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# **Evidence of phase nucleation during olivine diffusion creep: A new perspective for mantle strain localisation**

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- Mantle rheology
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- Creep cavitation

## **Abstract**

**For the past decades, grain size reduction leading to diffusion creep in olivine is believed to be a very important process for strain localisation in the lithospheric mantle. However, the mechanisms of grain size reduction in this regime are still poorly understood (e.g., Platt, 2015). Here we show new experimental results that document grain size reduction and material weakening during wet olivine diffusion creep. While occurring for both, mono-phase and two-phase aggregates, grain size reduction is coeval with strain localisation and local phase mixing in olivine-pyroxene aggregates. Based on evidence of fluid inclusions and cracks filled with a fine-grained phase mixture, we conclude that grain size reduces as a result of fluid-assisted nucleation that takes place in the presence of an aqueous fluid during diffusion creep. Cavitation induced by grain boundary sliding (creep cavitation) can be inferred, and may play a critical role for olivine grain size reduction. Amongst their implications for rock rheology in general, our findings highlight a key process for strain localisation in the ductile uppermost mantle.**

## **1. Introduction**

In order for tectonic plates to be isolated from each other by high-strain plate boundaries, such as subduction zones or narrow rifts, strain localisation has to occur across the strong uppermost mantle (Burov and Watts, 2006; Bercovici and Ricard, 2014). The deformation of the lithosphere strongly depends on this presence or absence of strain localisation. Although some brittle behaviour may be expected in the shallow mantle, extrapolations of lab-based flow laws to corresponding depths give predictions of the uppermost mantle as mostly plastic (Kohlstedt et al., 1995). In this regime, strain localisation typically arises from a local weakening of the deforming rock, the origin of which remains very elusive today.

Olivine is by far the most abundant phase in the upper mantle. For this reason, experimental, field-based, and modelling studies have focussed on the role of olivine for mantle rheology in the last

decades, concluding that grain size reduction and dominant diffusion creep may be the best candidate to account for quasi-viscous strain localisation (Rutter and Brodie, 1988; Drury et al., 1991; Bercovici and Ricard, 2012). Their conclusion is based on the fact that (1) grain size reduction is a ubiquitous feature of ductile shear zones, and (2) diffusion creep (including grain boundary sliding) is grain size sensitive, unlike dislocation creep which does not – or to a lesser extent in the case of disGBS (Hansen et al., 2011) – depend on grain size (Karato et al., 1986; Hirth and Kohlstedt, 2003). However, grain size reduction is not a process which is defined or understood during dominant diffusion creep (e.g., Rutter and Brodie, 1988; De Bresser et al., 2001). Thus, although reducing grain size in this regime may be a key factor for strain localisation (Rutter and Brodie, 1988; Bercovici and Ricard 2012; Platt, 2015), the processes are poorly known and require further investigation.

Many studies have pointed out the presence of minor phases, such as micas or pyroxenes, as a condition for small grain sizes during grain-size-sensitive creep (Hiraga et al., 2010; Herwegh et al., 2011; Farla et al., 2013; Linckens et al., 2014; Platt, 2015). Most of them attributed the reduction of grain size to a combination of dynamic recrystallization and grain boundary sliding (GBS), resulting in phase mixing. Following this approach, Bercovici and Ricard (2012) developed a theoretical model to propose that damages at olivine-pyroxene interfaces would indirectly drive grain size to reduction, provided that grain boundary pinning (Zener pinning) arises from phase mixing. However, natural evidence of grain size reduction induced by pinning of grain boundaries is still lacking; Zener pinning has been only shown to inhibit grain growth, not reducing grain size (Stünitz and FitzGerald, 1993; De Ronde et al. 2005; Warren and Hirth, 2006; Sundberg and Cooper, 2008). Furthermore, the link between phase mixing, grain size reduction and GBS during diffusion creep, as well as the transition from dislocation creep to diffusion creep, is still unclear (Dimanov and Dresen, 2007; Kilian et al. 2011; Platt, 2015). And not all aspects are supported by available data. In recent high-temperature (>1200°C) experiments on two-phase material (olivine + pyroxene), it has been

shown that diffusion creep tends to aggregate phases because of its related component of GBS, promoting grain growth instead of grain size reduction (Hiraga et al., 2013).

In this study, we show new experimental results that document grain size reduction during diffusion creep in olivine at wet conditions of the uppermost mantle. The reduction can be understood in the presence of second phases, but not necessarily; we document it for both mono-phase (olivine) and two-phase (olivine + pyroxene) aggregates. In presence of pyroxene, strain localisation also goes along with grain size reduction and gives rise to typical ductile shear zones where complete phase mixing occurs. Both chemical and microstructural features suggest that grain size reduction results from fluid-assisted nucleation of olivine and pyroxene grains.

## **2. Material and methods**

### **2.1. Sample preparation**

In all experiments, we used olivine (Fo<sub>91</sub>) from San Carlos (Arizona, USA) and clinopyroxene (Wo<sub>51</sub>En<sub>48</sub>Fs<sub>1</sub>) from Cranberry lake (Canada). To produce the starting material, we crushed gem-quality single crystals in an agate mortar and sorted the grain size using a decantation method with distilled water. For olivine, we used a grain size ranging from 1 to 10  $\mu\text{m}$  with a mean of 2  $\mu\text{m}$  in all experiments. As for clinopyroxene (CPx), two types of grain sizes were used: one with fine CPx between 5 and 20  $\mu\text{m}$ , and a second one with coarser CPx grains between 40 and 125  $\mu\text{m}$ . Olivine and pyroxene powders were mixed at a ratio of 70 to 30% (by weight) in a solution of ethanol, following the procedure described in de Ronde et al. (2005). The powder was then placed between two alumina shear pistons cut at 45° to the piston axis, wrapped in a nickel foil and enclosed in a platinum jacket welded at both ends. The shear piston surfaces have been previously roughened using 120-grit corundum paper. Before welding, 0.1 or 0.2 wt.% of distilled water were added. These amounts exceed the solubility of water in olivine and pyroxene at our experimental conditions (Zhao et al., 2004; Bromiley et al., 2004). Such wet conditions and grain size have been chosen to ensure that (1) olivine will deform in the diffusion creep regime (Hirth and Kohlstedt, 2003; Sunderg and

Cooper, 2008; Hansen et al., 2011), and (2) initial grains will be large enough to see significant grain size reduction, if applicable. We also have chosen to use clinopyroxene – instead of orthopyroxene – to ensure that secondary phases will be stronger than the olivine matrix (Bürgman and Dresen, 2008). Few grains of orthopyroxene (enstatite; ~0.2 wt.%) and amphibole (tremolite; ~0.8 wt.%) were present in the CPx powder despite initial handpicking (fig.1).

## **2.2. Deformation experiments**

The deformation experiments were conducted in a solid medium (NaCl) Griggs-type apparatus at Tromsø University (Norway). Temperature and pressure were alternately increased over several hours up to the conditions of experiment (900°C and 1.2 GPa). Samples were hot-pressed *in situ* for 24h (microstructures of hot-pressed material are available in supplementary figure 1). The deformation piston ( $\sigma_1$ -piston) was then advanced at a constant rate, first through the top lead piece, and then touching the alumina piston (fig.1A). Samples started to deform at this point, several hours after starting to advance the  $\sigma_1$ -piston. At the end of the experiment, the samples were quenched from 900°C to 200°C in 2 minutes. Both, pressure and differential stress decreased rapidly until the temperature stabilised at 200°C. Subsequently, the sample was decompressed at a rate of ~5 MPa per minute, keeping the differential stress ~100 MPa above the confining pressure to reduce the formation of unloading cracks. Finally, temperature was dropped to 30°C when the confining pressure was lower than 100 MPa. After the experiment, the samples were impregnated with epoxy, and then sectioned along the piston axis for thin sections.

## **2.3. Analytical procedures**

Sample microstructures were analysed with a scanning electron microscope (SEM) of ISTO/BRGM (Orléans, France) and a transmission electron microscope (TEM) at the University of Minnesota (Minneapolis, USA). SEM work has been performed on carbon-coated (20 nm thickness) thin section using a TESCAN MIRA 3 XMU at 25 kV and a working distance of 25 mm. TEM images

were taken using a FEI-TECNAI T12 at 120 kV through a focused ion beam (FIB) foil of 50-100 nm thickness. In the TEM, Energy dispersive X-ray spectroscopy (EDS) was used to analyse phases. Electron backscatter diffraction (EBSD) was employed for Lattice Preferred Orientation (LPO) and grain size determination on polished surfaces (diamond paste of 0.25  $\mu\text{m}$  followed by colloidal silica) with an EDAX Pegasus system at 25 kV and a working distance of 18 mm. Lower-hemisphere pole figures of LPO were constructed considering both, the whole map dataset (available in supplementary figure 2) and one measurement per grain acquired manually. The data from EBSD maps have been processed with the OIM<sup>TM</sup> - EDAX software, and the grain size distributions are shown with respect to the percent area of each category in order to compare between sample types. For LPO, the texture (J) and misorientation (M) indices are also given, which both quantify the degree of minerals alignment between  $J = 1 / M = 0$  for a uniform distribution, and  $J = \infty / M = 1$  for a crystal-like distribution considering one point per grain (Bunge, 1982; Skemer et al., 2005). Phase composition, including starting material, was measured with an electron microprobe CAMECA SX five at ISTO on carbon-coated (20 nm thickness) thin sections at 15 keV and 10 nA. The step size of the microprobe map was 0.5  $\mu\text{m}$ .

