

Emplacement of metamorphic core complexes and associated geothermal systems controlled by slab dynamics

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| 32 33 34 | https://doi.org/10.1016/j.eps1.2018.06.043 |
| 35 | ABSTRACT |
| 36 | Slab rollback results in the development of low-angle normal faults (detachments) and |
| 37 | metamorphic core complexes (MCCs) in back-arc domains. Although the mechanical |
| 38 | consequences of slab dynamics on lithospheric and crustal behaviors have already been studied, |

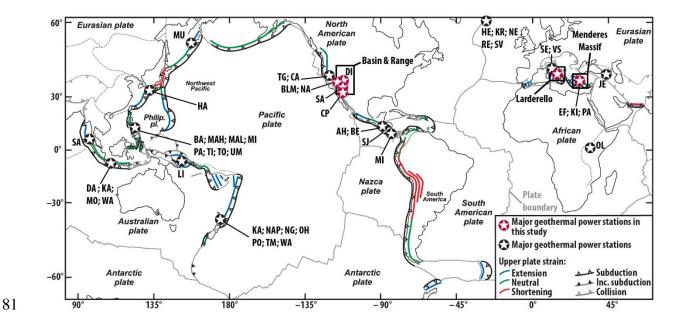
39 thermal effects have not been investigated yet. This study shows that slab rollback produces 40 lithospheric-scale thermal perturbations intrinsically associated with emplacement of amagmatic 41 high-enthalpy geothermal systems. Using a multi-scale numerical modeling approach, with 42 lithospheric-scale 3-D thermo-mechanical models of subduction, and 2-D models of fluid flow 43 at the scale of detachments, we demonstrate that subduction-induced extensional tectonics 44 controls the genesis and distribution of crustal-scale thermal domes from the base of the crust, 45 and the location of high-energy geothermal systems. We find that when slab tearing occurs, Moho 46 temperatures can temporarily increase by up to 250 °C due to significant shear heating in the 47 flowing upper mantle. Associated thermal anomalies (with characteristic width and spacing of 48 tens and hundreds of km, for crustal and lithospheric scales, respectively) then migrate 49 systematically toward the retreating trench. These thermal domes weaken the crust, localize 50 deformation and enhance the development of crustal-scale detachments. These thermo-51 mechanical instabilities mimic genesis of high-temperature MCCs with migmatitic cores in the 52 back-arc domain, such as those of the Menderes (western Anatolia, Turkey) and Larderello 53 (southern Tuscany) provinces in the Mediterranean realm, and those in the Basin and Range 54 (western United States), where detachments control the bulk of the heat transport. At the scale of 55 MCCs, the bulk fluid flow pattern is controlled by topography-driven flow while buoyancy-56 driven flow dominates within the permeable detachments, focusing reservoir location of high-57 energy geothermal systems at shallow depth beneath the detachments.

58

59 1. INTRODUCTION

60 The development of geothermal power plants has been increasing since the 1970s,61 building upon more than 100 years of history in geothermal energy extraction. Currently, the

62 installed global capacity is estimated at 12.6 GWe (Gigawatt electrical), and forecasts for 2050 63 point to a worldwide capacity of 140 GWe, approximately 8.3% of total world electricity 64 production (Bertani, 2016). Many of the high enthalpy geothermal resources (HEGRs) that make 65 such an ambitious goal possible are located in the vicinity of subduction zones and volcanic arcs, 66 where both magmatic and tectonic processes operate (Fig. 1). Others are located in "amagmatic" 67 provinces such as the Menderes Massif in Western Turkey and the Basin and Range in the 68 Western United States. Particularly noteworthy for this study is that while geothermal systems 69 associated with magmatism have been studied in detail (e.g. Cumming, 2009) those located in 70 "amagmatic" provinces have received less attention (Moeck et al., 2014; Roche et al. submitted). 71 Recent to present (i.e. Pliocene-Quaternary) magmatism in the upper crust across the 72 Menderes Massif and the Basin and Range is rare (Blackwell et al., 2009; Faulds et al., 2010) 73 compared to that of the Larderello geothermal field, located in the southern Tuscany (i.e. Italy) 74 (Santilano et al., 2015) (Fig. 1). Open discussions on the possible role of hidden magmatic 75 intrusions on these geothermal systems remains debated. Even if present, however, magmatic 76 intrusions alone cannot explain the extent of these geothermal provinces (several thousand km² 77 each), and therefore cannot account for high concentration of HEGRs. We must thus identify 78 other sources of heat (deeper and larger-scale) possibly associated with deep, large-scale 79 geodynamic processes involved by the nearby subduction systems.



82 Figure 1: The major subduction zones on Earth (modified from Schellart et al. 2007). Black stars 83 show the locations of major geothermal power stations that are larger than 50 MWe that are 84 currently operational or under construction. Red stars are reserved for highlighting those within 85 the study areas mentioned in this study. Geothermal stations: JE, Jermaghbyur (Armenia); Mi, 86 Miravalles (Costa Rica); AH, Ahuachapán, BE, Berlín (El Salvador); HE, Hellisheidi, KR, Krafla, NE, Nesjavellir, RE, Reykjanes, SV, Svartsengi (Iceland); DA, Darajat, KA, Kamojang, 87 88 MO, Mount Salak, SA, Sarulla, WA, Wayang Windu (Indonesia); LA, Larderello, SE, 89 Serrazzano, VS, Valle Secolo (Italy); HA, Hatchobaru (Japan); OL, Olkaria (Kenya); CP, Cerro 90 Prieto (Mexico); KA, Kawerau, NAP, Nga Awa Purua, NG, Ngatamariki, OH, Ohaaki, PO, 91 Poihipi, TM, Te Mihi, WA, Wairakei (New Zealand); SJ, San Jacinto Tizate (Nicaragua); LI, 92 Linhir (Papua New Guinea); BA, Bacman I, MAH, Mahanagdong, MAL, Malitbog, MI, 93 Mindanao I-II, PA, Palinpinon I-II, TI, Tiwi A-B-C, TO, Tongonan 1, UM, Upper Mahiao (Philippines); MU, Mutnovskaya, Russia; EF, Efeler, KI, Kızıldere, PA, Pamukören (Turkey); 94 95 BLM, CA, Calistoga, DV, Dixie Valley, NA, Navy, SA, Salton Sea, TG, The Geysers (United 96 States).

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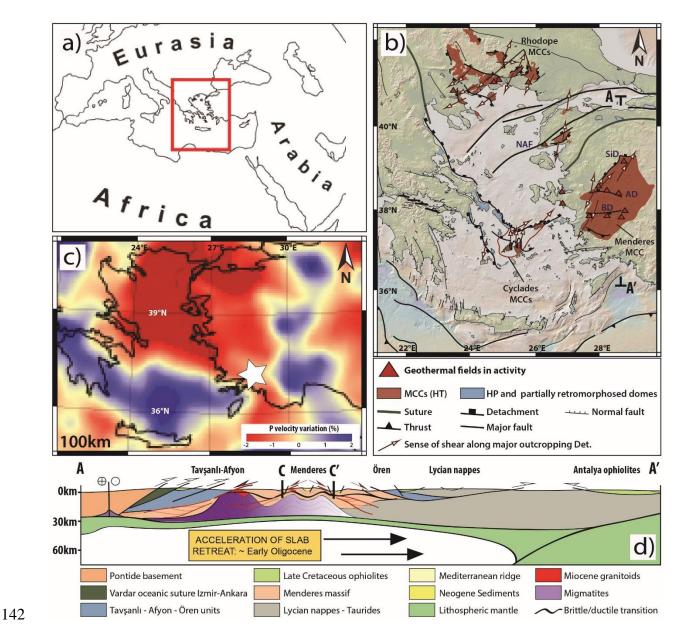
98 Slab rollback induces lithospheric extension in the overriding plate where low-angle 99 normal faults (detachments) control both the exhumation of metamorphic core complexes 100 (MCCs) and the magma ascent and/or fluid circulation (e.g. Reynolds and Lister, 1987; Huet *et*

101 al., 2011). Because detachments may correspond to permeable structures deeply rooted down to 102 the brittle-ductile transition (Famin et al., 2004; Mezri et al., 2015), active extensional domains 103 in back-arc regions could represent favorable settings for HEGRs. The possible sources of heat 104 responsible for regional high temperature-low pressure (HT-LP) metamorphic overprint recorded 105 in these MCCs include (i) heating associated with thermal diffusion of excess heat generated by 106 nappe stacking (increased radiogenic crustal heat, e.g. Bousquet et al., 1997), (ii) shear-heating 107 in the mantle (e.g. Schubert and Yuen, 1978), or (iii) advection of hot asthenosphere to shallow 108 depths during slab retreat (Wannamaker et al., 2008; Jolivet et al., 2015). However, no unifying 109 mechanism responsible for both the generation of MCCs and emplacement of high-enthalpy 110 geothermal systems in the same regions has yet been recognized. This is however a crucial 111 question since HEGRs represent a major economic interest in terms of exploration for carbon-112 free energy resources.

113 Here, we first document the self-consistent formation of crustal domes in the overriding 114 plate as a result of thermo-mechanical instabilities in 3-D numerical simulations of ocean-115 continent subduction dynamics. These models provide crucial thermal constraints for the mantle 116 and crust, and show the importance of shear heating and fast mantle flow on the overall heat 117 budget. Subduction-induced thermal signature in the overriding crust obtained from these 118 experiments is then used as basal thermal boundary condition in 2-D numerical models dedicated 119 to the understanding of fluid flow in the upper crust in presence of detachments that accommodate 120 the formation of these domes. Results show that deep upper crustal hot fluids are drained upward 121 by the permeable detachment. These results will be first compared with geological observations 122 from the Menderes Massif, and then in the discussion, with other cases in the Mediterranean 123 realm (Anatolia and Tuscany) and in the western United States.

