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Triangular Spectral Element simulation of two-dimensional elastic wave propagation using unstructured triangular grids

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SUMMARY

A Triangular Spectral Element Method (TSEM) is presented to simulate elastic wave propagation using an unstructured triangulation of the physical domain. TSEM makes use of a variational formulation of elastodynamics based on unstructured straight-sided triangles that allow enhanced flexibility when dealing with complex geometries and velocity structures. The displacement field is expanded into a high-order polynomial spectral approximation over each triangular subdomain. Continuity between the subdomains of the triangulation is enforced using a multidimensional Lagrangian interpolation built on a set of Fekete points of the triangle. High-order accuracy is achieved by resorting to an analytical computation of the associated internal product and bilinear forms leading to a non-diagonal mass matrix formulation. Therefore, the time stepping involves the solution of a sparse linear algebraic system even in the explicit case. In this paper the accuracy and the geometrical flexibility of the TSEM is explored. Comparison with classical spectral elements on quadrangular grids shows similar results in terms of accuracy and stability even for long simulations. Surface and interface waves are shown to be accurately modelled even in the case of complex topography with the TSEM. Numerical results are presented for 2-D canonical examples as well as more specific problems, such as 2-D elastic wave scattering by a cylinder embedded in an homogeneous half-space. They all illustrate the enhanced geometrical flexibility of the TSEM. This clearly suggests the need of further investigations in computational seismology specifically targeted towards efficient implementations of the TSEM both in the time and the frequency domain.

Key words: elastic waves, numerical simulation, spectral element method, triangular unstructured grids.

1 INTRODUCTION

Many problems in geophysics need to infer the physical and chemical parameter distributions of the Earth's interior from information provided by seismic wave propagation through complex media. Moreover, numerical simulations of earthquake-induced wave propagation within heterogeneous geological structures have important implications in terms of earthquake risk assessment and of strong motion predictions. Continuous improvements during the last decades, both in terms of acquisition techniques and seismic network density, lead today the possibility of exploiting new information provided by high-resolution multicomponent seismograms, over a wide range of frequencies. The development of new seismic interpretation methods, which take advantage of these high-resolution

observations, requires accurate numerical modelling tools for the simulation of the complete waveform field in heterogeneous geological media with complex geometries.

Recent developments towards high-order numerical modelling of seismic wave propagation (Seriani *et al.* 1992; Maggio *et al.* 1996; Faccioli *et al.* 1997; Komatitsch & Vilotte 1998; Komatitsch *et al.* 1999; Komatitsch & Tromp 1999; Komatitsch *et al.* 2000, 2001; Chaljub *et al.* 2003; Capdeville *et al.* 2003; Komatitsch *et al.* 2004) have been based on spectral element techniques (Patera 1984; Maday & Patera 1989; Bernardi & Maday 1992). There are several reasons for using spectral elements in computational seismology. First, by means of piecewise continuous geometrical maps, spectral elements have higher geometrical flexibility than spectral or pseudo-spectral methods, which are mainly confined to smooth problems defined on simple domains that can be mapped onto the n_d -cube (where n_d is the space dimension), while retaining the spatial exponential convergence for locally smooth solutions with quasi-optimal dispersion errors. Second, like low-order finite elements, spectral elements are based on the weak form of elastodynamics that involve only

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first-order spatial derivatives. The weak formulation has the nice property to handle naturally both interface continuity and free-boundary conditions, allowing very accurate resolution of evanescent interface and surface waves that are of major interest in seismology. Finally, spectral elements are much easier to implement than global spectral methods on today's generation parallel computers, which involve non-uniform distributed access to the memory.

Previous work with spectral element method (SEM) in computational seismology typically used explicit time stepping and quadrilateral elements, with a clever choice of the polynomial basis for the function expansion based on the Legendre family of Jacobi polynomials, and with a set of non-uniform collocation points defined as the Gauss–Lobatto–Legendre (GLL) cardinal points with the associated quadrature. Moreover, quadrangles allow the use of a tensor product to construct the Lobatto–Legendre cardinal interpolation basis (Bernardi & Maday 1992; Deville *et al.* 2002) in such a way that the mass matrix remains diagonal with a time-step restriction scaling as $\mathcal{O}(N^{-2})$, where N is the order of the polynomial basis, while the derivatives can be calculated using an efficient sum-factorization technique (Orszag 1980) at a cost of only $\mathcal{O}(EN^\alpha)$ with $\alpha = 3$ and $\alpha = 4$ for 2-D and 3-D problems, respectively, and E the number of elements. Apart from that, this method inherits the nice property of the associated GLL quadrature allowing for the exact integration of polynomial functions of order $2N - 1$, with only $N + 1$ points. Finally, straightforward C^0 continuity of the kinematic field can be insured while using conforming quadrangle meshes thanks to the local conforming maps and the cardinal Lobatto–Legendre interpolation basis.

The need for geometric flexibility is especially important in computational seismology when dealing with complex wave phenomena, such as the scattering by rough topographies of the Earth and sea bottom surfaces, or the seismic response of sedimentary basins with complex structures and fault geometries. Today, such flexibility is hardly achieved when using quadrangles for several reasons. First, when using non-conforming grids, continuity between mismatched elements must be enforced in a variational sense by resorting to the so-called mortar method (Bernardi *et al.* 1994; Ben Belgacem 1999), which adds both programming complexity and operation costs. Second, when resorting to unstructured meshes, that is meshes referenced using only one index, very few robust grid-generation software based on hexahedra are available today and all of them have difficulties to handle rapid multiscale mesh refinements and de-refinements. Third, the stability of explicit numerical schemes can be strongly affected when using quadrangles that are highly skewed, leading to non-uniform resolution and severe time-step restrictions. Higher geometrical flexibility is, therefore, a strong motivation for exploring the use of triangular elements and unstructured meshes, an extension that has been investigated by *hp*-finite element methods in these last decades using multivariate Lagrangian interpolation (Chen & Babuska 1995).