To measure *in situ* water content of both olivine and pyroxene grains, we performed ion probe measurements on gold-coated (20 nm thickness) thin sections using a Cameca IMS 1280-HR at the CRPG (Nancy, France). A primary beam of  $\text{Cs}^+$  was used with a current of 3 nA and a beam diameter of 10  $\mu\text{m}$ . The positive secondary beam was centred in a 2500  $\mu\text{m}$  image field aperture. The voltage offset was stable at -50 eV and the energy window has been set to 20 eV. The counting elements were  $^{16}\text{O}$ ,  $^{17}\text{O}$ ,  $^{16}\text{OH}$ ,  $^{17}\text{OH}$ ,  $^{28}\text{Si}$  and  $^{30}\text{Si}$  with a counting time between 3s (for Si) and 12s (for OH). The total counting time was 12 minutes per point. To calibrate the ratio H/Si, we used the ratio  $\text{H}_2\text{O}/\text{SiO}_2$  from standards, including basaltic glass (M35, M40, M48, T1G, StHs, K12G), synthetic forsterite ( $\text{Fo}_{100}$ ), clinopyroxene (cpxNSH), pyrope (MON 9) and quartz (Suprasil). The very good quality of

vacuum into the chamber ( $6-7 \times 10^{-10}$  torr) indicated that no epoxy degassing occurred during the analyses.

### **3. Results**

#### **3.1. Mechanical data**

The strain-stress curves of all experiments show an increase of differential stress to peak stress at a bulk shear strain of  $\gamma \approx 1$  (fig.1B). While the peak stress of the pure olivine sample reaches ~550 MPa, the one of the two-phase samples ranges above 750 MPa. These data indicate stronger samples when CPx is present, in agreement with previous data for pyroxene strength (Dimanov and Dresen, 2007; Dimanov et al., 2007; Chen et al., 2006). Following the peak stress, the differential stress drops progressively toward a steady-state stress of around 300 MPa for both, the pure olivine sample and two-phase samples with fine-grained CPx. In contrast, from  $\gamma \approx 2.5$  onward, the sample with coarse-grained CPx stabilises at a steady-state stress of 700 MPa until the end of the experiment.

#### **3.2 Microstructures and composition**

The main difference between mono- and two-phase aggregates is the occurrence or absence of strain localisation. While the pure olivine sample shows homogeneous deformation (fig.1C and supplementary figure 3), the strain in composite samples is localised to different degrees depending on the initial grain size of CPx. In presence of coarse CPx (40-125  $\mu\text{m}$ ), strain is highly localised within a ~50  $\mu\text{m}$  wide shear zone, which is well developed on the sample side near the piston corner (fig.1D). In contrast, the presence of fine-grained CPx (~2  $\mu\text{m}$ ) by the same proportion (30/70 %) promoted strain to localise into a shear zone of ~150  $\mu\text{m}$  width all through the sample (fig.1E). Samples deformed to only peak stress conditions do not show significant deformation, so that it can



be inferred that strain localisation takes place from peak stress conditions onwards during weakening of the sample.

Furthermore, using the angle ( $\theta$ ) between the shear plane (piston interface) and foliation plane (long axis of CPx porphyroclasts), and the relationship:  $\gamma = 2 / \tan 2\theta$  (Ramsay, 1980), we have estimated the strain gradients in both types of composite samples. With coarse CPx, strain ranges from a minimum of  $\gamma \approx 0.2$  near the shear piston to  $\gamma \approx 0.5$  in the 50- $\mu\text{m}$ -thick localised shear zone (fig.1D). With fine CPx, strain reaches  $\gamma \approx 0.5$  in the 150- $\mu\text{m}$ -thick localised shear zone, but we also see the development of strain partitioning with typical shear bands parallel to the shear plane where strain is higher (fig.1E). Considering the amount of displacement accommodated by the bulk sample over the time of experiment from the peak stress onward (see supplementary table 1), i.e., considering plastic strain only, we can estimate a shear strain rate of  $\sim 10^{-4} \text{ s}^{-1}$  in the 50- $\mu\text{m}$ -thick shear band and  $\sim 5 \cdot 10^{-5} \text{ s}^{-1}$  in the 150- $\mu\text{m}$ -thick one.

The two-phase mixture that develops at olivine-pyroxene clast interfaces is of particular interest. This phase mixture mostly typically forms thin layers which extend from the tip or side of CPx grains through the olivine matrix (fig.1F-H). Strain is highly localised in these layers. In samples with fine-grained CPx, the mixture has a grain size lower than or equal to 1  $\mu\text{m}$ , and it occurs directly in contact with the porphyroclasts of CPx. In contrast, the coarse-grained CPx clasts develop inner tails that consist of 1 to 2  $\mu\text{m}$  sized grains of pure CPx (fig.1F). These inner tails are mantled by elongated tails of a two-phase, intimately-mixed material of olivine and CPx. TEM observations indicate a grain size of 0.1 to 0.2  $\mu\text{m}$  for all phases of the mixture, whereas the adjacent olivine matrix reveals a homogeneous grain size with equiaxed grains of  $\sim 1 \mu\text{m}$  (fig.2A-B). The fine-grained material consists of well-mixed olivine and clinopyroxene with a very few grains of enstatite. There are no dislocations in the layers of fine-grained mixture, but dislocations are present in the larger grains of the olivine matrix (fig.2B).

In addition, cracks occur in the olivine matrix (fig.2C) and at the high-stress sides of CPx clasts (fig.2D). While new grains of olivine are present in cracks of the olivine matrix (fig.2C), the

CPx cracks are filled with a fine-grained mixture of olivine + CPx. Most of these CPx cracks contain one or more fluid inclusions at their tip, highlighting the presence of a free fluid phase during deformation (fig.2E-F).

In terms of composition, the phase mixture is too fine grained to measure the composition of individual grains by the electron microprobe. As a consequence, the integrated measurements of the phase mixture have an intermediate composition which ranges between the two end-members of single-phase olivine and diopside, as shown in figures 3A and 3B. We do not see any chemical effect of the presence of enstatite, suggesting that enstatite grains result from local equilibrium. During deformation, the compositions of both, olivine and diopside, have shifted slightly with respect to the starting material in monomineralic domains: olivine becomes more magnesium-(Mg) rich, and CPx more iron (Fe)-rich (fig.3C and 3D). The calcium (Ca) content of CPx decreases slightly, whereas Ca in olivine records some enrichment (fig.3D). Analyses of individual grains in the TEM show a larger variation in olivine and CPx grains in the mixture compared to olivine in monomineralic layers (fig.3E). We attribute these compositional changes to element exchange that tends to locally equilibrate the olivine and pyroxene compositions at 900°C and 1.2 GPa.

### **3.3 H<sub>2</sub>O content**

The ion probe dataset documents water-rich olivine grains with  $\sim 157 \pm 44$  wt. ppm H<sub>2</sub>O and pyroxene grains with  $\sim 147 \pm 63$  wt. ppm H<sub>2</sub>O (table 1). Within error, these values correspond to the water solubility of olivine and pyroxene at 900°C and 1.2 GPa, which have been estimated at 155 and 150 wt. ppm H<sub>2</sub>O, respectively (Kohlstedt et al., 1996; Bell et al., 2003; Zhao et al., 2004; Bromiley et al., 2004). There is one exception of deformed CPx in the shear zone of composite samples where more than 400 wt. ppm H<sub>2</sub>O are recorded, possibly because of the presence of sub-microscopic fluid inclusions.

All analyses that include grain boundaries yield higher water contents, typically between 300 and 800 wt. ppm H<sub>2</sub>O. In specific areas, we also measured more than 900 wt. ppm H<sub>2</sub>O. This includes

1) the surrounding matrix of amphibole grains, and 2) the shear zones where the density of grain boundaries substantially increased because of grain size reduction (table 1). While the former indicates that amphibole grains released some water during experiment – tremolite is metastable at 900°C and 1.2 GPa (Jenkins, 1983) – the latter suggests that grain boundaries contain a significant amount of water. As suggested by the presence of fluid inclusions, our ion probe data confirms that deformation occurred in water-saturated conditions during the experiments.