125 2. GEODYNAMIC AND GEOTHERMAL SETTINGS OF THE MENDERES MASSIF

126 During the Cenozoic, the eastern Mediterranean region (Figs. 2a and 2b) has undergone 127 a two-step tectono-metamorphic evolution. In the late Cretaceous-Eocene, the convergence of 128 Africa and Eurasia first led to the closure of the Izmir-Ankara Ocean. At this time, the accretion 129 of subducting continental and oceanic tectonic units (e.g. Jolivet and Brun, 2010) led toformation 130 of a south-verging crustal-scale orogenic wedge. Since the Oligo-Miocene, collapse of the 131 Hellenides-Taurides belt in this region is mainly controlled by the southward retreat of the 132 African slab, further accelerated in the middle Miocene by a major slab tearing event evidenced 133 by tomographic models below western Turkey (Fig. 2c) (e.g. Piromallo and Morelli, 2003). 134 Extension in the overriding plate has thus led to exhumation of different MCCs such as the 135 Cyclades in the Aegean Sea and the Menderes Massif in western Anatolia, accommodated by 136 crustal-scale low-angle normal faults such as the Simav, Alaşehir and Büyük Menderes 137 detachments (Hetzel et al., 1995; Bozkurt et al., 2011) (Figs. 2b and 2c). Currently, plate 138 kinematics in this region are characterized by more localized extension, mainly controlled by the 139 westward motion of Anatolia (Reilinger et al., 2006) and by N-S extension accommodated by 140 steep normal faults in the Gediz and Büyük Menderes Grabens, both consequences of slab 141 dynamics (e.g. Jolivet et al. 2013; Gessner et al., 2013; Sternai et al., 2014).



143 Figure 2: (a) Global map with red box showing the location on the study area. (b) Simplified 144 tectonic maps showing the main metamorphic core complexes and associated detachments faults 145 in the Aegean region (modified from Jolivet et al., (2015)). SiD: Simav Detachment, AD: 146 Alaşehir Detachment, BD: Büyük Detachment, NAF: North Anatolian Fault. (c) Tomographic 147 models from Piromallo and Morelli (2003) showing the Vp anomalies at the 100 km depth. White 148 star shows the location of a slab tear below the Menderes Massif. (d) Simplified cross-sections 149 highlighting slab retreat and formation of crustal detachments. CC' corresponds to the 2-D 150 numerical model cross-section.

152 The Menderes Massif is also recognized as an active geothermal area (see Fig. S1a in 153 Appendix 1). This region is characterized by long wavelength east-west variations of surface heat flow density with values locally exceeding 90 mW m⁻² (Erkan, 2015). At depth, it seems that a 154 155 similar east-west long wavelength thermal anomaly is also present, as suggested by the Curie-156 point isotherm map of Aydin et al. (2005). According to these authors, the depth of the 580 °C 157 isotherm would be lower than 10 km in western Anatolia (see Fig. S1b in Appendix 1). It turns 158 out that most of the geothermal systems in Turkey are located in the Menderes Massif (Fig. 2b) 159 where recent magmatism is almost absent. Here, geothermal fields are characterized by medium-160 to high-enthalpy, with reservoir temperature values ranging from 120 to 287 °C (e.g. Roche et al. 161 in revision). Most are used for district heating systems (e.g. Balçova and Salihli), whereas a few 162 are exploited for electricity production (e.g. Germencik, Salavatli; Kızıldere; Alaşehir). Some 163 authors have suggested that most of the geothermal activity can be considered as amagmatic in 164 origin (Faulds et al., 2010; Gessner et al., 2017). However, Ozdemir et al. (2017) considered a 165 probable magmatic intrusion in the crust to explain the heat source. Since there is presently no 166 evidence for the existence of such plutons, some authors suggest a deeper and larger heat source 167 triggered by large-scale tectonic processes such as subduction (Kaya, 2015; Gessner et al., 2017; 168 Roche et al., submitted). In that sense, Kaya (2015) invoked a possible lithospheric thinning as 169 the origin of the anomalously high heat flow. This example show that large-scale processes 170 related to lithosphere dynamics could be involved in the genesis of geothermal systems. We thus 171 need to employ a multi-scale approach (lithospheric- and crustal-scales), to improve the 172 characterization of heat transfer possesses from the mantle to the geothermal system.

174 3. 3-D THERMAL EVOLUTION OF SUBDUCTION

175 In a previous study dedicated to the analysis of surface deformation in the Aegean-176 Anatolian domain, Sternai et al. (2014) found that mantle flow due to slab rollback and tearing 177 can drag the upper plate from below, and explain upper plate extension and the formation of the 178 North Anatolian Fault. Their results emphasize the active role of mantle flow in driving the 179 surface strain and horizontal crustal velocities. However, the associated thermal processes were 180 not described by these authors. Because heat transport is inherently coupled with deformation, 181 mantle shearing may provide a strong heat source. Thus, we must consider it, especially if we 182 want to describe in detail the thermal features associated with 3-D subduction dynamics when 183 slab rollback and tearing occur. Indeed, while radioactive heat production is considered as the 184 main heat source in the continental crust, shear heating has been suggested to be important in the 185 mantle (Shubert and Yuen, 1978) and thus probably also in arc and back-arc settings where fast 186 slab dynamics may be associated with intense asthenospheric flow. Here, we perform similar numerical simulations than Sternai et al. (2014), but improve the analysis by investigating the 187 188 effects of shear heating. We describe the numerical results from a thermal point of view, by 189 focusing on the localization of crustal thermal anomalies in the overriding plate.

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3.1. Model setup

The numerical simulations were performed with the code "I3ELVIS" (Gerya, 2010) that solves the momentum, continuity and energy equations based on a staggered finite difference scheme combined with a marker-in-cell technique. Realistic, non-Newtonian visco-plastic rheologies are used in the model, and includes temperature- and pressure-dependent viscosities (see Appendix 2). The model setup is shown in Figure 3. The model domain measures

197 2000 x 328 x 1000 km in the x, y and z dimensions, respectively and is resolved by 198 501 x 165 x 197 grid points resulting in a resolution of 4, 2 and 5 km in the x, y and z dimensions, 199 respectively. It includes three continental plates (C1, C2 and C3), allowing reproduction of 200 similar tectonic events that affected the Tethys convergent domains (subduction, collision, slab 201 tearing, trench retreat; Sternai et al. 2014). These three continental plates are defined by a crust 202 of 35 km, 50 km and 45 km thick (Fig. 3). In addition to the trench-parallel weak fracture zone 203 allowing for subduction initiation, the model includes a trench perpendicular weak fracture zone 204 within the oceanic domain, which allows for slab tearing (Fig. 3).

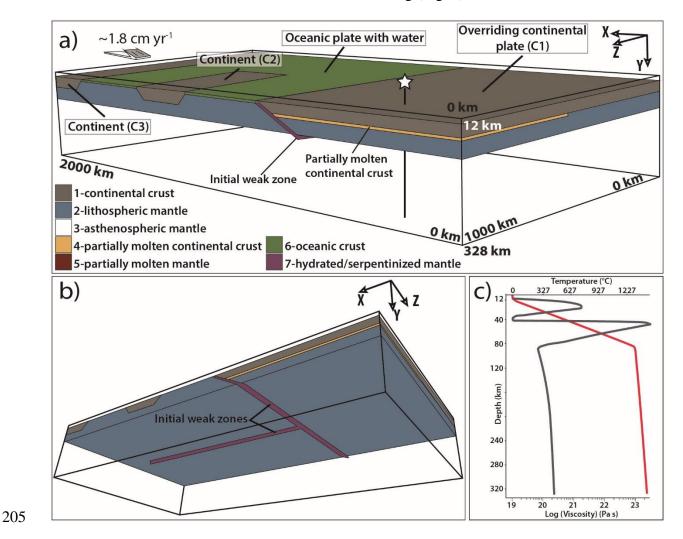


Figure 3: Numerical setup. (a) 3D initial model setup where the top layer ("sticky air", $y < \sim 12$ km") and the water are cut off for clarity. Colours showing different rock types. (b) Location of

the "weak zones" (i.e. hydrated/serpentinized mantle) into the lithosphere to trigger subduction
(z-parallel) and to allow slab tearing (x-parallel) in the initial model. (c) Initial vertical profiles
of viscosity (grey) and temperature (red), taken at the location shown by the white star.

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212 The initial thermal structure of C1, C2 and C3 is laterally uniform with 0 °C at the surface 213 and 1300 °C at 90, 140 and 150 km depth, respectively. The initial thermal structure of the oceanic 214 lithosphere corresponds to the cooling age of 120 Ma (e.g. Turcotte and Schubert 2002). The initial temperature gradient in the asthenospheric mantle is ~ 0.5 $^{\circ}$ C km⁻¹ (adiabatic). Boundary 215 216 conditions involve free slip on the z = 0 and z = 1000 km sides of the model domain, while uniform and constant x-parallel velocities equal to ~ 1.8 cm yr^{-1} (convergence) are imposed at 217 218 the x = 2000 km boundary, and the x = 0 km is fixed. Global mass conservation is ensured by 219 material outflow through the permeable lower boundary (y = 328 km). Surface processes are also 220 implemented using a highly simplified gross-scale erosion-sedimentation law. The parametric 221 study on various boundary conditions and parameters is presented in Sternai et al. (2014).