Extension of SEMs to unstructured triangular meshes hinges upon the application of more complex polynomial basis specifically tailored to accurately approximate smooth functions defined on the n_d -simplex. Drawing on ideas from Orszag's work on spherical harmonics (Orszag 1974), and on orthogonal polynomial basis initially derived by Proriot (1957) and Koorwinder (1975), Dubiner (1991) first overcame these difficulties and obtained a tensor-product-like spectral method for triangles based on Jacobi polynomials. In the construction of such orthogonal polynomial basis, Dubiner makes use of a non-rotational collapsed coordinate system, induced by the mapping of each triangular region to a rectangle, and of the generalization of the direct tensor products by the so-called warped

tensor product. Dubiner's basis has been extended to incompressible Navier–Stokes equations in 3-D by Sherwin & Karniadakis (1995a,b); Karniadakis & Sherwin (1999), and to geophysical fluid dynamics problems by Wingate & Boyd (1996).

One possible approach relies on a modal hierarchical approximation that has been extensively investigated by Sherwin & Karniadakis (1995a,b, 1996); Karniadakis & Sherwin (1999). This approach makes use of an almost orthogonal approximation basis, based on the modification of the original Dubiner's basis, which separate interior and boundary contributions, in order to insure C^0 continuity between the triangular subdomains. This so-called modified Dubiner's basis (Dubiner 1991), and its interior-orthogonal variant (Wingate & Boyd 1996), makes use of a triangular polynomial truncation in modes $\{x^n y^m, m + n \leq N\}$, where N is the global polynomial order of the expansion, together with an efficient warped tensor product and a Gauss-type quadrature formula defined on a squared-grid of points. This allows the backward transform to be still computed in $\mathcal{O}(EN^4)$ in 3-D, and the forward transformation in $\mathcal{O}(EN_q)$, where N_q is the order of the quadrature. All the computations are done in the modal space. However in practice, as noted in Hesthaven & Teng (2000), the quadrature formula is oversampled, it uses more grid points than required by the order of the polynomial basis. Even though the added complexity in the expression of the modified basis allows for C^0 continuity between the triangular elements, such a construction still depends on the orientation of the local coordinate system of the contributing elements. Moreover, the partial orthogonality of the basis destroys much of the sparsity of the SEM matrices and leads to a non-diagonal mass matrix (Warburton *et al.* 1999).

We investigate a second approach based on a nodal approximation (Taylor *et al.* 2000; Warburton *et al.* 2000; Hesthaven & Teng 2000; Bos *et al.* 2001). As in classical SEM, resorting to multivariate Lagrange polynomial interpolation allows straightforward C^0 continuity between triangular elements. It is worth noting here that a modal expansion can always be represented as a Lagrange polynomial expansion of equivalent order, defined on an appropriate set of points, a fact efficiently used in classical SEM on the n_d -cube. The central part is however the identification of an appropriate set of nodal points on the n_d -simplex that ensures good behaviour of the interpolating polynomials. While, in contrast to the n_d -cube, the identification of an optimal set of nodal points remains an open problem in the general case, significant progress has been recently made (Chen & Babuska 1995, 1996; Taylor & Wingate 2000; Warburton *et al.* 2000; Hesthaven & Teng 2000; Heinrichs 2005; Blyth & Pozrikidis 2005), that allows for the construction of well-behaved high-order approximations of smooth functions defined on the n_d -simplex. Unfortunately, these approximations have no underlying tensor-product construction. The computational complexity, for example, the spatial derivatives computation, scales asymptotically as $\mathcal{O}(EN^{2n_d})$, which becomes prohibitive for large N . However, for small values of N as used in classical SEM, for example, $N \leq 8$, the formulation can still be efficient.

Another important issue is the structure of the associated weight matrix. Classical SEM applications in computational seismology are generally explicit and make efficient use of the discrete orthogonality of the Lagrangian basis on the n_d -cube with respect to the inherited GLL discrete inner product. In the case of the Triangular Spectral Element Method (TSEM), such an interesting property can only be preserved by resorting to a quadrature formula using the same grid of nodal points than the one used to define the Lagrangian interpolation basis at the cost of a low-order quadrature. This accuracy loss in the weight matrix has been shown (Komatitsch *et al.*

2001) to produce unacceptable dispersion errors in the simulation of elastic wave propagation.

Here, we explore the use of the unstructured triangle based SEM introduced in Taylor & Wingate (2000) and Warburton *et al.* (2000), relying on the use of the Dubiner's polynomials (Koorwinder 1975; Dubiner 1991) and multivariate Lagrangian interpolation based on Fekete points (Taylor & Wingate 2000; Hesthaven & Teng 2000), for 2-D seismological applications in time domain with special attention to dispersion errors. It is worth mentioning similar type of studies that have been recently conducted independently by Pasquetti & Rapetti (2004) in the context of Helmholtz equations, and Giraldo & Warburton (2005) in geophysical fluid dynamics. The organization of the paper is as follows. After introducing the elastodynamic problem and its variational formulation in Section 2, Section 3 presents the geometrical and functional discretization of the problem within the context of triangular spectral elements, and some of the actual issues of the TSEM formulation are reviewed. The TSEM is first explored in Section 4 by solving canonical examples of 2-D elastic wave propagation allowing for comparisons with analytical solutions and classical SEM solutions. Finally more realistic 2-D numerical examples, such as the scattering by an elastic cylinder in a homogeneous half-space, and the elastic wave propagation in a layered medium are provided in Section 5 to illustrate the enhanced geometrical flexibility of the TSEM. The paper ends up with a discussion of further research directions.

2 THE ELASTODYNAMIC PROBLEM

Let us consider an elastic medium occupying an open domain $\Omega \subset \mathbb{R}^{n_d}$ bounded by a smooth boundary $\partial\Omega$ with $\bar{\Omega} = \Omega \cup \partial\Omega$, and a time interval of interest $\mathbb{I} = [0, T] \subset \mathbb{R}_+$. The displacement field is denoted by $\mathbf{u} : \Omega \times \mathbb{I} \rightarrow \mathbb{R}^{n_d}$, and the velocity field by $\mathbf{v}(\mathbf{x}, t) = \dot{\mathbf{u}}(\mathbf{x}, t)$ where the dot symbol indicates a differentiation with respect to time.