### 3.4 Mineral LPO and grain size

The olivine LPOs presented here have been obtained from pure olivine layers only, regardless of the sample type. For composite samples, we focussed on olivine in shear zones. In the hot-pressed sample, the olivine LPO is nearly random with very low texture and misorientation indices of  $J = 1.48$  and  $M = 0.017$  (fig.4). With deformation, an olivine LPO starts to develop at peak stress conditions, and then moderately strengthens with increasing strain, except for the shear zone with  $\gamma > 10$  (coarse CPx) where no clear pattern of LPO is observed. In any case, the texture and misorientation indices remain extremely low and never exceed  $J = 2$  and  $M = 0.1$ , regardless of both, the finite strain and presence or absence of CPx (fig.4). In terms of geometry, the fabric has the [001] axis close to the shear direction and the [010] axis normal to the shear plane, typical of so-called B-type fabric (Jung and Karato, 2001).

Olivine grain size reduction occurs for both, mono-phase and two-phase aggregates, but only after the peak stress. Indeed, the grain sizes at peak stress conditions shows a log-scale distribution and remains unchanged with respect to the hot-pressed sample; we document a mean grain size of  $\sim 2 \mu\text{m}$  and a mode of  $\sim 3 \mu\text{m}$  for both samples (fig.5). In contrast, grain size has been significantly reduced to a mean and mode of  $\sim 1.5 \mu\text{m}$  in the pure olivine sample ( $\gamma = 2.5$ ) and in the shear zone of the two-phase samples with fine-grained CPx ( $\gamma > 5$ ). The shear zone with coarse-grained CPx ( $\gamma > 10$ ) even records a grain size reduction with a mean size and mode of  $1.1 \mu\text{m}$  (fig.5). Furthermore,

with increasing strain, there is an increase from 10 to 16% of the maximum area fractions, indicating that grain size becomes more uniform during deformation.

It is apparent in figure 6 that new olivine grains appear randomly distributed within the olivine matrix. Based on EBSD maps in combination with inverse pole figures (color coding with respect to the shear direction X), we show that the crystal orientation of small grains ( $< 1 \mu\text{m}$ ) differs from one grain to another, as well as from the neighbouring olivine porphyroclasts by at least 30 degrees (fig.6A). Thus, new olivine grains neither have any crystallographic relationship with one another nor with the larger ones. Furthermore, most of these small grains are isolated and dispersed randomly within the olivine matrix, and the amount of larger olivine grains ( $> 3 \mu\text{m}$ ) decreases with increasing strain. These large grains disappear entirely in the high-strain shear zone ( $\gamma > 10$ ), whereas the amount of grains smaller than  $1 \mu\text{m}$  significantly increases (fig.6B).

In samples with fine-grained CPx ( $\gamma > 5$ ), the new pyroxene grains occur as mixed with olivine and have a grain size lower than or equal to  $1 \mu\text{m}$ . They develop a weak LPO ( $J = 1.94$ ;  $M = 0.024$ ) with the [001] axis close to the shear direction and (010) plane within the shear plane (fig.6C). These observations are consistent with the fact that the fine-grained CPx grains do not have any crystallographic relationships with respect to each other (fig.6D). We did not see any tails of pure CPx in these samples. In contrast, the sample with coarse-grained CPx ( $\gamma > 10$ ) developed inner tails of CPx aggregates with a mean grain size around  $1.4 \mu\text{m}$ . They show a strong preferred orientation ( $J > 28$ ;  $M > 0.34$ ), which is directly related to the orientation of the starting porphyroclast (fig.6D). Thus, all grains composing a single tail in coarse CPx have a similar crystallographic orientation as

the starting CPx (fig.6F). Note that we do not document any LPO in layers of phase mixture that extend from these tails because the grain size was too small ( $\sim 0.1 \mu\text{m}$ ) to be indexed at the EBSD.

## **4. Discussion**

### **4.1. Phase mixing and nucleation**

In our experiments, the production of very fine-grained olivine-CPx mixture and high strain deformation typically are joint features. Moreover, our documentation of CPx cracks filled by a phase mixture (fig.2) provides a key evidence for understanding how the phase mixture forms. The crack filling consists of approximately equal proportions of very small Cpx and olivine grains. The local nature of this filling demonstrates that both, olivine and pyroxene, have nucleated together at the same time during opening of the cracks. The presence of fluid inclusions and our ion probe dataset also indicate that a fluid phase was present during deformation. And the geometry and orientation of cracks (mode 1 cracks) suggest that phase nucleation is connected to a local stress drop. We do not exclude that the crack geometry could also be crystallographically-controlled.

In these cracks, phase mixing cannot result from a two-stage-process involving first the formation of the small grains, and then a mixing process by, e.g., grain boundary sliding (GBS) as proposed by Farla et al. (2013) and Linckens et al. (2014). The nature of the local mixture also excludes dynamic recrystallization. Instead, it is likely that phase mixture formed by simultaneous nucleation of the two phases (fig.7), giving rise to filling of low-stress sites, where, once formed as a single-stage process, very small grain sizes are preserved because of grain boundary pinning. The presence of an aqueous fluid makes it likely that the two phases precipitated from a fluid. The same grain size and distribution of phases in mixture layers extending from the CPx porphyroclasts (fig.1) suggest that these layers result from the same fluid-assisted nucleation process as the crack fills.

The occurrence of fine-grained, intimately-mixed phases in two- or poly-phases material is commonly observed in the core of mantle shear zones, particularly where strain has been highly localised (Warren and Hirth, 2006; Toy et al., 2010; Drury et al., 2011; Linckens et al., 2014). The

source mechanism of this mixing remains very uncertain so far. As summarised in Platt (2015), recent field studies suggested that the GBS component of diffusion creep might account for it, but recent high-temperature deformation experiments of olivine + pyroxene aggregates in the diffusion creep regime do not support GBS as the source of mixing; grain neighbour switching helps to aggregate phases rather than disperse them (Hiraga et al., 2013).

According to different authors, phase mixing may be the result of solid-melt interactions (Dijkstra et al., 2002), or sub-solidus phase transformation (Newman et al., 1999; de Ronde et al., 2005). But the pressure-temperature conditions of our experiments exclude melting, and both, olivine and clinopyroxene, are stable in these conditions. As an alternative, the process of fluid-assisted nucleation we described above may account for some observed phase mixing in nature, particularly for low-temperature shear zones where dissolution-precipitation commonly occurs (e.g., Herwegh et al., 2011). We do not exclude either that chemical adjustment to local equilibrium – in combination with dissolution-precipitation – could be one of the driving potentials for nucleation.

#### **4.2. Olivine fabric and diffusion creep**

In our samples, the strength ( $J$  and  $M$  indices) of the B-type olivine fabric moderately increases up to  $\gamma > 5$  in olivine layers, but it remains very weak and the B-type fabric does not show up anymore at  $\gamma > 10$  (fig.4). In any case, we document extremely weak LPOs considering the amount of strain accommodated. For instance, one would expect  $J > 10$  and  $M > 0.3$  for a gamma strain higher than 3 (Hansen et al., 2014; Mainprice et al., 2015), whereas we never quantify higher than  $J = 2$  and  $M = 0.1$ , irrespective of the amount of finite strain.

While a strong LPO is typical of dominant dislocation creep (or disGBS; Hansen et al., 2012), a weak or absent LPO despite intense finite strain commonly indicates diffusion creep deformation (including GBS; Fliervoet et al., 1999; Drury et al., 2011; Herwegh et al., 2011). Furthermore, Sundberg and Cooper (2008) have shown that B-type fabric may occur during olivine diffusion creep, and especially in presence of (ortho)pyroxene. Based on numerical results (Bons and den Brok, 2000),

they attributed the B-type fabric to the GBS component of diffusion creep when accommodated by anisotropic lattice-controlled grain boundary migration. The recent experiments of Miyazaki et al. (2013) on olivine diffusion creep further support this point. In our samples, the presence of very weak B-type fabric is therefore consistent with olivine deforming by diffusion creep in combination with GBS. Again, it should be noted that the weak LPO forms in pure olivine aggregates and not in mixture layers, where the grain size was too small ( $< 0.2 \mu\text{m}$ ) to be indexed at the EBSD. It is also probable that fine-grained CPx deformed by diffusion creep based on their weak LPO (fig.6C). In contrast, the strong, host-controlled LPO of the inner tails of CPx involves dominant dislocation creep and related dynamic recrystallization, probably by sub-grain rotation.

### **4.3. Grain size reduction**

In this study, we document grain size reduction after peak stress during substantial weakening of the sample strength (fig.5). This reduction occurs for olivine and CPx grains in both, mono-phase and two-phase aggregates. Based on the strong LPO, we inferred grain size to be reduced by dynamic recrystallization in the inner parts of large CPx tails (figs.2 and 6). However, dynamic recrystallization did not produce the very fine-grained mixture of olivine and CPx. And we inferred from our microstructural features that the phase mixture results from nucleation, probably fluid-assisted.