Heat production by viscous or plastic shearing (H_s), consisting of the dissipation of the mechanical energy during irreversible non-elastic deformation, is controlled by the deviatoric stresses σ'_{ij} and strain rates $\dot{\varepsilon}'_{ij}$, as follow (Gerya, 2010):

$$225 H_s = \sigma'_{ij} \dot{\varepsilon}'_{ij} (1)$$

The possibility to investigate H_s in our numerical simulations is a significant advance with respect to the previous models presented in Sternai *et al.* (2014). In order to test the possibility that slab tearing would enhance mantle shear heating, two series of numerical models, with and without slab tearing, have been performed, all other settings being equal (i.e. same boundary conditions, material properties, see more information in Appendix 2).

2 **3.2. Results**

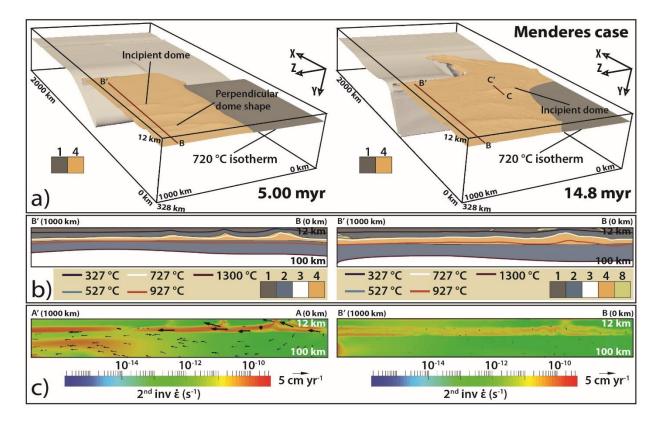
233 Before focusing on thermal effects associated with slab dynamics, we briefly present the 234 model evolution. The overall sequence of events is robust and includes first an early subduction 235 of the oceanic domain between C1 and C2 with localized extensional deformation in the 236 overriding plate. In our models, it includes the magmatic arc and the back-arc domain (see video 237 S1 in Appendix 1). During this first subduction event, a toroidal mantle flow occurs below C1, 238 as induced by the down-going slab. This event also controls crustal flow and surface 239 deformation. Afterward, continental collision between C1 and C2 occurs, locally increasing slab 240 dip and thus favoring slab tearing. Later subduction of the oceanic domain between C1 and C3 241 induces widespread extensional deformation in the overriding plate. This last event is highly 242 conditioned by the previous horizontal to sub-horizontal return flow of hot asthenosphere, which 243 warms up the incipiently subducting lithosphere close to the slab tear, enhancing here a non-244 cylindrical (i.e. not parallel to the initial upper plate margin) slab rollback. Rheological 245 stratification of the upper plate is characterized at this stage by a thin rigid lithospheric mantle 246 (~10 km). Deformation is localized in the overriding plate with strike-slip deformation 247 propagating toward the subducting plate (Sternai et al., 2014).

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3.2.1. Thermo-mechanical instabilities

The early subduction event is characterized by the development of several positive thermal anomalies (i.e. anomalously high temperatures) (i) at the base of the crust with wavelengths around 200 km, and (ii) in the overriding lower crust, within a partially molten lowviscosity layer, with wavelengths around 30 km (Figs. 4a and 4b). The thermal instabilities in the low-viscosity crust generate dome-like structures cored by partially molten low-viscosity 255 material (orange colour in Figs. 4a and 4b). These domes are elongated parallel to the subduction 256 trench and separated by 200 - 300 km (Fig. 4a). With time, new thermal domes appear toward 257 the trench, controlled by the flow of low viscosity material in response to both slab rollback and 258 tearing (Fig. 4b; Videos S2-S3 in Appendix 1). The strain rate distribution shows that mature 259 crustal domes preferentially localize deformation, rather than incipient crustal domes closer to 260 the trench (Fig. 4c). In addition, deformation localizes around the edges of these domes, showing 261 the importance of lateral crustal strength contrasts on strain localization (Video S4 in Appendix 262 1). At 14.8 Myr, two domes have disappeared but the thickness of the partially molten layer at 263 the base of the crust has tripled (from ~ 4 km to 15 km thick, Fig. 4b; Video S3 in Appendix 1). 264 Meanwhile, the horizontal component of flow velocity in the partially molten layer has decreased 265 (from ~ 5 to ~ 1 cm yr⁻¹, Fig. 4c). On the opposite, above the slab tear, the deformation is localized 266 (see Fig. 4b in Sternai et al. (2014)) and horizontal component of crustal and mantle velocities have increased up to ~ 6 and ~ 9 cm yr⁻¹, respectively. The shear heating and the advective mantle 267 268 heat flow components near the fast velocity zones are enhanced accordingly, as detailed below.



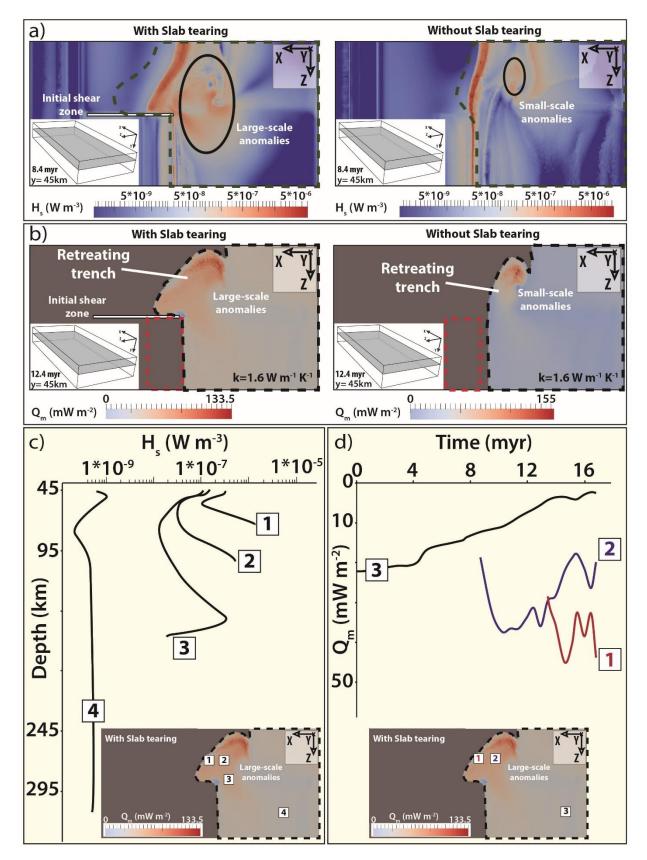
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Figure 4: Thermo-mechanical evolution of the model. (a) The 720 °C isotherm at 5 myr and at
14.8 myr, respectively. Colours showing different rock types: 1, 4 indicate upper and lower crust,
respectively, see also Figure 3. Note the position of CC' that may correspond to the 2-D numerical
model cross-section. (b) Vertical cross-sections showing different rock types and isotherms.
Colours showing different rock types: 1-2-3-4 as defined in Figure 3; 8-hydrated crust. (c)
Vertical cross-sections showing the second invariant of the strain rate tensor and velocity vectors.

3.2.2. Slab dynamics and shear heating

The contribution of shear heating to heat production in our reference model (with slab tearing between C2 and the oceanic domain) is compared to similar simulations without slab tearing (Fig. 5; see Fig. S3 in Appendix 1). The frictional heat produced in the overriding plate locally reaches values of ~ 5.0μ W m⁻³ regardless of slab tearing (Fig. 5). However, when slab tearing occurs, a larger-scale thermal perturbation appears and develops below and at the base of the crust (~ 400 x 200 km at 12.4 Myr; see Fig. 5b). Anomalies associated with shear heating are 285 thus distributed over a larger domain in the case of tearing because of a more widespread mantle 286 flow around the tear, and appear more localized and parallel to the subduction trench without 287 tearing (Fig. 5a, see right panel). In addition, our results show that the amount of heat produced 288 by shearing leads to an increase of mantle heat flow (Q_m) at the base of the crust, and particularly above the tear. In particular, for average shear heating of ~ $2.0 \ \mu W \ m^{-3}$ and mantle thickness of 289 290 30 km (Fig. 5c, profile 1), the contribution to the heat flow nearby the subduction front is of ~ 60 mW m⁻² at 12.4 Myr. Conversely, far from the subduction front, shear heating is insignificant (< 291 1.0 nW m⁻³, see Fig. 5c, profile 4), implying no contribution of this mechanism to heat production 292 293 by this mechanism (Fig. 5d, profile 1).

294 Shear heating in the mantle during slab retreat and tearing plays a key role in increasing 295 temperatures at the base of the overriding crust, where mantle heat flow values are around 100 mW m⁻² and reach locally up to 130 mW m⁻² above the slab tear at 12.4 Myr (Fig. 5b, see left 296 297 panels). We found that 46 % of the heat flow at the base of the crust is due to mantle shear heating, 298 the remaining part being due to the advection of hot material. In the absence of slab tearing, the average of mantle heat flow at similar times is around 80 mW m⁻², reaching locally up to 155 299 mW m⁻² but over a much smaller area, (Fig. 5b, right). We therefore suggest that advection of hot 300 301 asthenosphere to shallow depths during slab retreat and tearing plays an important role in 302 increasing temperatures at the base of the crust (Fig. 6). Furthermore, mantle heat flow values may reach steady-state after ~ 4 Myr (values around $40 - 50 \text{ mW m}^{-2}$, Fig. 5d). 303





305 Figure 5: Mantle heat source with and without tearing at the mantle-crust transition. (a) Plan view

306 of shear heating (H_s) at the mantle-crust transition at 8.4 Myr. Dashed line on both panels shows 307 the plan view of the overriding plate C1. (b) Plan view of mantle heat flow (Q_m) at the mantle-308 crust transition at 12.4 Myr. Black and red dashed lines on both panels show the plan view of the 309 overriding mantle, and of the overriding C2, respectively. (c) Vertical depth-shear heating (H_s) 310 profiles in the mantle below the stretched overriding plate at $t_0 + 14.8$ myr, taken at the location 311 shown by the white squares. (d) Evolution of mantle heat flow (Q_m) at the mantle-crust transition. 312 The values are taken at the location shown by the white squares.