The Euler–Lagrange equations of elastodynamics may be written as

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \text{div}[\boldsymbol{\sigma}] + \mathbf{f}, \quad (1)$$

with the initial conditions

$$\mathbf{u}(\mathbf{x}, 0) = \mathbf{u}_0(\mathbf{x}) \quad \text{and} \quad \mathbf{v}(\mathbf{x}, 0) = \mathbf{v}_0(\mathbf{x}), \quad (2)$$

and, for sake of simplicity, let us consider only the following free-surface boundary condition

$$\boldsymbol{\sigma}(\mathbf{x}, t) \cdot \mathbf{n}(\mathbf{x}) = 0 \quad \text{on } \partial\Omega, \quad (3)$$

where $\rho(\mathbf{x})$ denotes the reference mass density. The symmetric Cauchy stress tensor is denoted by $\boldsymbol{\sigma} : \bar{\Omega} \times \mathbb{I} \rightarrow \mathbb{S} \subset \mathbb{R}^{n_d \times n_d}$ where \mathbb{S} is the subspace of symmetric second-order tensors of dimension $n_d(n_d + 1)/2$. For linear elastic medium,

$$\boldsymbol{\sigma} = \mathbf{C} : \boldsymbol{\epsilon} = \mathbf{C} : \nabla \mathbf{u}, \quad (4)$$

where the linearized elastic stiffness tensor $\mathbf{C}(\mathbf{x})$ is symmetric, with minor and major symmetries, and positive definite restricted to \mathbb{S} . The infinitesimal strain tensor is denoted $\boldsymbol{\epsilon} \in \mathbb{S}$ and is defined as,

$$\boldsymbol{\epsilon}[\mathbf{u}] \doteq \nabla^s \mathbf{u} = \frac{1}{2} [\nabla \mathbf{u} + (\nabla \mathbf{u})^T]. \quad (5)$$

Although the method can be applied to general anisotropic media, in the present work only linear isotropic elasticity will be considered,

$$C_{ijkl} = \lambda \delta_{ij} \delta_{kl} + \mu (\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk}), \quad (6)$$

with λ and μ the Lamé constants of the medium.

Finally, in the following \mathbf{f} is either a collocated force,

$$\mathbf{f}(\mathbf{x}, t) = \mathbf{F} \delta(\mathbf{x} - \mathbf{x}_s) G(t - t_0), \quad (7)$$

where $\mathbf{F} \in \mathbb{R}^{n_d}$ is the vector of the force amplitude components; or a generalized body force, that is, it can be expressed as $\mathbf{f} = \text{div}[\mathbf{m}]$, where $\mathbf{m} \in \mathbb{S}$ is the symmetric second-order moment tensor, with classically

$$\mathbf{m}(\mathbf{x}, t) = -\mathcal{M} \delta(\mathbf{x} - \mathbf{x}_s) G(t - t_0), \quad (8)$$

where $\mathcal{M} \in \mathbb{S}$, $\delta(\cdot)$ is the Dirac delta function, and $G(\cdot)$ the source time function.

A variational formulation of the elastodynamic problem can be obtained by introducing the space of admissible kinematic fields (displacement or velocity) fields, as

$$\mathcal{S}_t := \{\mathbf{u}(\mathbf{x}, t) : \Omega \times \mathbb{I} \rightarrow \mathbb{R}^{n_d} \mid \mathbf{u} \in H^1(\Omega)^{n_d}, \forall t \in \mathbb{I}\}, \quad (9)$$

where $H^1(\Omega)^{n_d}$ denotes the space of vector fields defined on Ω that are square integrable and have square integrable first-order partial derivatives in space, over the domain Ω . Considering the associated space of kinematic field variations at each time t , $\delta\mathcal{S} := \{\mathbf{w}(\mathbf{x}) : \Omega \rightarrow \mathbb{R}^{n_d} \mid \mathbf{w} \in H^1(\Omega)^{n_d}\}$, the variational formulation leads to search for $\mathbf{u} \in \mathcal{S}^t$ such that $\forall \mathbf{w} \in \delta\mathcal{S}$ and $\forall t \in \mathbb{I}$

$$\left(\mathbf{w}, \rho \frac{\partial^2 \mathbf{u}}{\partial t^2} \right) = (\mathbf{w}, \mathbf{f}) - \mathcal{A}(\mathbf{w}, \mathbf{u}), \quad (10)$$

with the initial conditions

$$(\mathbf{w}, \mathbf{u}(\mathbf{x}, 0)) = (\mathbf{w}, \mathbf{u}_0) \quad \text{and} \quad (\mathbf{w}, \mathbf{v}(\mathbf{x}, 0)) = (\mathbf{w}, \mathbf{v}_0), \quad (11)$$

and where the inner products refer to standard L^2 and energy inner products:

$$(\mathbf{w}, \mathbf{u}) = \int_{\Omega} \mathbf{w} \cdot \mathbf{u} \, d\Omega, \quad \mathcal{A}(\mathbf{w}, \mathbf{u}) = \int_{\Omega} \nabla \mathbf{w} : \mathbf{C} : \nabla \mathbf{u} \, d\Omega.$$

3 DISCRETIZATION OF THE ELASTODYNAMIC PROBLEM

In the following, for sake of simplicity, we shall restrict the presentation to the 2-D case even though generalization to 3-D is straightforward.