In addition, based on available flow laws for wet olivine (Hirth and Kohlstedt, 2003; Hansen et al., 2011), we show that grain size reduction of the pure olivine sample took place in the diffusion creep field along the strain rate isolines. The olivine grain size of both, pure olivine layers and mixture layers, in the two-phase samples also falls within the diffusion creep field, which supports again dominant diffusion creep for olivine (fig.8). In all cases, grain size reduction occurred below the experimentally calibrated olivine piezometer (Van der Wal et al., 1993), which defines the stress-grain size relationships for dynamically recrystallized grains as dictated by the rate of mechanical work (Austin and Evans, 2007). Even if we consider the occurrence of bulging (Platt and Behr, 2011),

the mean grain size of deformed olivine aggregates stands below the minimum size of bulge (dotted line in fig.8). Thus, dynamic recrystallization has not contributed in reducing olivine grain size. As a possible alternative, Zener pinning is effective in maintaining the small size of grains in mixed layers. This mechanism has been proposed as potentially able to reduce grain size below the piezometer (Bercovici and Ricard, 2012). However, in absence of pyroxene grains in the olivine matrix (the non-mixed parts), and of course, for the pure olivine sample, a mechanism other than Zener pinning is required.

#### **4.4. Creep cavitation as a potential origin for grain size reduction**

During dominant diffusion creep, the deformation of poly-crystalline material involves a component of grain boundary sliding (GBS; e.g., Langdon, 2006). If crystal-plastic or diffusional mass transport processes cannot accommodate the local sliding of grains fast enough, GBS may lead to the formation of micro-cavities which open (and may close again), giving rise to a process termed creep cavitation (Kassner and Hayes, 2003; Dimanov et al., 2007). In nature, this mechanism is coeval with phase nucleation resulting from dissolution-precipitation (Fusseis et al., 2009; Kilian et al., 2011; Herwegh et al., 2011). Such a nucleation process is a viable mechanism for reducing grain size in the diffusion creep domain and will depend on the solubility of rock components. Based on our evidence of nucleation in micro-cracks, we therefore propose that grain refinement has occurred in pure olivine layers by nucleation in sites produced by creep cavitation.

In this view, nucleation in dilatant sites is expected to yield small, randomly oriented grains, which may subsequently grow at the expense of the old ones with a preferred orientation, reducing grain size and randomising the mineral LPO (fig.9A). The small size of these new grains assures the operation of GBS as their dominant deformation mechanism. If the nucleation rate is high enough, GBS does not produce any LPO, because the grains are continuously renewed with random orientations. In contrast, at moderate or low nucleation rates, the new grains do not sufficiently decrease the pre-existing fabric, giving rise to a preferred orientation (e.g., B-type fabric), the strength



of which depends on the nucleation rate. Such a nucleation model accounts for (1) grain size reduction within the diffusion creep field, (2) the dispersion of new olivine grains within the olivine matrix, (3) the absence or weak LPO despite high strain deformation, and (4) the occurrence of phase mixing at phase interfaces (fig.9B). This process is relatively easy to detect if nucleation of mixed phases occurs (e.g., Kilian et al., 2011; Platt, 2015), but in the case of a single-phase aggregate with the same phase nucleating, it is more difficult and requires at least a LPO analysis.

#### **4.5. Implications for strain localisation**

The nucleation of new grains as a process of grain size reduction during dominant diffusion creep highlights a potentially important source for weakening and strain localisation, provided that grain size reduction is locally enhanced. In our experiments, strain only localises in two-phase aggregates where strong and locally cracked CPx clasts are present. The occurrence of mode-1-cracks at the rim of CPx porphyroclasts suggests that stress locally increased during deformation. As shown during creep cavitation of metals, micro-cavities form most easily at sites of higher stresses (Kassner and Hayes, 2003). Thus, it is likely that the pure olivine matrix adjacent to CPx porphyroclasts suffered more creep cavitation and phase nucleation, enhancing grain size reduction (fig.9C). This would promote local weakening and subsequent strain localisation within the olivine matrix. We also envisage that strain localisation propagates because of stress concentration (shear stress) and related creep cavitation at the tip of the incipient shear zone (fig.9C).

The absence of strain localisation in pure olivine aggregates may be caused by the fact that strong CPx clasts as stress raisers are absent and creep cavitation may be homogeneous. Furthermore, a different degree of strain localisation, i.e. a wide shear zone instead of a narrow shear zone, is expected when there are more weakening areas, i.e., more olivine/CPx interfaces (finer-grained CPx

produces more cavitation sites giving rise to a larger volume of weaker material and thus a wider zone).

This process provides a consistent approach to answer for strain localisation during olivine diffusion creep, with crucial implications for the lithosphere dynamics. For instance, recent quantifications of silicon diffusion in olivine (Fei et al., 2016) have predicted grain-boundary diffusion creep (cobble creep) to be dominant – at the expense of dislocation creep – in the whole uppermost mantle. Moreover, numerical models of upper mantle convections have shown that strain localisation induced by grain size reduction during olivine diffusion creep have a great potential in promoting plate boundaries, which is a *sine qua non* condition for Plate Tectonics to originate (Bercovici and Ricard, 2014). We stress nevertheless that the nature of phase nucleation during diffusion creep remains an open question, particularly for mono-phase aggregates. The processes controlling grain size equilibrium within the diffusion creep field also remain very elusive. Defining an equilibrium grain size as a function of deformation parameters is indeed critical to quantify strain localisation in the lithospheric mantle, and hence, to better constrain its implications for the lithosphere dynamics.

## **Conclusion**

In this study, we performed Griggs-type deformation experiments on pure olivine and composite (olivine + diopside) aggregates with 0.1-0.2 wt% H<sub>2</sub>O at 900°C and 1.2 GPa. Starting with a mean grain size of 2 µm for olivine, we explored how diffusion creep may be important for grain size reduction and strain localisation in the wet uppermost mantle. While we document olivine grain size reduction and a substantial weakening for all sample types, we develop typical ductile shear zones for two-phase samples. Strain localisation is coeval with complete phase mixing of olivine and CPx in very fine-grained layers that extend from CPx porphyroclasts. The phase mixture is also found as mantling CPx tails with strong LPO, as well as in cracks of large CPx with fluid inclusions. For

olivine aggregates, we further document (1) some cracks containing new grains, and (2) absent or very weak LPO (B-type fabric) despite substantial finite strain.

While phase mixing is inferred to form by nucleation of two-phase aggregates at olivine/pyroxene interfaces, both, olivine grain size reduction and strain localisation are proposed to arise from creep cavitation induced by grain boundary sliding and subsequent fluid-assisted nucleation. These findings provide a key source for strain localisation in the uppermost mantle, including at the scale of the lithosphere. We therefore emphasize creep cavitation and diffusion creep to be considered in future studies investigating on the consequences of strain localisation for the lithosphere.

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## Table and figures captions

**Table 1 | Sample water content** – Post-experiment water content of the olivine matrix and single crystals (in wt. ppm of H<sub>2</sub>O) in the hot-pressed, peak stress, pure olivine and composites samples. The measurements have been performed using ion probe at the CRPG (Nancy, France) on gold-coated thin section (see text for analytical conditions). The terms “amph.” and “SZ” refer to a measurement taken by an amphibole grain or within the high-strain shear zone, respectively.

**Figure 1 | Sample assembly, strain-stress curves and microstructures.** **A)** Sample assembly in the Griggs-type apparatus. WC = Tungsten carbide; Pt = Platinum;  $\sigma_1$  = deformation piston;  $\sigma_3$  = confining piston. **B)** Differential stress (MPa) versus shear strain ( $\gamma$ ) that shows the mechanical behaviour of a pure olivine sample (green), two composite samples with 30 wt.% of fine-grained (5-20  $\mu\text{m}$ ) CPx (light blue), and two composite samples, including a “peak-stress” experiment, with 30 wt.% of coarse-grained (40-125  $\mu\text{m}$ ) CPx (purple). For all experiments, the olivine grain size is between 1 and 10  $\mu\text{m}$ , and the temperature, confining pressure and bulk strain rate are set to 900°C, 1.2 GPa, and  $\sim 3 \cdot 10^{-5} \text{ s}^{-1}$ , respectively. **C)** SEM image (Back-Scatter Electron (BSE) image) of the pure olivine sample. The analytical conditions are described in the text. **D)** BSE image of the composite sample with coarse-grained CPx. Strain localisation occurred near the bottom side within a shear zone of  $\sim 50 \mu\text{m}$  width. **E)** BSE image of one two-phase sample with fine-grained CPx. The second experiment shows the same microstructure. Strain localised within a shear zone of  $\sim 150 \mu\text{m}$  width



where shear bands have been developed. For both sample types (with fine vs. coarse CPx), we also give an estimation of the finite strain ( $\gamma$ ) involved at the right of each picture based on the angle ( $\theta$ ) between the long axis of CPx (dotted lines) and shear plane (piston side).  $\gamma = 2 / \tan 2\theta$  (Ramsay, 1980). **From F to H**) BSE images of the bi-phase deformation product (mixture) that extends from starting CPx. The mixture of CPx + Ol also rims pure CPx aggregates.