313

314 To summarize, slab tearing facilitates the rollback of the subducting plate and extension 315 within the upper plate. Consequently, slab tearing and its associated mantle flow contributes to 316 the increase in heat flux at the base of the crust by (i) enhancing mantle shear heating and (ii) 317 controlling the return flow of hot asthenosphere (e.g. toroidal and poloidal mantle flow 318 components). Both mechanisms together appear to be able to increase the Moho temperature by 319 up to 250 °C (Fig. 6). Therefore, slab tearing may (i) affect the heat source responsible for regional HT-LP metamorphic rocks in MCCs and (ii) explain regional high-temperature 320 321 anomalies across amagmatic geothermal systems in post-subduction settings.



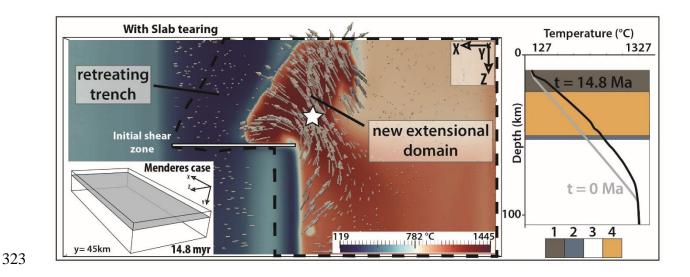


Figure 6: Plan view of temperature anomaly at the mantle-crust transition (~ 45 km depth) in the case of slab tearing. Grey arrows represent the velocity vectors in the asthenosphere. Black dashed line on the left panel shows the plan view of the overriding plate C1. Right panel: vertical temperature profiles at to and to + 14.8 myr, taken at the location shown by the white star. Colours showing different rock types: 1-2-3-4, as defined in Figure 3.

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330 4. FROM SUBCRUSTAL THERMAL ANOMALIES TO GEOTHERMAL SYSTEMS:

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2-D MODEL OF FLUID CIRCULATION

332 Results of the 3-D model show that at 12.4 Myr, mantle heat flow can reach anomalously high values exceeding 130 mW m⁻² (Fig. 5b). At 10 km depth above the tearing, temperature 333 334 values vary between 450 and 500 °C, and are thus similar to estimated temperatures from 335 aeromagnetic data at the same depth in the Menderes Massif (~ 580 °C) (Aydin et al., 2005). 336 Using these results, we defined a 2-D fluid flow model in a porous media to analyse the thermal 337 consequences of anomalously high basal heat flow on fluid circulation in the upper crust. The 338 advantage of this model is a good spatial resolution (see Appendix 2), representative 339 permeability, and realistic rock and fluid properties.

340 The model measures 120 x 10 km and is designed to represent a SSW-NNE cross section 341 of the Menderes massif. We choose the basal heat flow in order to (1) account for previous 3-D 342 numerical results where mantle heat flow could reach values up to 130 mW m^{-2} (Fig. 5b), and (2) 343 reproduce temperatures above 500 °C at 10 km depth, as suggested by Curie-point depths in 344 western Anatolia (Aydin et al., 2005). The objective of this model is to understand the effects of 345 high basal heat flux on the fluid flow circulation pattern, in particular around permeable 346 detachments. In the following, we describe the main characteristics of the model setup and 347 present the main results.

4.1. Model setup

350 Coupling between Darcy's law, heat transfer equation and mass conservation is performed using the Comsol Multiphysics[™] software (finite element method). Details about the 351 352 numerical procedure (benchmark experiments, model setup, fluid and rock properties) are given 353 in Appendix 2. The model is shown in Figure 7, where two detachment faults (with a dip angle 354 varying from 10 to 20°) represent the Büyük Menderes and the Alaşehir Menderes detachments 355 (Fig. 2b). Figure 7a illustrates the mesh refinement in permeable zones (close to the surface and 356 within the detachments). A convective flux condition was imposed at the top of the detachments, 357 in order to allow the emergence of hot fluids at the surface. In addition, we use temperature-358 dependent density and viscosity laws for fluids (see Appendix 2). No magmatic source is present 359 in the model, and the chosen basal heat flow value at a depth of 10 km corresponds to 120 mW m⁻² (Fig. 7b). This value is therefore consistent with both criteria (i.e. mantle heat flow from our 360 3-D model and Curie-point depths estimations). A constant pressure of 10^5 Pa is imposed at the 361 362 surface allowing fluid influx while no flow is allowed across the others boundaries of the box 363 (Fig. 7b). At time t = 0, thermal regime is purely conductive (see white isotherms in Fig. 7c). 364 Then, permeability values are switched on (color code of Figure 7c; Appendix 2) and the transient 365 evolution of temperature and velocity fields are recorded during 5 Myr. Permeability in the 366 basement (k_b) decreases exponentially with depth (Manning and Ingebritsen, 1999) (see Fig. 7c 367 and Appendix 2) while detachment permeability is assumed constant (k_d) . Despite a number of 368 arguments in such extensional setting suggest high permeability at the surface (highly fractured 369 and karstified rock, see Özen et al. (2012)) numerical values remain unconstrained. We therefore decided to test a wide range of realistic permeabilities for the basement (i.e. from 10⁻¹⁷ to 10⁻¹⁴ 370 371 m²) and the detachment fault with same range of values (Fig. 7b).

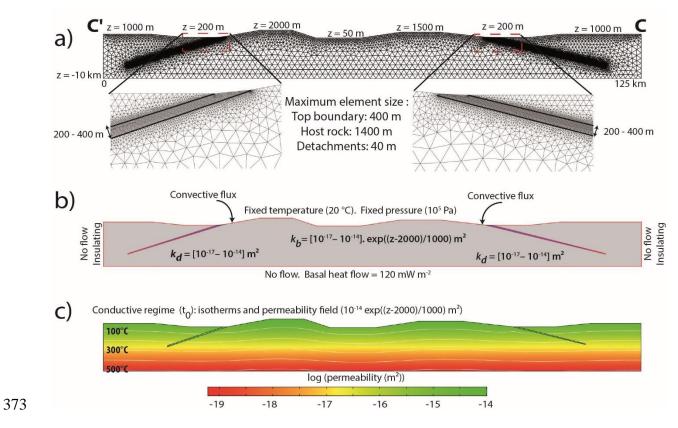


Figure 7: (a) Geometry and mesh used for 2-D models of fluid circulation in the upper crust of 374 375 the Menderes area, where MCCs and detachments are reproduced. This cross section would 376 correspond, from left to right, to a N-S cross section, from Salihli to Salavatlı geothermal areas. 377 Mesh is refined at the top surface and within detachments, where permeability is the highest. (b) 378 Boundary conditions and range of values for permeability (note the depth-dependence of the host 379 rock permeability). (c) Steady-state conductive regime, where isotherms in white are separated 380 by 100 °C. Colors refer to permeability values affected at time t > 0 (see text) for the case detailed 381 in Figure 9.

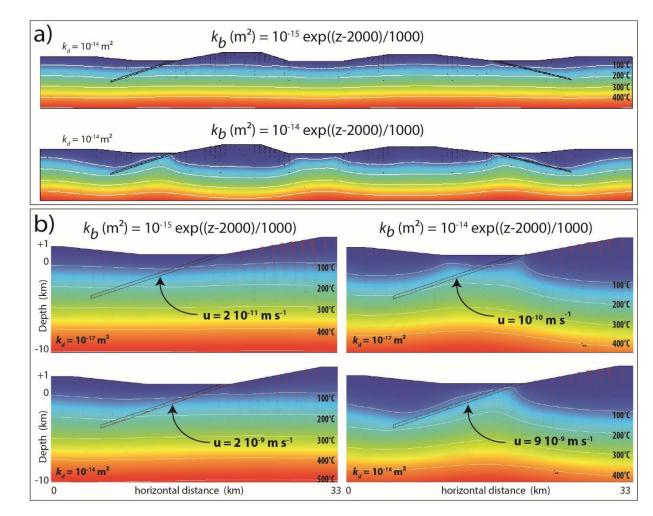
- 382
- **4.2. Results**

384

4.2.1. Role of basement and detachment permeabilities

Figure 8 illustrates steady-state temperature fields for different combinations of both basement and detachment permeability. In Figure 8a, results show the major role of k_b to distort

significantly the isotherms, even if k_d is high (10⁻¹⁴ m²). In the upper case of Figure 8a, isotherms 387 388 remain flat and no thermal reservoir forms beneath the detachments. Alternatively, the lower case 389 with realistic higher permeability values shows a general fluid circulation pattern characterized 390 by: (i) surface meteoric fluids that flow from topographic highs to the top of the detachment fault 391 and other topographic lows, inducing a negative thermal anomaly in the hanging walls of 392 detachments; (ii) at depth, hot fluids are drained upward by the permeable detachments allowing 393 for isotherms to rise along the fault zones (see uplifted isotherms in bottom case of Fig. 8a). A 394 positive thermal anomaly is due to hot fluids rising up toward the top of the detachment while a 395 negative thermal anomaly induced by topography-driven flow grows in the hanging walls of 396 detachments, leading to the formation of hot fluid reservoirs beneath the detachments (near the 397 surface). To synthetize, at the scale of the whole massif, thermal undulations mimicking dome-398 like structures are localized beneath topographic lows in the case of a high basement permeability 399 (Fig. 8a, bottom case).