3.1 Geometrical discretization

The original physical domain $\bar{\Omega}$ is approximated by a decomposition into n_e non-overlapping polygonal subdomains $\bar{\Omega}_e$ as

$$\bar{\Omega} \approx \bar{\Omega}^h = \bigcup_{e=1}^{n_e} \bar{\Omega}_e \quad \text{and} \quad \Omega_e \cap \Omega_{e'} = \emptyset \text{ if } e \neq e'. \quad (12)$$

While classical SEM are based on a quadrangular domain decomposition, we shall assume here a domain decomposition based on simple straight-sided subdomains $\bar{\Omega}_e$ allowing for a conforming unstructured triangulation \mathcal{T}_h of $\bar{\Omega}$. It is worth noting here that such a triangulation is consistent with most of the modelling tools used in subsurface geophysics and allows to handle complex geological structures.

Straight-sided triangular subdomains $\bar{\Omega}_e \in \mathcal{T}_h(\bar{\Omega})$ can be linearly transformed, see Fig. 1, into the reference simplex,

$$\mathcal{T}^2 = \{(r, s) \in \square \mid r + s \leq 0\}, \quad (13)$$

where $\square = \Lambda \times \Lambda$, with $\Lambda = [-1, 1]$, is the unit quadrangle. The

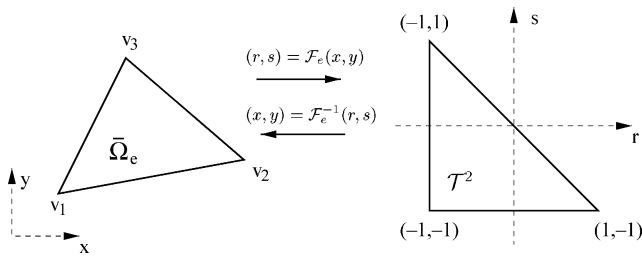


Figure 1. Affine transformation \mathcal{F}_e from an arbitrary straight-sided triangular element $\bar{\Omega}_e$ to the reference simplex \mathcal{T}^2 .

locally compatible invertible map $\mathcal{F}_e: \bar{\Omega}_e \rightarrow \mathcal{T}^2$, is an affine map defined as

$$\mathbf{x}(r, s) = \mathcal{F}_e^{-1}(r, s) = -\frac{(r+s)}{2}\mathbf{v}_1 + \frac{(1+r)}{2}\mathbf{v}_2 + \frac{(1+s)}{2}\mathbf{v}_3, \quad (14)$$

where $\mathbf{v}_1, \mathbf{v}_2, \mathbf{v}_3$ are the position vectors of the three vertices of $\bar{\Omega}_e$. It is worth noting here that such a map yields to a constant Jacobian $J_e = |\frac{\partial(\mathbf{x}, \mathbf{y})}{\partial(r, s)}|$ over each subdomain, an essential feature for the remaining.

The variational formulation of the elastodynamics can be restated by simply replacing $\bar{\Omega}$ with $\mathcal{I}_h(\bar{\Omega})$, together with the inner products:

$$\begin{aligned} (w, u) &= \sum_{e=1}^{n_e} \int_{\bar{\Omega}_e} \mathbf{w}^e \cdot \mathbf{u}^e d\Omega, \\ \mathcal{A}(w, u) &= \sum_{e=1}^{n_e} \mathcal{A}^e(\mathbf{w}^e, \mathbf{u}^e) = \sum_{e=1}^{n_e} \int_{\bar{\Omega}_e} \nabla \mathbf{w}^e : \mathbf{C} : \nabla \mathbf{u}^e d\Omega, \end{aligned} \quad (15)$$

where \mathbf{u}^e and \mathbf{w}^e denotes the restriction of \mathbf{u} and \mathbf{w} , respectively, to $\bar{\Omega}_e$, that is $\mathbf{u}^e := \mathbf{u}|_{\bar{\Omega}_e}: \bar{\Omega}_e \times \mathbb{I} \rightarrow \mathbb{R}^{nd}$.

3.2 Piecewise polynomial approximation

Associated with the triangulation \mathcal{I}_h , let us consider a piecewise polynomial approximation of the kinematic fields with the finite dimensional subspaces

$$S_t^h \subset S_t = \{\mathbf{u}^h \in S_t, \text{ and } \mathbf{u}^h|_{\bar{\Omega}_e} \circ \mathcal{F}_e \in \mathbb{P}_N(\mathcal{T}^2)\}, \quad (16)$$

$$\delta S^h \subset \delta S = \{\mathbf{w}^h \in \delta S, \text{ and } \mathbf{w}^h|_{\bar{\Omega}_e} \circ \mathcal{F}_e \in \mathbb{P}_N(\mathcal{T}^2)\}, \quad (17)$$

where $\mathbb{P}_N(\mathcal{T}^2)$ denotes the space of polynomials of degree less or equal to N and defined on the reference simplex \mathcal{T}^2 , that is,

$$\mathbb{P}_N(\mathcal{T}^2) = \{r^n s^m; n, m \geq 0, n + m \leq N\}. \quad (18)$$

An appropriate starting point in developing the multidimensional expansion is to construct a system of orthogonal polynomials, with respect to the L^2 inner product, on the reference simplex \mathcal{T}^2 . Interest in orthogonal polynomials originates from the fact that they naturally define a complete basis and allow for a straightforward computation of their derivatives.

In classical SEM this is readily achieved by resorting to a tensor product construction of one-dimensional Jacobi polynomials $p_n^{\alpha, \beta}$ of degree n , depending of two real parameters α and β with $\alpha, \beta > -1$ (Abramowitz & Stegun 1972). These are the only polynomial eigenvalue solutions of a singular Sturm–Liouville problem over Λ , allowing for spectral accuracy as shown by Gottlieb & Orszag (1977). Such a tensor product construction is rooted in the bounded definition of the reference domain $\square = \Lambda \times \Lambda$ in a Cartesian coordinate system. However, the reference simplex domain \mathcal{T}^2 does

not naturally inherit that property since the bounds of the Cartesian coordinates (r, s) are dependent on each other.