**Figure 2 | Phase mixture and cracking. From A to C)** TEM images (bright field) through Focused Ion Beam (FIB) section of a mixture layer (A) and adjacent olivine matrix (B) in the shear zone of the composite sample with coarse-grained CPx. In the matrix, a few dislocations (B) and some cracks with new olivine grain (C) have been observed. **D)** BSE image of cracks filled by two-phase mixture at the rim of large pyroxene grains. These cracks only develop in the direction of maximum normal stress. **E and F)** Observations at the polarized optical microscope and SEM (BSE) image of fluid inclusions at the tip of CPx cracks. Ol = olivine; CPx = clinopyroxene.

**Figure 3 | Composition of the starting material and deformation product. A)** Element map (microprobe) of the magnesium distribution in the shear zone of the sample with coarse-grained CPx. The location is shown in figure 1D. The color scale refers to point counting of elements. **From B to D)** Microprobe analyses that document the Magnesium (Mg), Calcium (Ca) and Iron (Fe) contents (per unit of structural formulae normalised for 4 cations) of olivine (green squares), CPx (light blue squares) and mixture (red squares) in the same area. We also show spot analyses of the starting material, including olivine and diopside (black squares).  $Mg\# = Mg/(Mg + Fe)$ . We only give an overall composition of the mixture because its grain size ( $\sim 0.1 \mu m$ ) is one order of magnitude below the spot size ( $\sim 1 \mu m$ ) of the microprobe beam. Thus, several grains of the mixture are measured in one measurement. The mixture composition extends from the changed composition of olivine and CPx grains, indicating that (1) olivine and CPx compose the mixture, and (2) starting olivine and CPx grains equilibrated at  $900^\circ C$  and  $1.2 GPa$  (best seen in D). **E)** Chemical analyses of olivine and pyroxene grains in the phase mixture using EDX at the TEM. The graph axes refer to the Mg# and

Si/Mg ratio based on point counting. While the element contents are consistent with olivine and diopside as composing the mixture, they show some variations that we attribute to local equilibrium (see text).

**Figure 4 | Olivine Lattice Preferred Orientation (LPO).** From top to bottom, we document the olivine LPO after hot-pressing ( $\gamma = 0$ ), at peak stress conditions ( $\gamma = 1$ ), after deformation of the pure olivine sample ( $\gamma = 2.5$ ), and within the shear zones of the two-phase samples with fine-grained CPx ( $\gamma > 5$ ) and coarse-grained CPx ( $\gamma > 10$ ). The LPOs are shown in lower-hemisphere pole figures of the three reference axes for orthorhombic olivine ([100], [010] and [001]) with respect to the shear direction (white dot) and shear plane (horizontal solid line). The contours and grey shading highlight multiples of uniform distribution. These LPO includes one point per grain acquired manually (the map-based LPOs are available in supplementary figure 2). N = number of data; J = texture index (Bunge, 1982); M = misorientation index (Skemer et al., 2005).

**Figure 5 | Olivine grain size distribution.** Histograms of grain size diameter ( $\mu\text{m}$ ) versus area fraction (%) for each category of olivine grain size. The grain sizes have been calculated based on EBSD maps shown in figure 6 and using area-equivalent diameter. The threshold angle of misorientation to define grain boundaries was  $10^\circ$ . The step size was  $0.3 \mu\text{m}$ , except for the sample with  $\gamma > 10$  where we used a step size of  $0.2 \mu\text{m}$ . From top to bottom, we show the grain size distribution of a hot-pressed sample (which includes 30 wt.% of fine-grained CPx), a sample quenched at peak stress conditions (which includes 30 wt.% of coarse-grained CPx), and the final grain size distribution for the pure olivine sample, two-phase sample with fine-grained CPx and two-phase sample with coarse-grained CPx. The data for deformed two-phase samples have been acquired within their respective shear zones. Both the mean (red line) and mode (orange line) show a grain size reduction (black arrow) from the peak stress onward. N = number of olivine grains.

**Figure 6 | Spatial distribution and pyroxene LPOs.** A) EBSD maps combined with inverse pole figures (IPF; bottom left) of olivine LPO within the pure olivine sample ( $A_1$ ), the shear zone of one two-phase sample with fine-grained CPx ( $A_2$ ), and the one with coarse-grained CPx ( $A_3$ ). The color coding refers to the angle (between  $0$  and  $90^\circ$ ) of each axis with respect to the shear direction (X). The step size is  $0.3 \mu\text{m}$  for all maps, except for the sample with  $\gamma > 10$  ( $A_3$ ) where we used a step size of  $0.2 \mu\text{m}$ . We give the maximum finite strain ( $\gamma$ ) for indication. Grain boundaries are defined considering misorientation angles higher than  $10^\circ$ . The black

areas are CPx grains and non-indexed points. **B)** Map-related distribution of olivine grain size for the pure olivine ( $B_1$ ) and composite samples with fine- ( $B_2$ ) and coarse-grained ( $B_3$ ) CPx. We considered three categories of grain size: below 1  $\mu\text{m}$  (red), between 1 and 3  $\mu\text{m}$  (green), and above 3  $\mu\text{m}$  (grey). **C and D)** LPO (C) and EBSD map (D) combined with IPF of pyroxene grains in the shear zone of a sample with fine-grained CPx. The location is shown in figure 6A<sub>2</sub>. **E and F)** LPO (E) and EBSD map (F) combined with IPF of pyroxene tails in the shear zone of a sample with coarse-grained CPx. LPOs are shown for the (100) plane, (010) plane and [001] axis of diopside with respect to the shear direction (white dot) and shear plane (horizontal solid line) considering one point per grain ( $N$  = number of grain). Contours and grey shading are multiples of uniform distribution.  $J$  = texture index;  $M$  = misorientation index. For coarse-grained CPx (F), we also show a second EBSD map with randomly attributed color for each grain, highlighting the grain size distribution in CPx tails.

**Figure 7 | Mechanism of crack healing by phase mixture.** A crack first opens in the direction of maximum normal stress ( $\sigma_1$ ), promoting pumping of the surrounding fluid from the grain boundary. The fluid solute (mixture) precipitates because of stress drop in the opening crack where a part of fluid is trapped (fluid inclusions).

**Figure 8 | Deformation mechanism map (DMM) for wet olivine at 900°C and 1.2 GPa.** DMM predicts the strain rate and dominant deformation mechanism, i.e., dislocation creep vs. diffusion creep, as a function of differential stress and mean grain size for olivine. On this DMM, we plot the deformation conditions (stress and grain size) at peak stress and after deformation ( $\gamma = 2.5$ ) of the pure olivine sample (green squares), as well as conditions after deformation of the two-phase samples with fine- ( $\gamma > 5$ ; light blue square) and coarse-grained CPx ( $\gamma > 10$ ; purple square), including the mixtures. The DMM has been constructed after flow laws from Hirth and Kohlstedt (2003) using a water concentration of 1000 ppm and applying the correction for diffusion creep of Hansen et al. (2011). The olivine piezometer (yellow line) defines the stress-grain size relationships for dynamically recrystallized grains (Van der Wal et al., 1993). The dotted yellow line defines the minimum size of bulge for olivine (Platt and Behr, 2011). For the pure olivine sample, we highlight substantial weakening within the diffusion creep field and below both, the olivine piezometer and minimum size of bulge (black arrow).

**Figure 9 | Model of fluid-assisted nucleation and strain localisation during diffusion creep. A)**

Nucleation induced by creep cavitation during plastic deformation of an olivine aggregate (green), including intra-crystalline deformation (diffusion creep) and grain boundary sliding (GBS). As a consequence of GBS, some cavities are formed and instantaneously filled by precipitation of new olivine grains (red). These new, randomly oriented grains then grow at the expense of the old ones while the olivine aggregate keeps deforming.

**B)** Sketches that illustrate the formation of phase mixture at olivine (green)-pyroxene (light blue) interfaces because of GBS-related creep cavitation and dissolution-precipitation (solution transfer) during diffusion creep (modified after Kassner and Hayes, 2003). The olivine-pyroxene mixture (yellow) forms by (1) dissolution of the olivine and pyroxene components at stressed interfaces, i.e., normal to the maximum stress ( $\sigma_1$ ), and then (2) precipitation of the fluid solute in low-stress sites produced by GBS. **C)** Creep cavitation as a source for strain localisation. Because of stress concentrations (color scale) at pyroxene boundaries that stand at high angle to the direction of  $\sigma_1$ , creep cavitation and related nucleation are locally enhanced in the olivine matrix, which weakens and starts localising strain owing to grain size reduction. Due to shear stress concentrations at the tip of the shear zone, the shear plane propagates into the olivine matrix. While solution transfer produces the olivine-pyroxene mixture, the tails of pure CPx are produced by dynamic recrystallization. CPx = clinopyroxene.