401

Figure 8: Results for thermal perturbations due to fluid circulation in permeable zones for varying basement permeability (k_b) and for varying detachment permeability (k_d). (a) role of the basement permeability for a fixed value of k_d (10⁻¹⁴ m²). (b) Zoom on the left detachment, with varying permeabilities (small k_d value in the top row; high k_d value in the bottom row). Left (right) column corresponds to a small (high) basement permeability.

When k_d is varied (Fig. 8b), it turns out that thermal reservoirs establish at shallow depth when both k_d and maximum k_b values are important (10⁻¹⁴ m², bottom right case in Fig. 8b). In the case where k_d is low (10⁻¹⁷ m², top case in Fig. 8b) two thermal reservoirs appear only with a high maximum k_b value, suggesting that topography-driven flow is dominant. However, 412 temperatures at shallow depth and fluid velocity values within the detachment are much lower 413 than in the high k_d case (bottom right case in Fig. 8b). Crustal-scale permeable faults and their 414 induced high topography thus control the spatial distribution of upper-crust thermal anomalies at 415 depth, mimicking dome-like structures beneath topographic lows (Fig. 8a, bottom case, and Fig. 416 8b, right column).

417

4.2.2. Fluid flow field and temperature profiles

418 Figure 9a illustrates the fluid flow velocity pattern in the case of Figure 8a (bottom case). 419 Fluid flow is favored by high-topography and permeable zones such as detachments. Located 420 within detachments, high velocity areas (> 10^{-10} m / s – or 0.32 cm / yr) are recorded down to 5 421 km deep (red areas). The bottom panel of Figure 9a shows a horizontal temperature profile at 1 422 km depth. It is important to note that temperature anomalies of ~ 140 °C are focused close to the 423 top of the detachments. Figure 9b (left column) shows computed vertical temperature profiles at different distances from the two detachments, at a given time (i.e. 4×10^4 yr). Figure 9b (right 424 425 column) illustrates temperature measurements at the Aydin-Salavatlı geothermal field, Büyük 426 Menderes Graben, within 2 boreholes ~1.5 km apart. Although the comparison of daily-measured 427 thermal profiles with these two sets of vertical temperature profiles is limited, one can observe 428 some similarities with (i) a high-temperature gradient at the surface, decreasing rapidly with 429 depth, and (ii) some negative values of the temperature gradient. In addition, modeled 430 temperatures are comparable, with emergence temperatures around 60 °C and reservoir 431 temperatures at depth around 180 - 200 °C. Because our density law is simplified (see Appendix 432 2), and because the vapour phase is not accounted for, the computed profiles show rather smooth 433 curves when compared to measurements. However, the typical convective signatures in 434 temperature profiles are similar.

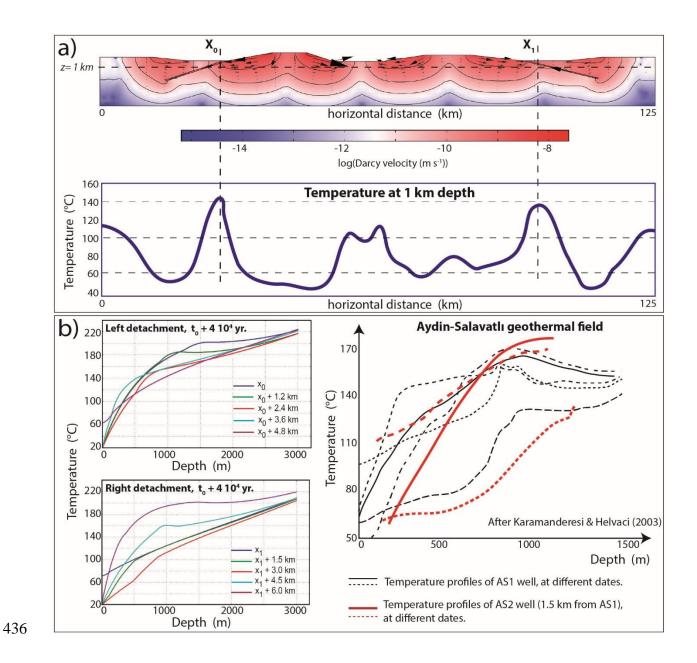


Figure 9: Results for the experiment shown in the lower case of Figure 8a (and right case of Figure 8b). (a) Fluid flow velocity field (colors, isocontours and arrows) and horizontal temperature profile at 1 km depth (dashed line in the fluid flow pattern). Note that the largest temperature perturbations correspond to the top of the detachment locations (x_0 and x_1). (b) Computed vertical temperature profiles at time $t_0 + 4 \, 10^4$ yr. x0 and x1 are indicated in Figure 9a. On the right, measured temperature profiles at the Aydin-Salavath geothermal field; black curves

(plain and dashed) correspond to different measures in the same AS1 borehole (different dates of
measurements) and red lines are measured in the AS2 borehole, 1.5 km from the AS1 borehole
(after Karamanderesi and Helvaci, 2003).

446

447 **5. DISCUSSION**

448 5.1. Large-scale thermo-mechanical boudinage, and emplacement of MCC in Western 449 Anatolia

450 The modeled thermo-mechanical instabilities (Fig. 4) are not only analogous to crustal 451 and lithospheric boudinage (Ricard and Froidevaux, 1986), but they add a thermal component to 452 what was generally assumed to be purely mechanical. These instabilities developed in the 453 overriding plate are triggered by both shear heating and hot mantle flows. These mechanisms 454 indeed induce a thermal weakening of the lithosphere, thus controlling the development of 455 boudinage at different scales, and the localization of MCCs in the extensional crust. It is important 456 to note that these domes are also promoted by the low-viscosity crust, which is related to the 457 chosen initial thermal regime in our models. When the slab tear is accounted for, the crust is weak 458 over a wider domain above the tear, increasing its ability to flow (e.g. Block and Royden, 1990; 459 Rey et al., 2009) and to form HT domes. In other words, shear heating and mantle flow control 460 the position of positive thermal anomalies in the overriding crust, which, in turn, control the 461 deformation pattern in the lower crust during extension. Such a lithospheric thermal weakening 462 is further enhanced by the accumulation of magmas in the back-arc domain, which is widely 463 promoted by slab rollback and tearing processes (Menant et al., 2016b).

In the Cyclades (Greece), the dominant wavelength of MCCs (several tens of kilometres, similar to the spacing between the different islands) is compatible with that expected for crustalscale boudinage (Fig. 4). At the scale of the whole Aegean domain, long-wavelength variations

467 of Moho depth (Tirel et al., 2004; Karabulut et al., 2013) are more reminiscent of lithospheric-468 scale boudinage (several hundreds of km; Fig. 4). This boudinage of the crust induces migmatite-469 cored MCCs which were first exhumed in the northern Menderes Massif in the Micoene (Cenki-470 Tok et al., 2016), and then in the central and eastern Cyclades since the lower Miocene (Jolivet 471 et al., 2015), coevally with a further acceleration of trench retreat related to the Hellenic slab 472 tearing. This is consistent with our model, where dome-like structures, cored by partially molten 473 low-viscosity material, develop first in the overriding plate, and then migrate toward the trench, 474 in response to both slab rollback and tearing (Figs. 4a and 4b). In addition, we suggest also that 475 excess heat due to these subduction dynamics controlled the retrogression in the greenschist-476 facies of high-pressure metamorphic rocks in Cyclades (post-orogenic extension), consistently 477 with acceleration of slab retreat around 35 Ma (Jolivet et al., 2015). Furthermore, our numerical 478 experiments highlight an increase of Moho temperature during a few Myrs related to 479 asthenosphere upwelling below the overriding plate (Figs. 5d and 6). We therefore suggest a 480 similar heating for the mantle-crust boundary in the Anatolian-Aegean domain, which is 481 consistent with the presence of HT metamorphic domes and the formation of syn-extension 482 granites and migmatites throughout the entire western Anatolian-Aegean domain between 20 Ma 483 and 8 Ma (Jolivet et al., 2015; Menant et al., 2016a).

In the Menderes MCC (located above the slab tear, see Fig. 2), strain was first localized in the north, along the Simav Detachment (early Miocene, stage 1 after Gessner *et al.* 2013) accommodating the exhumation of an asymmetric migmatite-cored MCC (Rey *et al.*, 2009; Cenki-Tok *et al.*, 2016). Then, strain migrated southward, toward the trench and localized within the central part of the Menderes Massif (Fig. 2c). The Alaşehir and Büyük Menderes detachments assisted exhumation of the lower crust during slab tearing (middle-late Miocene, stage 2 after 490 Gessner et al. 2013). This implies that the central part of the Menderes Massif had become weaker 491 than the previously activated Simav area, probably due to the extra source of heat associated with 492 slab tearing. According to Labrousse et al. (2016), the evolution of the style of extension from an 493 asymmetric MCC (localized deformation, case of the Simav detachment) to a double-dome 494 symmetric MCC (distributed deformation, case of the Menderes detachments) implies that heat 495 input at the base of the crust is higher than heat dissipation due to stretching. These observations 496 are consistent with the thermal features observed in our model, which emphasize the crucial role 497 of shear heating, as well as poloidal and toroidal components of mantle flow, to heat the lower 498 crust (Figs. 5 and 6). Both mechanisms are thus responsible for the presence of large-scale 499 thermal anomalies at depth (i.e. 580 °C at 10 km depth) and at the surface (i.e. heat flow values around 100 mW m⁻², Erkan, 2015). As a consequence, the thermal state of the crust induced by 500 501 elevated mantle heat flow could control the style of extension (asymmetric versus symmetric 502 MCC).