To develop a suitable tensorial type basis for unstructured triangular regions, a new coordinate system is introduced where local coordinates have independent bounds. This can be achieved while using the so-called collapsed coordinate system Karniadakis & Sherwin (1999), a non-rotational coordinate system resulting from the singular mapping,

$$\eta = 2 \frac{(1+r)}{(1-s)} - 1, \quad (19)$$

$$\zeta = s, \quad (20)$$

with like in classical SEM,

$$\mathcal{T}^2 = \{(\eta, \zeta) \mid (\eta, \zeta) \in \square\}. \quad (21)$$

Such a mapping introduces a non-physical singularity at $(-1, 1)$ much like cylindrical or spherical coordinate systems.

3.2.1 Spectral expansion

Drawing on ideas from Orszag's work on spherical harmonics (Orszag 1974), Dubiner (1991) first constructed an orthogonal polynomial basis in two dimensions that takes advantage of the orthogonality of Jacobi polynomials and which was further extended to 3-D by Sherwin & Karniadakis (1995a), Karniadakis & Sherwin (1999). Dubiner's basis has been shown to be related to the polynomial solution of a separable Sturm–Liouville eigenvalue problem defined on \mathcal{T}^2 achieving spectral accuracy (Owens 1998). Dubiner's orthogonal basis is given by

$$\Phi_{nm}(r(\eta), s(\zeta)) = p_n^{0,0}(\eta) \left(\frac{1-\zeta}{2} \right)^n p_m^{2n+1,0}(\zeta), \quad (22)$$

where (η, ζ) are the collapsed coordinates, and by definition $p_k^{\alpha, \beta}$ is the k th-order Jacobi polynomial defined on Λ and orthogonal with respect to L_w^2 inner product,

$$\langle p_k^{\alpha, \beta}, p_l^{\alpha, \beta} \rangle^w = \int_{\Lambda} w(x) p_k^{\alpha, \beta} p_l^{\alpha, \beta} dx = \delta_{kl} h_k^{\alpha, \beta}, \quad (23)$$

with

$$w(x) = (1-x)^\alpha (1+x)^\beta, \quad (24)$$

$$h_k^{\alpha, \beta} = \frac{2^{\alpha+\beta+1}}{2k+\alpha+\beta+1} \frac{\Gamma(k+\alpha+1)\Gamma(k+\beta+1)}{k! \Gamma(k+\alpha+\beta+1)}, \quad (25)$$

where $\Gamma(\cdot)$ denotes the Gamma function (Abramowitz & Stegun 1972).

The basis may be cast as the product of two polynomials in the (η, ζ) coordinates

$$\Phi_{nm}(r, s) = \Phi_n^1(\eta) \Phi_{nm}^2(\zeta), \quad (26)$$

where $\Phi_n^1(\eta) = p_n^{0,0}(\eta)$ is the Legendre polynomial of degree n , and $\Phi_{nm}^2(\zeta) = \left(\frac{1-\zeta}{2} \right)^n p_m^{2n+1,0}(\zeta)$ a polynomial introduced to maintain the orthogonality of the triangular basis. The Jacobi polynomial $p_k^{\alpha,0}$ has zeros that are declustered away from $\zeta = -1$ for increasing α , an important feature for maintaining the linear independence of the expansion and for well-conditioning numerical systems (Karniadakis & Sherwin 1999). Such factorization of 2-D functions, as the product of a principal function Φ_n^1 and a tensorial function Φ_{nm}^2 different for each principal function, is referred by Dubiner as a warped tensor product and results from the decomposition of the commutative algebra over \mathcal{T}^2 into two independent

linear subspaces. The warped product construction is an extension of the classical direct tensor product that retains the numerical efficiency of the sum-factorization process. The set of polynomials Φ_{nm} defined a complete orthogonal polynomial basis with respect to the uniform Legendre inner product thanks to the factor $(\frac{1-\zeta}{2})^n$,

$$\langle \Phi_{pq}, \Phi_{kl} \rangle_{T^2} = \int_{-1}^1 \int_{-1}^{-s} \Phi_{pq}(r, s) \Phi_{kl}(r, s) dr ds = \gamma_{pq} \delta_{pk} \delta_{ql}, \quad (27)$$

with the normalization constant,

$$\gamma_{pq} = \frac{2}{(2p+1)(p+q+1)}. \quad (28)$$

Let us consider $\mathbb{P}_N(T^2) = \text{span}\{\Phi_{nm}\}_{(n,m) \in M}$, where $M = \{(n, m); 0 \leq n, m \leq N, n+m \leq N\}$. The cardinality of this set is $\mathcal{N} = (N+1)(N+2)/2$, and the truncated spectral expansion $P_N u$ at degree N of any function $u \in L^2(T^2)$ is given by

$$P_N u(r, s) = \sum_{n=0}^N \sum_{m=0}^{N-n} \hat{u}_{nm} \Phi_{nm}(r, s), \quad (29)$$

where $\{\hat{u}_{nm}\}_{(n,m) \in M}$ denotes the modal coefficients of the spectral expansion of u in the Dubiner's basis. Taking into account the orthogonality relationship, yields to the relations $\hat{u}_{nm} = \frac{1}{\gamma_{nm}} \langle u, \Phi_{nm} \rangle_{T^2}$, and $\langle u - P_N u, \Phi \rangle_{T^2} = 0, \forall \Phi \in \mathbb{P}_N(T^2)$ which simply express that $P_N u$ is the orthogonal projection of u onto $\mathbb{P}_N(T^2)$ with respect to the Legendre inner product.

3.2.2 Lagrangian interpolation

The orthogonality of the previous Dubiner's basis is attractive, but the impact of using such spectral expansion is that all modes are needed to evaluate $P_N u$ pointwise. Moreover, for the actual resolution of the elastodynamic problem such an expansion has to be tessellated while maintaining a C^0 continuity between subdomains of the triangulation \mathcal{T}_h and boundary conditions must be approximated. This is not easily handled using the modal spectral expansion, and requires splitting into interior and boundary modal contributions with the penalty that the modified expansion basis becomes only semi-orthogonal and leads to higher computational complexity (Sherwin & Karniadakis 1995a; Wingate & Boyd 1996).