Figure 1

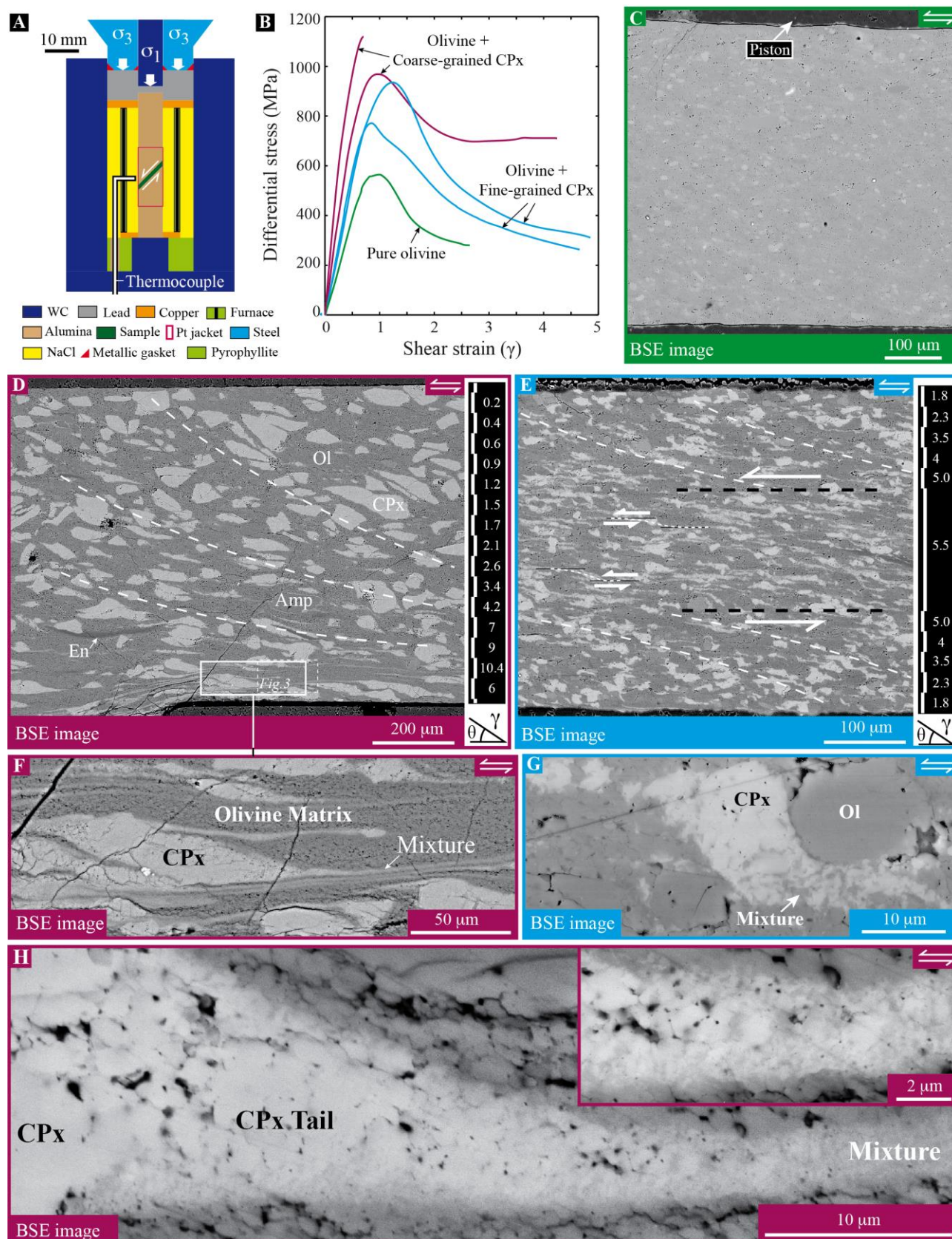




Figure 2

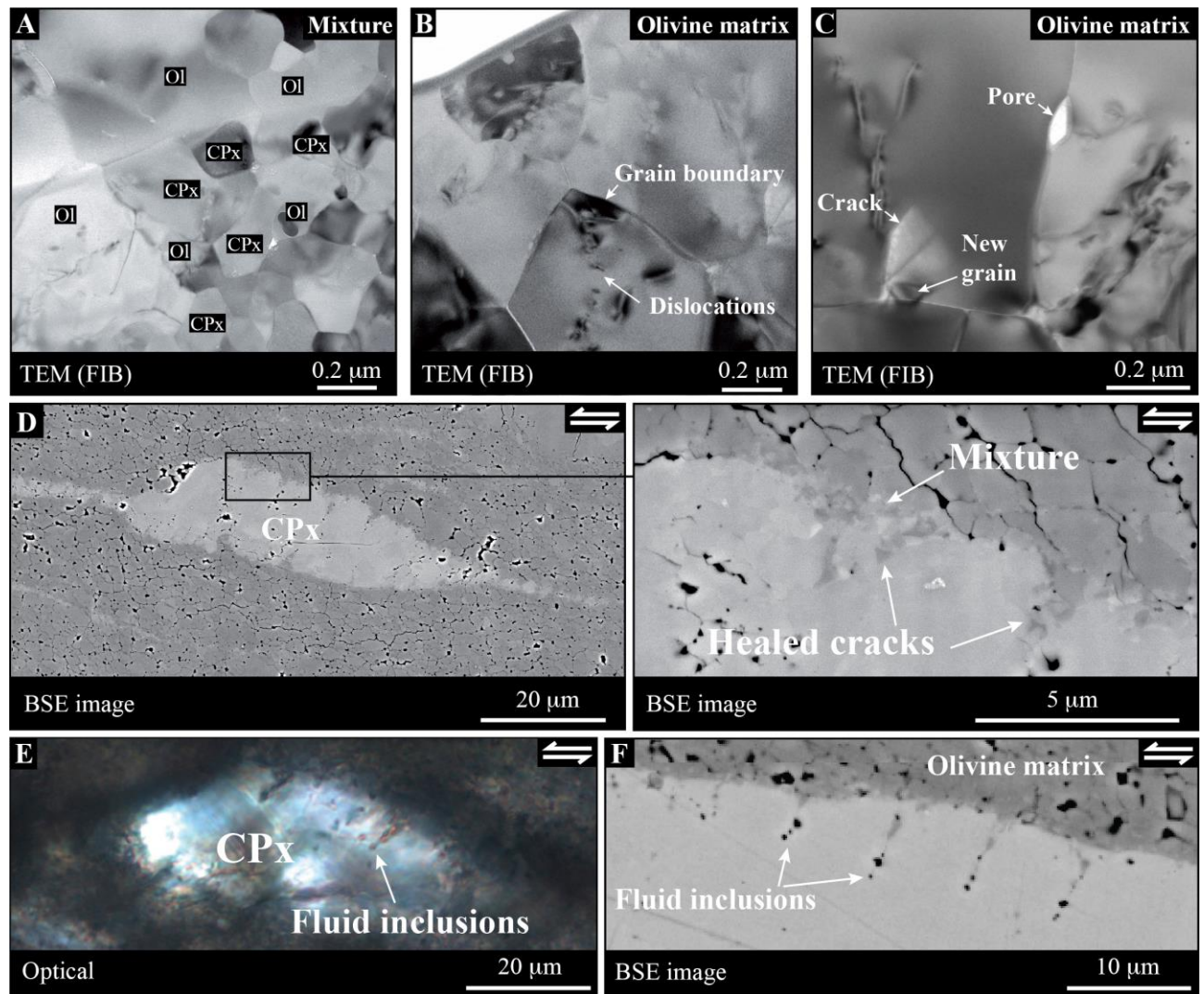


Figure 3

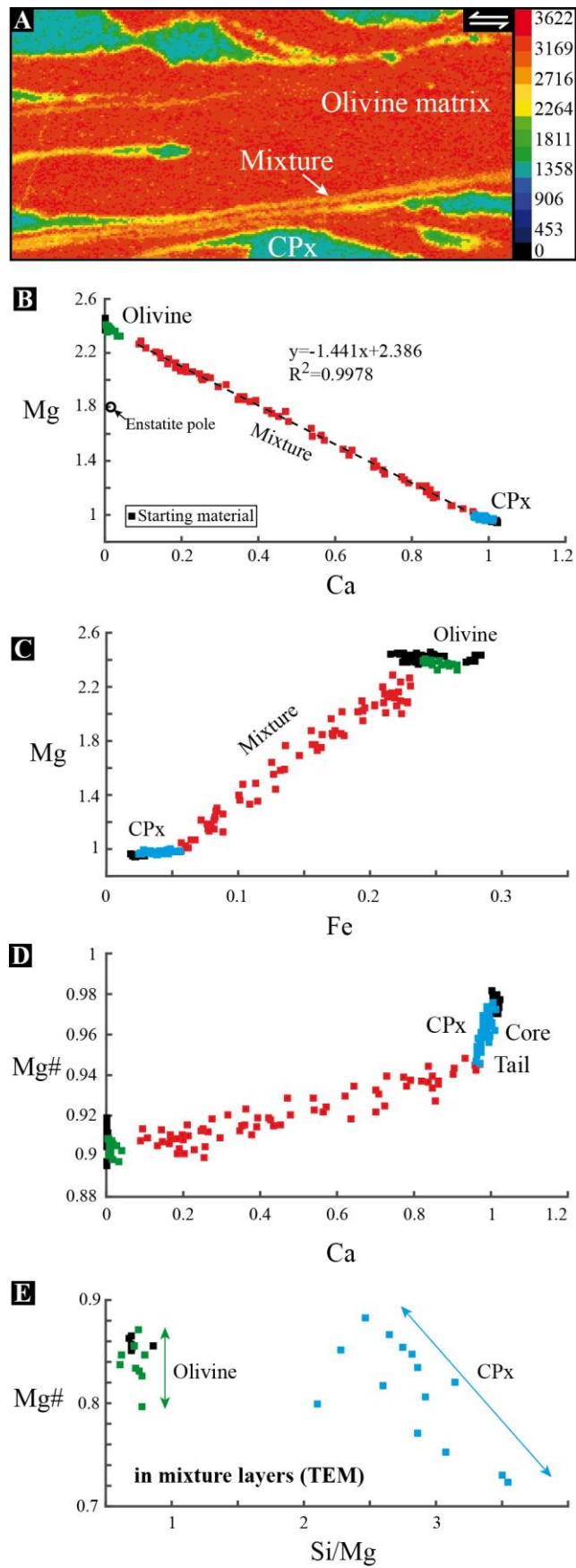


Figure 4

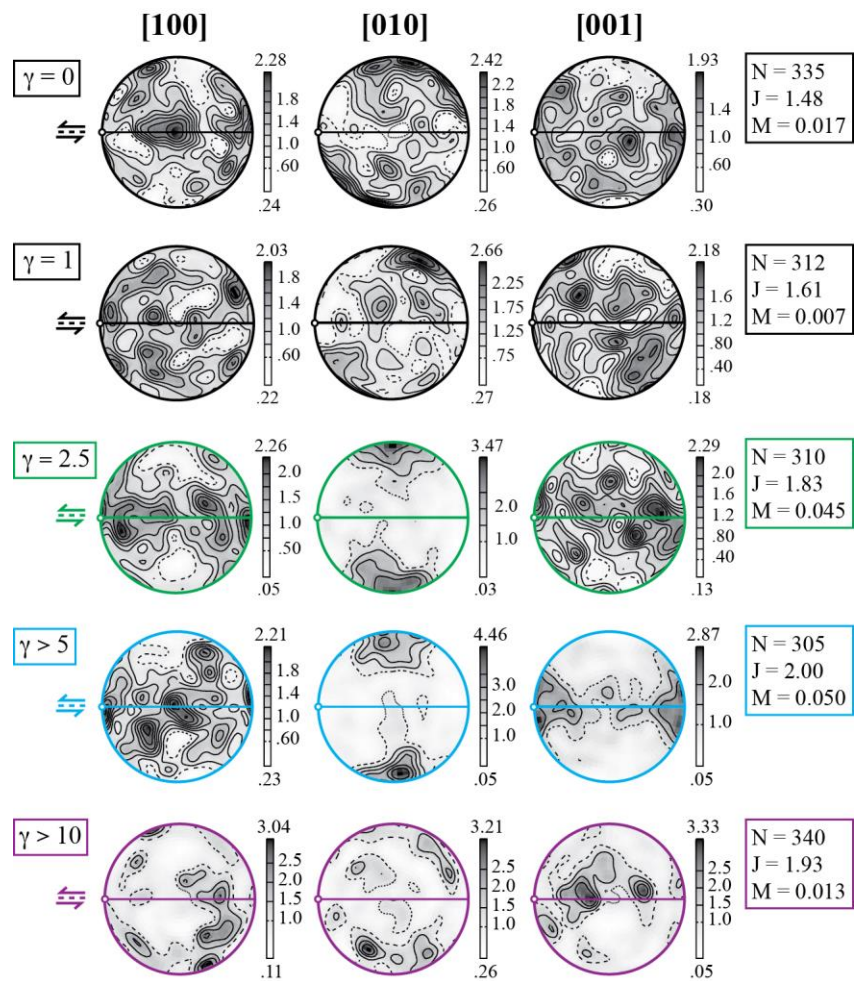




Figure 5

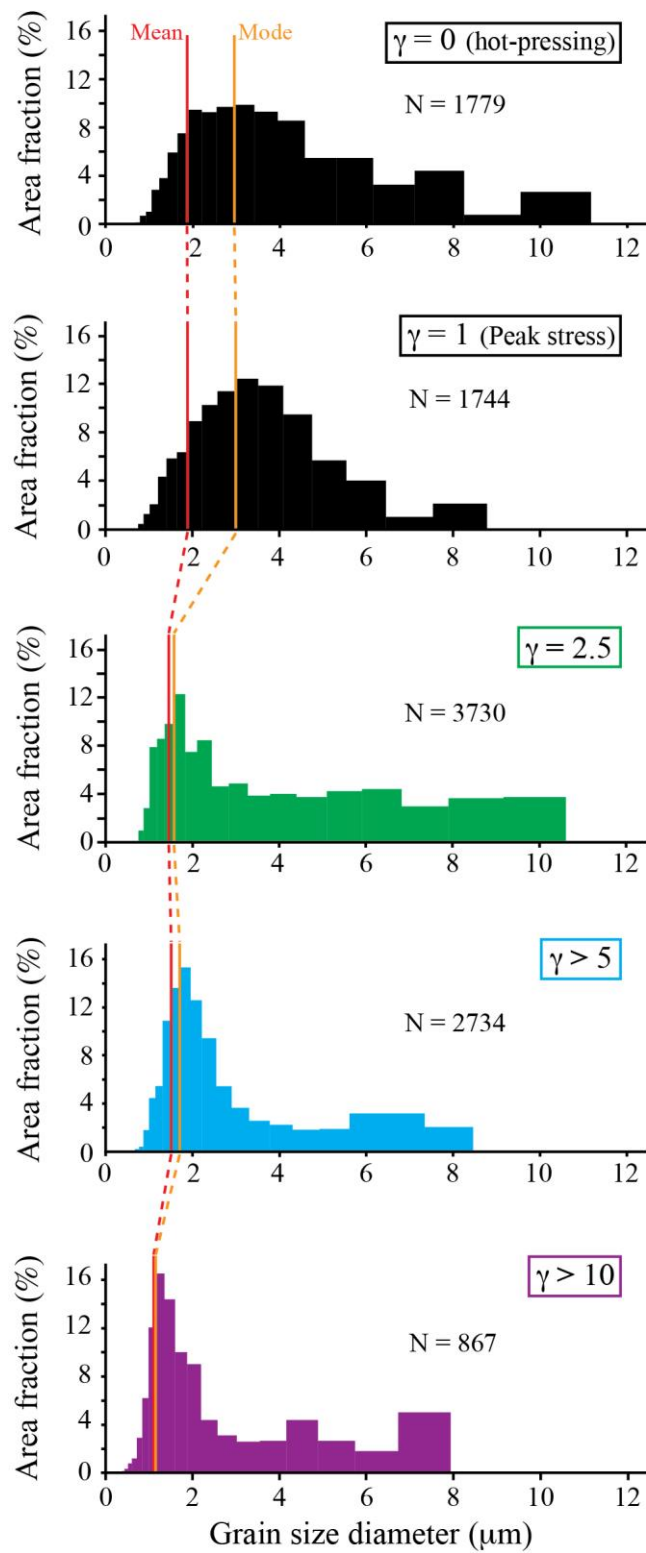


Figure 6

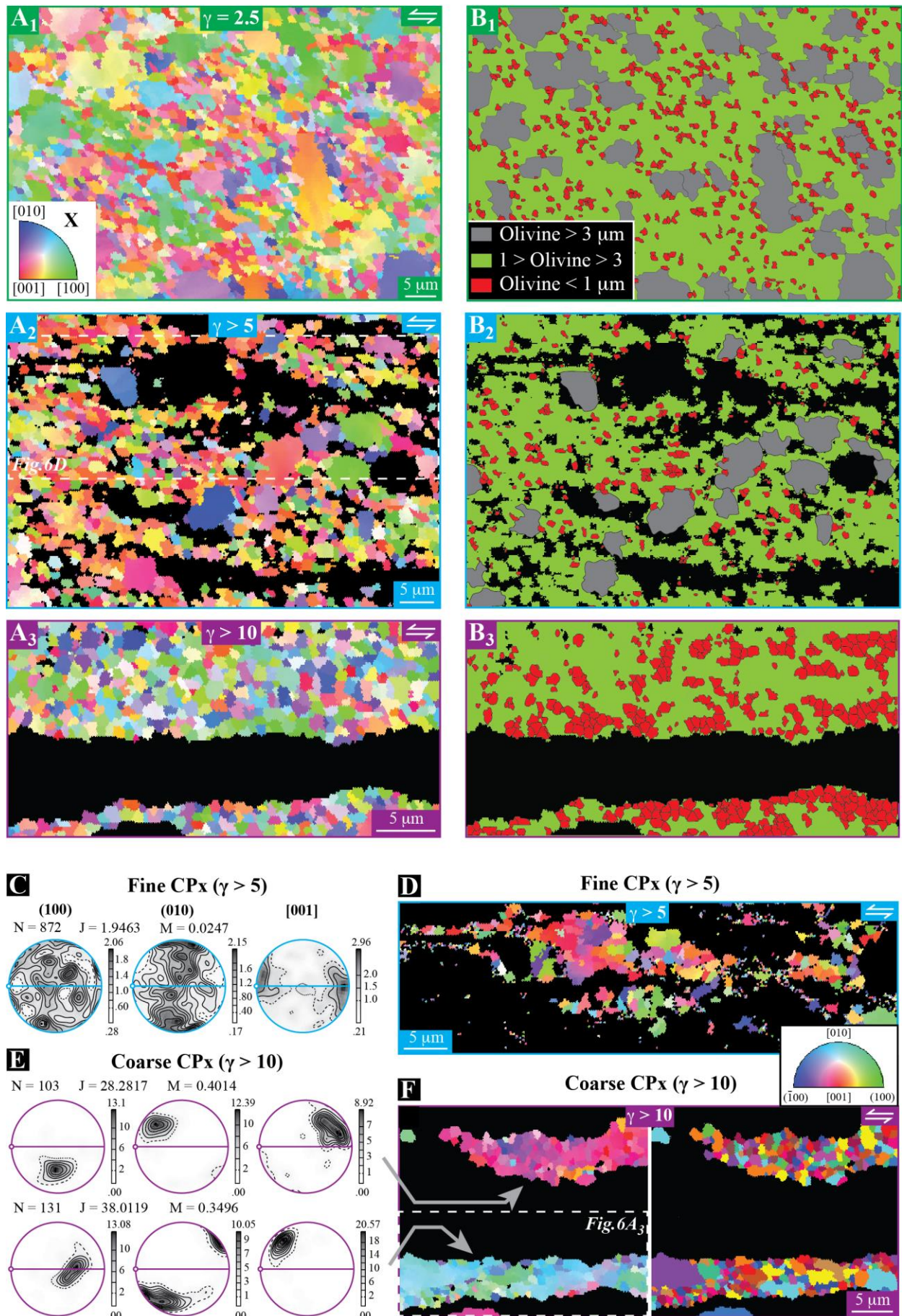


Figure 7

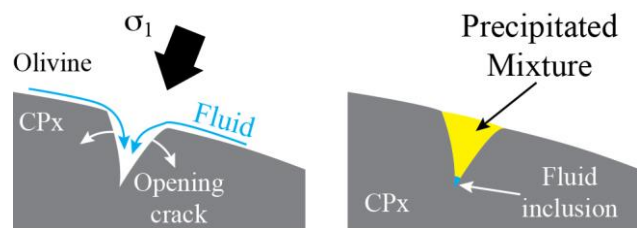






Figure 9

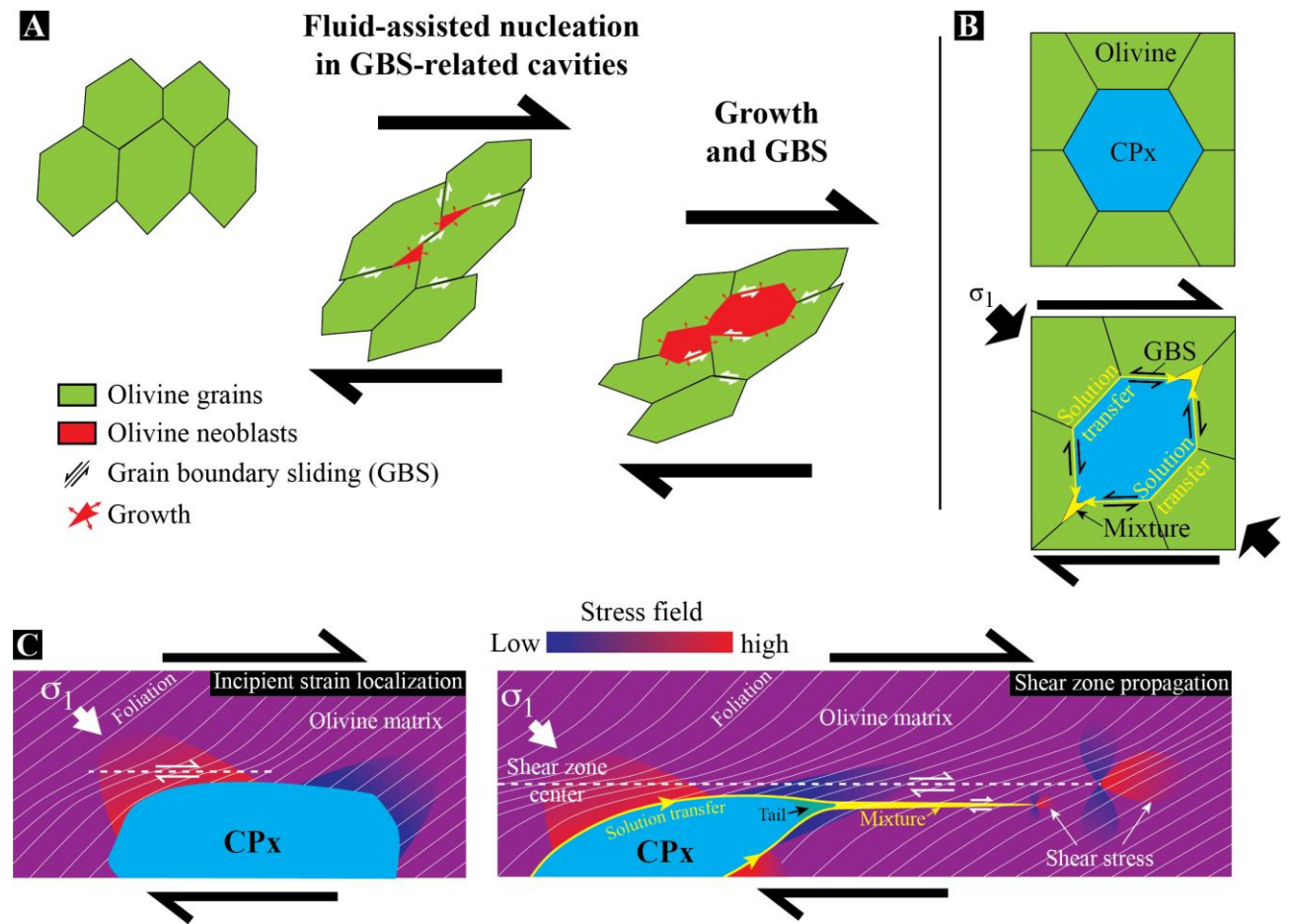


Table 1

