation of samples, it seems that the sorption efficiency in time is steady. The sorption capacity is guided by two major parameters, infiltration kinetics and the composition of the matrix.
 - The effluent matrix played a contrasting role on the sorption efficiency, depending on the molecular charge and the speciation at the tested pH: anionic species were favored by this complex matrix in contrast to cationic ones, for which the sorption efficiency was lower. Some NOM and/or electrolytes of the effluent were also adsorbed onto the filter and played a key role in the sorption of anionic compounds whereas they were in competition with cationic species. Further analyses need to be carried out to characterize them.
 - The applied models fitted our data well, but due to the pseudo equilibrium that was reached, the calculated constants did not correspond to previous observations for all the models. However, even a low kinetic (0.1 MPa) favored sorption processes, and at higher injection pressure sorption processes were more efficient

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- 604 The key role played by the interlayer cation can 605 direct the choice of geosorbent for further 606 studies, using clays minerals that are naturally 607 saturated by Ca²⁺, rather than by Na⁺
- 608 Implementation in the field of the tertiary 609 treatment technique presented here requires 610 further experiments. Nevertheless, this study 611 stresses out the relevance of the material in a 612 field application for a good removal efficiency 613 especially in comparison with tertiary 614 treatments using chemical products, potentially 615 toxic for the environment. The main question 616 now is the management costs induced by this 617 technique, especially concerning the durability 618 of the filter.

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