Another possible way is to resort, like in classical SEM, to a Lagrangian interpolation approximation (Bos *et al.* 2001; Taylor *et al.* 2000; Taylor & Wingate 2000; Warburton *et al.* 2000; Hesthaven & Teng 2000) based on a set of nodes defined inside and on the edges of the reference simplex. Function continuity is easily enforced by equating coincident nodal values at the nodes shared between subdomains.

The actual construction of a multivariate Lagrangian interpolation relies on the introduction of a complete polynomial basis. Let $I_N u \in \mathbb{P}_N(T^2)$ be the multivariate Lagrangian interpolation polynomial of $u(r, s) \in L^2(T^2)$, defined by a set of \mathcal{N} nodes that we shall discuss later, then using the complete Dubiner's polynomial basis of eq. (22), we can write

$$I_N u(r, s) = \sum_{n=0}^N \sum_{m=0}^{N-n} \tilde{u}_{nm} \Phi_{nm}(r, s). \quad (30)$$

Using the interpolation condition,

$$I_N u(r_k, s_k) = u(r_k, s_k) \quad 1 \leq k \leq \mathcal{N}, \quad (31)$$

leads to the inverse discrete spectral transform (Karniadakis &

Sherwin 1999)

$$\begin{aligned} u(r_k, s_k) &= \sum_{n=0}^N \sum_{m=0}^{N-n} \Phi_{nm}(r_k, s_k) \tilde{u}_{nm} \\ &= \sum_{n=0}^N \sum_{m=0}^{N-n} V_{knm} \tilde{u}_{nm} = \sum_{j=1}^{\mathcal{N}} V_{kj} \tilde{u}_j, \end{aligned} \quad (32)$$

where in the last term an ordering of the modal coefficients \tilde{u}_j and the polynomial basis has been introduced for sake of simplicity, using a one-to-one relation $j := j(n, m)$. The generalized Vandermonde matrix V is defined by the elements $V_{kj} = \Phi_j(r_k, s_k)$. The associated discrete spectral transform which determines the modal coefficients from the prescribed function values $u(r_k, s_k)$, is therefore given as,

$$\tilde{u}_l = \sum_{k=1}^{\mathcal{N}} V_{lk}^{-1} u(r_k, s_k). \quad (33)$$

Defining the cardinal Lagrangian function basis $\{\Psi_i\}_{i=1}^{\mathcal{N}}$ of $\mathbb{P}_N(T^2)$, which satisfies $\Psi_i(r_j, s_j) = \delta_{ij}$, yields the canonical form of the interpolation polynomial

$$I_N u(r, s) = \sum_{j=1}^{\mathcal{N}} u(r_j, s_j) \Psi_j(r, s). \quad (34)$$

Combining eqs (30) and (34), and using eq. (33) leads to the genuine form of the multivariate Lagrangian interpolation functions as

$$\Psi_i(r, s) = \sum_{j=1}^{\mathcal{N}} V_{ij}^{-T} \Phi_j(r, s), \quad \text{with} \quad V_{ik}^{-T} = \frac{1}{\gamma_k} \langle \Psi_i, \Phi_k \rangle_{T^2}. \quad (35)$$

Taking into account the completeness property of the Dubiner's basis, any function of $L^2(T^2)$ can be decomposed into the formal series

$$u(r, s) = \sum_{k=1}^{\infty} \hat{u}_k \Phi_k(r, s). \quad (36)$$

Inserting the spectral expansion of eq. (36) in the right-hand side of the discrete spectral transform (33) yields

$$\begin{aligned} \tilde{u}_k &= \sum_{l=1}^{\mathcal{N}} V_{kl}^{-1} \sum_{j=1}^{\infty} \hat{u}_j V_{lj} = \sum_{j=1}^{\infty} \hat{u}_j \sum_{l=1}^{\mathcal{N}} V_{kl}^{-1} V_{lj} \\ &= \hat{u}_k + \sum_{j=\mathcal{N}+1}^{\infty} \hat{u}_j \sum_{l=1}^{\mathcal{N}} V_{kl}^{-1} V_{lj}, \end{aligned} \quad (37)$$

and, therefore

$$I_N u(r, s) = P_N u(r, s) + R_N u(r, s), \quad (38)$$

where $R_N u$ is given by

$$R_N u(r, s) = \sum_{k=0}^{\mathcal{N}} \left(\sum_{j=\mathcal{N}+1}^{\infty} \hat{u}_j \sum_{l=1}^{\mathcal{N}} V_{kl}^{-1} V_{lj} \right) \Phi_k(r, s). \quad (39)$$

The aliasing error $R_N u \in \mathbb{P}_N(T^2)$ due to the interpolation is a low-order contribution that depends on the high-order terms of the spectral expansion of u . The interpolation error can be cast as

$$\|u - I_N u\|_{T^2}^2 = \|u - P_N u\|_{T^2}^2 + \|R_N u\|_{T^2}^2. \quad (40)$$

For any function $u \in L^2(T^2)$, the error norm $\|u - I_N u\|_{T^2}$ is an upper bound of the truncation error $\|u - P_N u\|_{T^2}$ and inherits the spectral decay of Dubiner's expansion modes \hat{u}_k with respect to k .