<b>Sample</b> <b>Water content</b> <b>(wt. ppm H<sub>2</sub>O)</b>	<b>Hot-pressing</b>	<b>Peak stress</b>	<b>Pure olivine</b>	<b>Two-phase</b> <b>(fine-grained</b> <b>CPx)</b>	<b>Two-phase</b> <b>(coarse-grained</b> <b>CPx)</b>
<b>Olivine matrix</b>	597.2 ± 76 532.26 ± 68 532.15 ± 60 459.62 ± 48 505.29 ± 50 729.38 ± 55 (amph.) 347.53 ± 478 306.44 ± 54	684.26 ± 54 935.09 ± 49 (amph.) 693.32 ± 61	370.09 ± 47 526.20 ± 55 368.08 ± 47 461.07 ± 49 424.32 ± 64	707.94 ± 48 396.15 ± 49 479.78 ± 497 509.05 ± 46 614.57 ± 50 912.9 ± 52 (amph.) 773.23 ± 60 476.21 ± 49 786.47 ± 83 474.63 ± 48 546.59 ± 59 649.04 ± 59	421.28 445.48 442.37 528.25 544.00 1115.43 (amph.) 1009.8 (amph.) 824.74 661.00 1034.74 (SZ) 1156.76 (SZ) 1283.67 (SZ)
<b>Single olivine grain</b>				157.25 ± 44	
<b>Single CPx grain</b>	148.85 ± 61 147.48 ± 61 209.57 ± 63 317.81 ± 67 184.64 ± 63 244.31 ± 62	160.55 ± 64 150.00 ± 62 314.47 ± 64 129.6 ± 61	684.26 ± 54 935.09 ± 49 (amph.) 693.32 ± 61	166.60 ± 45	436.66 ± 72 (SZ) 648.1 ± 78 (SZ) 477.89 ± 64 (SZ) 473.51 ± 126 (SZ)