503 Furthermore, hot fluids circulating within crustal-scale permeable faults help increasing 504 basal temperatures (around the ductile/brittle transitions) by several tens of °C (Fig. 8a), resulting 505 in a positive feedback for the formation of new shear zones and MCCs at depth. In this case, 506 magmatic bodies such as granitoids and migmatites may be developed and localized below the 507 detachment, as it seems to be the case in the Menderes with the Salihli diorite and Simav granites. 508 The progressive formation of HT domes topped with extensional detachments can thus 509 be summarized as follows: (1) mechanical (boudinage) and thermal instabilities within the 510 stretched lithosphere generate a series of domes, periodically spaced, producing rheological 511 heterogeneities (i.e. low-viscosity layers) that are likely to localize extensional shearing 512 deformation on their edges (Le Pourhiet et al., 2003; Huet et al., 2011) and (2) upward flow of deep hot fluids and downward flow of cold surface fluids further increase thermal contrasts acrossthe shear zones, enhancing the localization of deformation.

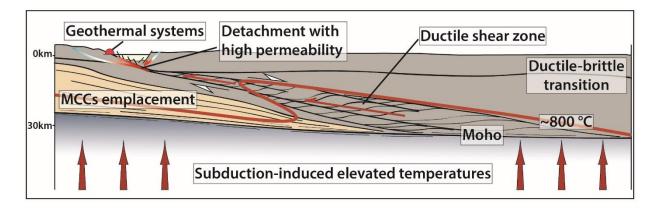
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- 516

5.2. Detachments and localisation of HEGRs in Western Anatolia

517 The relationships between the localization of the deformation and thermal domes (Fig. 4) 518 are similar to that documented in MCCs, and may be associated with crustal-scale permeable 519 faults, which can provide pathways for meteoric waters to flow into the actively deforming 520 middle crust (e.g. Famin et al., 2005; Mulch et al., 2006). As shown in Figure 5, the excess of 521 mantle heat flow is transfered by conduction into the crust, affecting the fluids present in the 522 crustal porosity. These fluids may then undergo deformation-driven flow in ductile shear zones 523 (e.g. Oliver, 1996), but also thermally driven (i.e. buoyancy-driven) flow through the crust, where 524 high permeability detachments may easily collect and bring up deep hot fluids. Indeed, our 2-D 525 numerical models suggest that an elevated basal temperature (580 °C) at 10 km depth would induce temperatures of 300 – 350 °C at a depth of 6 km and thus a sufficiently high fluid density 526 527 contrast to permit upward flow along the low-angle fault in the shallower crust. In that case, 528 buoyancy-driven flow is superimposed to topography-driven flow (Fig. 8). In other words, the 529 topography-driven flow, which prevails in the regional fluid flow pattern, is dominated by 530 buoyancy-driven flow within highly permeable detachments.

Although the spatiotemporal evolution of permeability within detachments is poorly known, field observations on these geological structures (Famin *et al.*, 2005) suggest that they could represent highly permeable zones of several hundreds of meters thick where fluid flow is facilitated (Fig. 10). Moreover, if these channelized fluid flow systems are tectonically active, earthquake faulting may be associated with seismic pumping that enhances fluid migration 536 toward dilation zones (Sibson et al., 1975; Famin et al., 2005). As a consequence, detachments 537 may be considered as the crustal-scale structural control for the circulation of deep geothermal 538 fluids related to HEGRs (e.g. Bellani et al., 2004; Roche et al. submitted), driving the long-term 539 crustal-scale history of the geothermal systems (Fig. 10). However, it is noteworthy that most of 540 the geothermal systems in the Menderes Massif reside in fault intersection zones, where N-S 541 transfer faults and low-angle normal faults mostly formed dilational jogs that seem to promote 542 the emergence of hot waters and gas vents (Roche et al., submitted). Fault interactions would 543 thus allow for fluid rising in the hanging wall from the reservoirs located below the detachment 544 (Fig. 8b, right column), and control the location of thermal springs. Further numerical simulations 545 would therefore be required to confirm this hypothesis based on field observations.

546



548 Figure 10: Schematic cross section showing fluid flow associated with detachment zone in back-549 arc area. Red arrows indicate fluid circulation in ductile crust and circulation of meteoric fluids 550 in the upper crust are underlined by colored pathways (blue for cold and red for warm). 551

553

5.3. Subduction dynamics and localisation of HERSs: the Larderello (Tuscany) and the Basin and Range (Western United States) areas

554 Our 3-D and 2-D model results are relevant to other regions, and thus may explain 555 relationships between subduction dynamics and the location of geothermal provinces; for 556 instance, (i) in the Larderello area post-orogenic extension is active in back-arc domain; or (ii) in 557 the Basin and Range Province (western United States). In both cases, MCCs are exhumed along 558 low-angle normal faults, and therefore represent a favorable setting for HEGRs. While some of 559 them are considered as "amagmatic" in origin (e.g. Bellani et al., 2004; Faulds et al., 2010), some 560 authors require a magmatic heat source (e.g. Koenig and McNitt, 1983; Santilano et al. 2015). Through these two main additional examples, we show that the "magmatic" vs. "amagmatic" 561 562 classification may be ambiguous according to the long-term behavior of these geothermal 563 systems.

564 In the Northern Tyrrhenian Sea and Tuscany regions, subduction dynamics has also been 565 controlled by slab retreat since the Oligo-Miocene. This region is characterized by a shallow 566 Moho discontinuity (20 - 25 km depth), and a reduced lithosphere thickness due to uprising 567 asthenosphere and the delamination of crustal lithosphere (Gianelli, 2008). At crustal-scale a 568 series of low-angle normal faults crosscut the old thrusts (e.g. Faccenna et al., 1997; Jolivet et 569 al., 1998), and thus cannot be explained by a reactivation of pre-existing inherited discontinuities. 570 Instead, our numerical models suggest that thermo-mechanical boudinage induced by slab 571 rollback triggers the formation of localized shear zones and allows the exhumation of MCCs (e.g. 572 Elba Islands, Fig. S4 in Appendix 1). These shear zones are still active (Bellani et al., 2004) and 573 may control the ascent of magmatic intrusions, such as beneath the Larderello geothermal field.

574 We therefore suggest that magmatic intrusions in the upper crust result directly from the deep 575 thermal anomaly associated with slab dynamics during extension.

576 Although subduction dynamics are quite different in the Basin and Range province (i.e. 577 first characterized by slab retreat since the Eocene at the northern edge of the Farallon slab 578 (Schellart *et al.*, 2010), and then by an asthenospheric upwelling above the Californian slab 579 window at 30 Ma (Atwater, 1970)), similar remarks also hold for this region. Indeed, our results 580 are consistent with geological observations where the presence of a conductor at 15-35 km 581 depth range (Wannamaker et al., 2008) suggests that the central part of the Basin and Range 582 domain has become weaker, probably due to an extra source of heat associated with slab window 583 (i.e. magma underplating due to mantle flow and shear heating). In light of our numerical results, 584 we propose that fast-flowing asthenosphere also strongly heats the lithospheric mantle and the 585 lower crust via shear heating and mantle upwelling processes. Lithospheric weakening thus 586 promotes the propagation of major fault zones throughout the crust, leading to the connection 587 between the weaker conductive lower crust and the brittle upper crust (Fig. 10). Hot thermal 588 fluids at depth can then ascend within the damage fault zones, which thus control the location of 589 HEGRs at the surface (Faulds *et al.*, 2010). It is noteworthy that the presence of recent intrusions 590 (e.g. Steam Boat, Casa Diablo in the Walker Lane geothermal belt, Koenig and McNitt, 1983) 591 locally enhances thermally-driven flow, by increasing the temperatures of the geothermal systems 592 but this seems marginal as little active volcanism is recognized in this region (Faulds et al., 593 2010).

595 6. CONCLUSIONS

596 3-D numerical experiments show that the mantle flow and shear heating resulting from slab retreat and tearing have a significant effect on Moho temperatures during 5 - 10 Myrs. Such 597 598 a mechanism induces lithospheric and crustal thermal boudinage with different wavelengths, 599 which in turn creates thermally-driven rheological contrasts that localize deformation and lead to 600 the formation of crustal-scale permeable detachments. These structures allow for the exhumation 601 of MCCs and for the emplacement of HEGRs comparable to those observed in the Mediterranean 602 realm and in the Western United States. Although there is no consensus on a worldwide 603 classification of geothermal systems, our results highlight the importance of the spatial and 604 temporal scales of subduction dynamics in the control of genesis of geothermal systems.