3.2.3 Interpolation points and inner products

Actually the interpolation error may be important and a critical issue, besides the smoothness of the interpolated function, is the choice of a suitable distribution of nodal points $\{(r_k, s_k)\}_{k=1}^N$ in T^2 . For classical SEM, interpolation in the reference quadrangle \square resorts to the tensor-product construction of a Lagrangian interpolation basis of $\mathbb{P}_N(\Lambda)$ defined by $N + 1$ GLL nodes in Λ . This yields close to optimal interpolation properties, with points defined on the boundary of Λ , a key feature for ensuring C^0 continuity between subdomains and to approximate essential boundary conditions. Extension to non-tensor-product domains, like the n_d -simplex, still involves extensive search for optimal sets of interpolation points (Bos 1983, 1991; Chen & Babuska 1995, 1996; Hesthaven 1998; Taylor & Wingate 2000; Taylor *et al.* 2000; Heinrichs 2005; Blyth & Pozrikidis 2006), minimizing the constant L_N appearing in the Lebesgue inequality $|u - I_N u| \leq (1 + L_N)|u - P_N u|$ which provides a bound of the interpolation error. At this stage, a natural choice is the Fekete nodal set (Taylor *et al.* 2000). They can be computed numerically by maximizing the determinant of the Vandermonde matrix V , independently of the choice of the ambient polynomial basis. For quadrangles, Fekete points (Bos 1991; Bos *et al.* 2001) are unique and they are given by the tensor-product of GLL points. For triangles, when the Vandermonde matrix is not singular, the Fekete points have been conjectured (Bos 1991) to have a maximum number of points on the boundary of the reference simplex. These boundary points were shown (Bos 1991; Taylor *et al.* 2000) to be GLL points. This allows to enforce C^0 continuity and to use mixed conforming meshes combining triangles and quadrangles (Komatitsch *et al.* 2001). Fekete points have to be computed numerically (Bos 1983, 1991; Chen & Babuska 1995; Taylor & Wingate 2000; Taylor *et al.* 2000) and are known up to degree $N = 19$. They are not actually optimal points, for example, they do not minimize the Lebesgue constant, but exhibit a good behaviour, for example, $L_N \leq N$ and $L_N \propto \sqrt{N}$ (Taylor *et al.* 2000). Moreover, the Lagrangian functions built on Fekete points are maximum at these points.

The numerical quadrature associated with the set of interpolation points plays an essential role for collocated spectral methods. In classical SEM, the set of interpolation points and the associated numerical quadrature are built by a tensor-product construction of the GLL points defined on Λ , which allow to exactly integrate polynomials of \mathbb{P}_{2N-1} over Λ using $N + 1$ interpolation points. Together with the tensor-product construction, this allows to define a uniformly equivalent discrete inner product and a discrete orthogonality structure, an essential property that optimize the spectral transforms and lead to the popular collocated form of the SEM with a diagonal mass matrix. Today it is yet unclear, despite some interesting progress (Taylor *et al.* 2005; Heinrichs 2005; Blyth & Pozrikidis 2005), how to define Gauss–Lobatto type of quadratures for non-tensor-product domains in order to extend collocated SEM with a diagonal mass matrix to triangles.

A Newton–Cotes quadrature formula can be associated with the N Fekete points $\{(r_k, s_k)\}_{k=1}^N$. Let Ψ_k be the Lagrangian polynomials of degree N associated with the Fekete points, then the associated quadrature weights are given by

$$\begin{aligned}\omega_k &= \sum_{\alpha=1}^N \omega_{\alpha} \Psi_k(r_{\alpha}, s_{\alpha}) = \int_{T^2} \Psi_k(r, s) d\Omega \\ &= \int_{T^2} \left(\sum_{j=1}^N V_{kj}^{-T} \Phi_j(r, s) \right) \Phi_1(r, s) d\Omega = \gamma_1 V_{k1}^{-T},\end{aligned}\quad (41)$$

where the orthogonality of the Dubiner's basis has been used and Φ_1 is the uniformly constant polynomial $\Phi_1(r, s) = 1$, with $\gamma_1 = \gamma_{00} = 2$ from eq. (28). By construction, the N Fekete points and the associated weights $\{\omega_k\}_{k=1}^N$ give a formula which exactly integrates a polynomial of $\mathbb{P}_N(T^2)$, a minimal result.

In terms of the modal coefficients of the Dubiner's expansion, the L^2 inner product yields

$$\begin{aligned}\langle I_N u, I_N v \rangle_{T^2} &= \int_{T^2} I_N u(r, s) I_N v(r, s) d\Omega \\ &= \int_{T^2} \left(\sum_{j=1}^N \tilde{u}_j \Phi_j(r, s) \right) \left(\sum_{i=1}^N \tilde{v}_i \Phi_i(r, s) \right) d\Omega \\ &= \sum_{i=1}^N \tilde{u}_i \gamma_i \tilde{v}_i = \underline{\tilde{u}}^T \Gamma \underline{\tilde{v}},\end{aligned}\quad (42)$$

where Γ is the diagonal matrix that denotes the Dubiner's metric, $\Gamma_{ij} = \gamma_i \delta_{ij}$.

In terms of the Lagrangian basis built on the Fekete points, and denoting $u_i = u(r_i, s_i)$ the function evaluation at the Fekete points, the L^2 inner product yields

$$\begin{aligned}\langle I_N u, I_N v \rangle_{T^2} &= \left\langle \sum_{j=1}^N u_j \Psi_j(r, s), \sum_{i=1}^N v_i \Psi_i(r, s) \right\rangle_{T^2} \\ &= \sum_{j=1}^N \sum_{i=1}^N u_j \left(\sum_{l=1}^N V_{jl}^{-T} \gamma_l V_{li}^{-1} \right) v_i \\ &= \underline{u}^T \underline{W} \underline{v},\end{aligned}\quad (43)$$

where \underline{u} denotes the vector that gather all the Fekete point values of u , for example, $\underline{u} = \{u_1, \dots, u_N\}$. Finally, the matrix \underline{W} denotes the inner product metric, for example, $\underline{W} = V^{-T} \Gamma V^{-1}$.

Taking into account eqs (41) and (43), the quadrature weights can also be written as

$$\omega_k = \langle \Psi_k, \Phi_1 \rangle_{T^2} = \sum_{l=1}^N W_{kl},\quad (44)$$

and the discrete inner product associated with the Newton–Cotes quadrature formula yields

$$\begin{aligned}\langle I_N u, I_N v \rangle_N &= \sum_{\alpha=1}^N \omega_{\alpha} u_{\alpha} v_{\alpha} = \sum_{\alpha=1}^N u_{\alpha} \left(\sum_{\beta=1}^N W_{\alpha\beta} \right) v_{\alpha} \\ &= \underline{u}^T \tilde{W} \underline{v},\end{aligned}\quad (45)$$

where \tilde{W} is the lumped diagonal matrix associated with \underline{W} .