605

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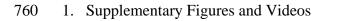
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| 758 | |
| | |

759 APPENDIX



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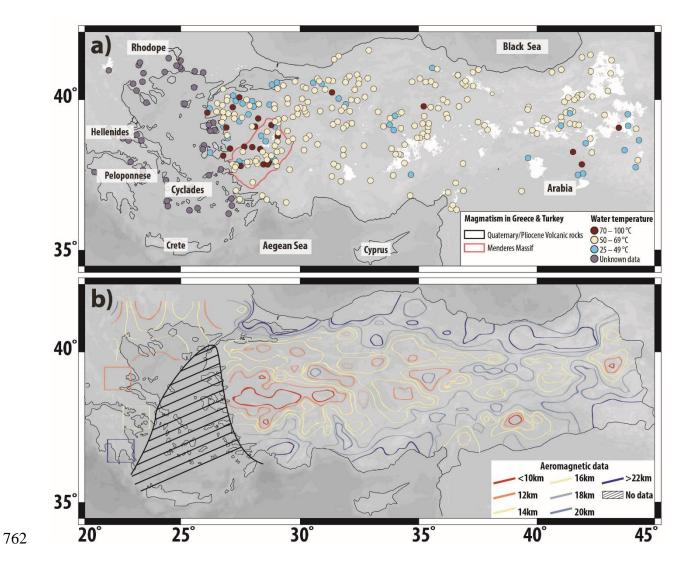


Figure S1: Maps of the Aegean-Anatolian region. (a) Geothermal map of eastern Mediterranean
region highlighting major thermal occurrences based on a compilation of several data sources
(from the MTA (2005); Mendrinos *et al.* (2010) and Andritsos *et al.* (2015)), and spatial
distribution of Pliocene-Quaternary volcanic rocks (from the geological map of the MTA). (b)

- 767 Curie-point depth map from Tselentis (1991); Stampolidis and Tsokas (2002) and Aydin *et al.*
- 768 (2005).
- 769

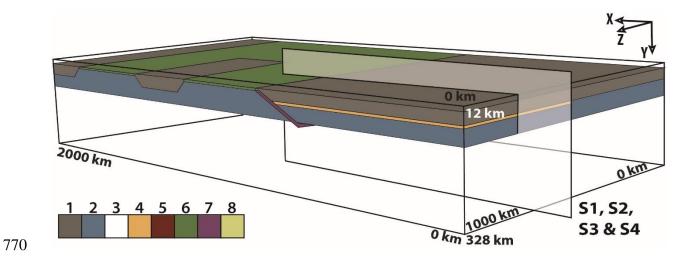
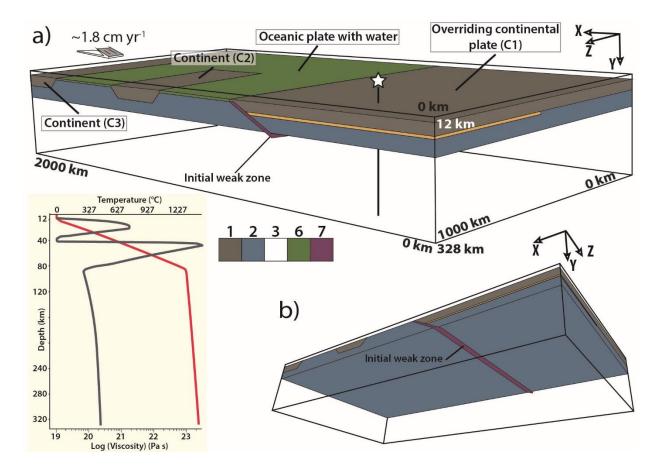


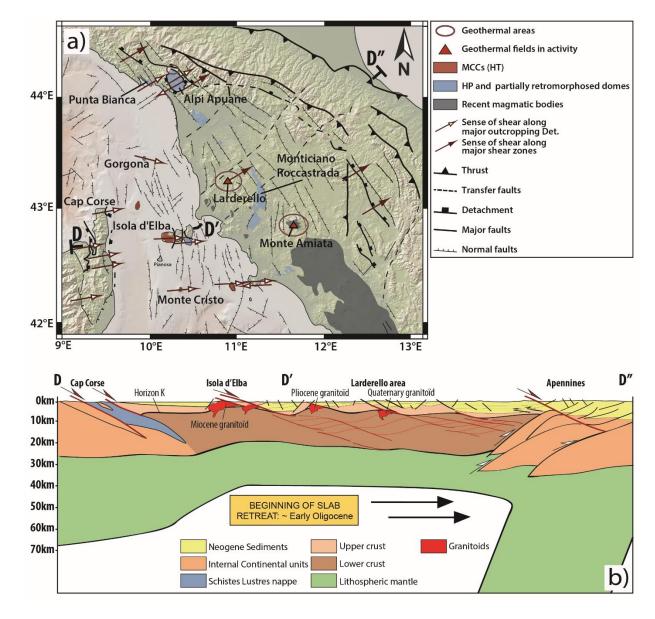
Figure S2: Location of videos shown by the vertical cross-section from our reference numerical

model. Colours showing different rock types: 1-2-3-4-5-6-7-8 as defined in Figure 3.



773

Figure S3: Experimental setup without slab tearing. (a) 3D initial model setup where the top layer ("sticky air", $y < \sim 12$ km") and the water are cut off for clarity. Colours showing different rock types as defined in Figure 3. Vertical viscosity (grey) and temperature (red) profiles at t₀, taken at the location shown by the white star. (b) Location of the "weak zone" (i.e. hydrated/serpentinized mantle) into the lithosphere to initialise subduction (z-parallel).



780

Figure S4: Simplified tectonic map showing the main metamorphic core complexes and
associated detachments faults. (a) Map of the Northern Tyrrhenian region and Northern
Apennines, modified from Jolivet *et al.* (1998). (b) Simplified cross-sections highlighting slab
retreat and formation of crustal detachments.

786 Videos S1 – S4 showing the ascent of partially molten material (the yellowish color), the thermal

domes, the composition and the second invariant of the strain rate tensor evolution, respectively.

| 788 | Note that the location of the modeled arc in our numerical model is the position of mantle |
|-----|--|
| 789 | upwellings (i.e. molten material) projected at the surface. Even if the distance between arc and |
| 790 | trench changes in time and space, note that the distance should be around $100 - 150$ km from the |
| 791 | trench toward the upper plate. |
| 792 | |
| 793 | 2. Supplementary materials |
| 794 | |
| 795 | 2.1. 3-D numerical approach |
| 796 | |
| 797 | Continuity and momentum equations |
| 798 | The code I3ELVIS uses a staggered finite difference scheme combined with the marker-in- |
| 799 | cell technique (Gerya, 2010). Lagrangian advecting markers are thus combined with an immobile |
| 800 | Eulerian grid. The incompressible continuity equation describes the conservation of mass during |
| 801 | the deformation of a continuous medium (rocks) as: |
| 802 | $div(\vec{v}) = 0,$ |
| 803 | (2) |
| 804 | where \vec{v} is the local velocity and div() is the divergence operator. |
| 805 | The conservation of momentum is obtained through the solution of the Stokes equation: |
| 806 | $\frac{\partial \sigma_{ij}'}{\partial x_j} - \frac{\partial P}{\partial x_i} + \rho g_i = 0,$ |
| 807 | (3) |
| 808 | where <i>i</i> and <i>j</i> denote the coordinate indices (i.e. x, y, z), σ' is the deviatoric stress tensor, x_i and |
| 809 | x_j are the spatial coordinates and g_i is the <i>i</i> th component of the gravity vector \vec{g} . |
| | |

811 *Heat conservation equation*

812 In order to predict changes in temperature due to heat transport, the Lagrangian heat 813 conservation equation is solved, which consider conductive heat transport, as well as internal heat 814 generation:

815
$$\rho C_p \frac{DT}{Dt} = -\frac{\partial q_i}{\partial x_i} + H,$$

816 (4)

817 where the heat flux vector \vec{q} is related to the temperature gradient in space as:

818
$$q_i = -k \frac{\partial T}{\partial x_i}.$$

819 (5)

T is temperature and *k* is the thermal conductivity of the material, which depends on pressure (*P*), T, and composition of the material. *Cp* is the isobaric heat capacity, $\frac{DT}{Dt}$ is the substantive time

derivative of temperature and *H* is the volumetric heat productions. The latter term includes
several types of heat generation/consumption processes:

$$824 \qquad H = H_r + H_s + H_a \,,$$

825 (6)

where H_r is the radiogenic heat production, H_s is the shear heating and H_a is the adiabatic heat production. H_s is related to dissipation of the mechanical energy during irreversible non-elastic (e.g. viscous) deformation. It is calculated as:

829 $H_s = \sigma'_{ij} \dot{\varepsilon}'_{ij}$,

830 (7)

831 where $\dot{\varepsilon}'$ is the strain rate tensors. H_a corresponds to heat production related to pressure changes. 832 It is calculated as:

833
$$H_a = T\alpha \frac{DP}{Dt}$$
,

834 (8)

835 where $\frac{DP}{Dt}$ is the substantive time derivative of pressure. Advection of temperature is performed 836 by using Lagrangian markers (Gerya, 2010).

837

838 Viscous rheology of rocks

839 The physical properties of rocks used in our experiments are given in Table 1. Among 840 them, the density of solid rocks depends on *P*, *T*, and composition. In our experiments, ρ_{solid} is 841 calculated as follow:

842
$$\rho_{solid} = \rho_{0solid} \left[1 + \beta (P - P_r) \right] * \left[1 - \alpha (T - T_r) \right]$$

843 (9)

844 where ρ_{0solid} is the standard density of solid rocks at reference pressure P_r (10⁵ Pa = 1 bar) and 845 temperature T_r (298.15 K = 25 °C); α and β are respectively the thermal expansion and 846 compressibility of rock. As density is also modified by phase changes (such as partial melting 847 which is implemented in this code), effective rock density ρ_{eff} is calculated as follow:

848
$$\rho_{eff} = \rho_{solid} \left(1 - M + M \frac{\rho_{0molten}}{\rho_{0solid}}\right), \tag{10}$$

849 where $\rho_{0molten}$ is the standard density of molten rock, and *M* is the volumetric melt fraction in 850 partially molten rock (see below for more information). In addition, non-Newtonian visco-plastic 851 rheologies used in our experiments are implemented by both ductile and brittle/plastic experimentally constrained laws. Effective viscosity for dislocation creep thus depends on thestrain rate, pressure and temperature. It is calculated as follow:

854
$$\eta_{creep} = \dot{\varepsilon}_{II} \frac{1-n}{n} A_D \frac{-1}{n} \exp\left(\frac{E+P V}{n R T}\right),$$

856 where $\dot{\epsilon}_{II}$ is the square root of the second invariant of the strain rate tensor, *R* is the gas constant, 857 *n* is the creep exponent, *A_D* is the pre-exponential factor, *E* is the activation energy) and *V* is the 858 activation volume. These parameters depend on the applied viscous flow law (i.e. wet quartzite, 859 plagioclase (An₇₅), dry olivine and wet olivine flow laws; Table 1) (*Ranalli*, 1995). This ductile 860 behavior is limited with a brittle/plastic one, implemented by using the Drucker-Prager criterion 861 σ_{yield} (i.e. plastic strength) (*Ranalli*, 1995) as follow:

862
$$\eta_{creep} \leq \frac{\sigma_{yield}}{2\dot{\varepsilon}_{II}},$$

863 (12)

864 where
$$\sigma_{yield}$$
 is calculated as:

865
$$\sigma_{yield} = \sigma_{\mathcal{C}} + P \sin(\varphi),$$
 (13)

where σ_c is the compressive strength of the rock, *P* is the dynamic pressure and φ is the effective internal friction angle depending on the fluid and melt presence (see details in Gerya and Meilick (2011)).

869

870 Fluid/melt dynamics: example of partial melting

871 In our experiments, partial melting process is also included. For all crustal rocks, the 872 volumetric melt fraction (M_0) is calculated as follow:

873 $M_0 = 0$ at $T < T_{solidus}$

874
$$M_0 = \frac{T - T_{solidus}}{T_{liquidus} - T_{solidus}}$$
 at $T_{solidus} < T < T_{liquidus}$

875 (14)

876 $M_0 = 1$ at $T > T_{liquidus}$

where M_0 is the volumetric fraction of melt with no previous melt extraction, $T_{solidus}$ and $T_{liquidus}$ 877 878 are, respectively, the solidus and liquidus temperatures depending on the pressure and rock 879 composition (Table 1). For the mantle, the degree of partial melting depends on the water 880 content according to the parameterization of Katz et al. (2003). Resulting partially molten 881 rocks can then undergo a succession of melt extraction episodes depending on their melt 882 extraction threshold M_{max} and non-extractable melt fraction M_{min} , both equal to 1%. Only the 883 exceeding volumetric melt fraction (i.e. > 1 %) is then extracted from partially molten rocks, 884 thus generating magma markers. For each extraction episode, the melt fraction M_{ext} recorded in the partially molten rock markers is calculated as: 885

886 $M_{ext} = M - M_{min}$,

887 (15)

where M is the volumetric melt fraction in partially molten rock, accounting for previous meltextraction events. It is calculated as:

 $890 \qquad M = M_0 - \Sigma M_{ext},$

891 (16)

where ΣM_{ext} is the total melt fraction from previous extraction episodes. Then, *M* varies dynamically until remaining solid rock is no longer able to undergo additional partial melting (i.e. $\Sigma M_{ext} > M_0$). Magma markers resulting from these extraction episodes are then instantaneously transmitted to the surface as free melt is assumed to propagate upward much faster than rocks deform (Hawkesworth, 1997).

| Material | k | Hr | ρo | CP | Ea | Va | α | β | n | ηο | Viscous | sin (Φ _{eff}) |
|-----------------------|--------------------------------------|-----------------------|-----------------------|---------------------------------------|-------------------------|-------------------------------------|--------------------|-----------------------|-----|-----------------------|----------|-------------------------|
| | (W m ⁻¹ K ⁻¹) | (mW m ⁻³) | (kg m ⁻³) | (J kg ⁻¹ K ⁻¹) | (kg mol ⁻¹) | (m ³ mol ⁻¹) | (K ⁻¹) | (kbar ⁻¹) | | (Pa ⁿ s) | flow law | |
| Sticky-air | 20 | 0 | 1 | 100 | 0 | 0 | 0 | 0 | 1 | 1x10 ¹⁹ | Air | 0 |
| Water | 20 | 0 | 1000 | 3330 | 0 | 0 | 0 | 0 | 1 | 1x10 ¹⁹ | Water | 0 |
| Sediment | 0.64+807/(T+77) | 2 | 2600 | 1000 | 154 | 8 | 3x10 ⁻⁵ | 1x10 ⁻³ | 2.3 | 1.97x10 ¹⁷ | Wet Qz. | 0.15 |
| Cont. Crsut (C1 & C3) | 0.64+807/(T+77) | 2 | 2750 | 1000 | 154 | 8 | 3x10 ⁻⁵ | 1x10 ⁻³ | 2.3 | 1.17x10 ¹⁷ | Wet Qz. | 0.15 |
| Cont. Crsut (2) | 1.18+807/(T+77) | 2 | 2950 | 1000 | 238 | 8 | 3x10 ⁻⁵ | 1x10 ⁻³ | 3.2 | 4.8x10 ²² | Wet Qz. | 0.15 |
| Oc. Crust | 1.18+474/(T+77) | 0.25 | 3000 | 1000 | 238 | 8 | 3x10 ⁻⁵ | 1x10 ⁻³ | 3.2 | 4.8x10 ²² | Wet Qz. | 0.15 |
| Mantle | 0.73+1293/(T+77) | 0.02 | 3300 | 1000 | 532 | 8 | 3x10 ⁻⁵ | 1x10 ⁻³ | 3.5 | 3.98x10 ¹⁶ | Dry Ol. | 0.6 |
| Weak zone | 0.73+1293/(T+77) | 0.05 | 3300 | 1000 | 47 | 8 | 3x10 ⁻⁵ | 1x10 ⁻³ | 4 | 5x10 ²⁰ | Wet OI. | 0 |

897

Table 1: Material properties used in the numerical experiments. k denotes the thermal conductivity, H_r is the radiogenic heat production, ρ_0 is the density, C_p is the specific heat capacity, E_a is the activation energy, V_a is the activation volume, α is the thermal expansion, β is the compressibility coefficient, n is the stress exponent, η_0 is the reference viscosity and Φ_{eff} is the effective internal friction angle. Qz. and Ol. correspond to the abbreviations of Quartzite and Olivine.

905 **2.2. 2-D numerical approach**

906

The numerical model presented in Figures 7 and 8 has been built on the same basis as those published by Guillou-Frottier *et al.* (2013). Darcy's law is coupled with the heat equation in a porous medium and with mass conservation. We have used the Comsol MultiphysicsTM software, where temperature-dependent properties can be easily implemented. Benchmark experiments have already been performed and published (Garibaldi *et al.*, 2010).

The numerical mesh consisted in more than 32,000 triangles, with a maximum size of 40 m within the detachment. Petrophysical properties are given in Table 2. Fluid density law was chosen to fit the experimental data for pure water between 20 and 350 °C:

915 $\rho_L(T) = 1002.4 - 0.1905 * T - 0.0025 * T^2$

916 (17)

917 where T is temperature in °C and ρ_L the fluid density in kg m⁻³. For temperature greater than 918 350°C, fluid density is assigned a constant value of 630 kg m⁻³. This choice has no fundamental 919 consequences on the results since at these high temperatures, fluid is located at depth greater than 920 5 km, where permeability does not allow fluid circulation. For the fluid dynamic viscosity, the 921 law used has been written as:

922
$$\mu(T) = 2.414 \ 10^{-5} \times \exp\left(\frac{570}{T+133}\right)$$

923 (18)

924 where T is in °C and dynamic viscosity μ is in Pa s.

925 The initial pressure field increases linearly with depth. The initial temperature field is 926 computed in a conductive regime, such that the surface temperature is 20 °C and the bottom of 927 the box (10 km depth) is close to 500 °C, as it is suggested by Aydin et al. (2005). To reach a temperature around ~ 500 °C at a depth of 10 km, a basal heat flow of 120 mW m⁻² is imposed 928 929 during the transient behaviour. At t > 0, permeability values (see Table 2) are affected to the two 930 units, and transient evolution of temperature and velocity fields are recorded. The chosen permeability law accounts for depth-dependence reaching a low value (~ 10^{-18} m²) at the brittle-931 932 ductile transition, as suggested by Violay et al. (2017).

| | Basement | Detachment |
|-------------------------------------|---|-------------------------|
| Eq. thermal conductivity(*) | 2.8 | 1.6 |
| Porosity (%) | 5 | 30 |
| Permeability (**) (m ²) | $[10^{-17} - 10^{-14}]exp((z-2000)/1000)$ | $[10^{-17} - 10^{-14}]$ |

| | Heat production (µW.m ⁻³) | 0 | |
|-----|---|-----------------|-------|
| | 1.0 | 0 | |
| 933 | Table 2: Material properties used in the numerical experiments. (*) the end | quivalent the | ermal |
| 934 | 4 conductivity accounts for solid matrix and fluid-filled pores. (**) perme | eability decre | eases |
| 935 | 5 exponentially with depth, except in the detachment. | | |
| 936 | 5 | | |
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