This collocated form used in Komatitsch *et al.* (2001) is however a minimal result since, using the Newton–Cotes quadrature, such a form is only exact if the integrand belongs to \mathbb{P}_N . This lack of accuracy of the Newton–Cotes quadrature associated with the Fekete points can have dramatic effect when using a diagonal mass formulation with the loss of the spectral convergence (Pasquetti & Rapetti 2004). It is worth noting here that improved multivariate quadrature points have been recently proposed by Taylor *et al.* (2005) to increase the strength of the numerical quadrature. However the new quadrature points do not coincide with the Fekete points, defined for interpolation and C^0 continuity, and therefore, do not provide for an extension of the collocated spectral element formulation to triangles but open interesting perspectives for more general curved triangulations and non-uniform material properties within a triangle.

3.2.4 Spectral element discretization

Within the framework of an unstructured triangulation $\mathcal{T}_h(\Omega)$ based on straight-sided triangles, the scalar product can be written as

$$(\mathbf{w}^h, \rho \mathbf{u}^h) = \sum_{e=1}^{n_e} \int_{\Omega_e} \rho^e \mathbf{w}^{he} \cdot \mathbf{u}^{he} d\Omega, \quad (46)$$

where $\mathbf{u}^{he} := \mathbf{u}^h|_{\Omega_e}$ denotes the restriction of the discrete approximation \mathbf{u}^h to the element Ω_e , with $\mathbf{u}^{he} \circ \mathcal{F}_e \in \mathbb{P}_N(\mathcal{T}^2)$.

Assuming piecewise constant material density ρ^e within the triangulation,

$$\begin{aligned} \int_{\Omega_e} \rho^e \mathbf{w}^{he} \cdot \mathbf{u}^{he} d\Omega &= \rho^e J^e \int_{\mathcal{T}^2} \mathbf{w}^{he}(r, s) \cdot \mathbf{u}^{he}(r, s) d\mathcal{T}^2 \\ &= \rho^e J^e \sum_{k=1}^2 \langle \mathbf{w}_k^{he}, \mathbf{u}_k^{he} \rangle_{\mathcal{T}^2} \\ &= \sum_{k=1}^2 \mathbf{w}_k^{heT} \mathbf{M}^e \mathbf{u}_k^{he}, \end{aligned} \quad (47)$$

where \mathbf{u}_k^{he} denotes the vector that gather the values of \mathbf{u}_k^{he} at the \mathcal{N} Fekete points and $\mathbf{M}^e = \rho^e J^e \mathbf{W}$ is an $\mathcal{N} \times \mathcal{N}$ matrix. Denoting $\mathbf{u}^{he} := (\mathbf{u}_1^{he}, \mathbf{u}_2^{he})$, one gets

$$\int_{\Omega_e} \rho^e \mathbf{w}^{he} \cdot \mathbf{u}^{he} d\Omega = \mathbf{u}^{heT} \mathbf{M}^e \mathbf{u}^{he}, \quad (48)$$

where \mathbf{M}^e denotes the element mass matrix with $\mathbf{M}^e = \mathbf{I}_2 \otimes \mathbf{M}^e$, and \mathbf{I}_2 is the 2×2 identity matrix. This induces a vector space norm that plays the role of the usual unweighted L^2 norm. It is worth noting here that in contrast with classical SEM, the element mass matrix is only block diagonal but it is exactly computed.

On the other hand, the bilinear form

$$\mathcal{A}(\mathbf{w}^h, \mathbf{u}^h) = \sum_{e=1}^{n_e} \int_{\Omega_e} \nabla \mathbf{w}^{he} : \mathbf{C}^e : \nabla \mathbf{u}^{he} d\Omega, \quad (49)$$

requires the evaluation of Cartesian derivatives. In the reference simplex, derivatives can be readily computed making use of the Dubiner's orthogonal basis as

$$\begin{aligned} \partial_r \mathbf{u}_k^{he}(r_i, s_i) &= \sum_{j=1}^{\mathcal{N}} \tilde{u}_{kj}^e \partial_r \Phi_j(r_i, s_i) \\ &= \sum_{l=1}^{\mathcal{N}} \mathbf{u}_k^{he}(r_l, s_l) \sum_{j=1}^{\mathcal{N}} V_{jl}^{-1} \partial_r \Phi_j(r_i, s_i), \end{aligned} \quad (50)$$

denoting $D_{ij}^r = \partial_r \Phi_j(r_i, s_i)$, then

$$\partial_r \mathbf{u}_k^{he} = \mathbf{D}^r \mathbf{V}^{-1} \mathbf{u}_k^{he}. \quad (51)$$

Making use of the affine geometrical mapping \mathcal{F}^e , the Cartesian derivatives can be readily computed

$$\bar{\mathbf{D}}^l = (\mathbf{D}^r r_{,l} + \mathbf{D}^s s_{,l}) \mathbf{V}^{-1}, \quad (52)$$

where $r_{,l}$, and $s_{,l}$ refers to the geometrical derivatives constants within each Ω_e . Assuming piecewise constant stiffnesses C_{ijkl}^e within the triangulation, the bilinear form is written as

$$\mathcal{A}(\mathbf{w}^h, \mathbf{u}^h) = \sum_{e=1}^{n_e} J^e \sum_{ijkl=1}^{n_d} \mathbf{w}_i^{heT} (\bar{\mathbf{D}}^{jT} C_{ijkl}^e \mathbf{W} \bar{\mathbf{D}}^l) \mathbf{u}_k^{he}. \quad (53)$$

The external force term $(\mathbf{w}^h, \mathbf{f}^h)$, in the case of a collocated force (7), follows from eq. (46), while in the case of a generalized body force (8) it follows from eq. (53).

Finally the construction of \mathcal{S}_t^h and $\delta \mathcal{S}^h$ is completed by imposing C^0 continuity between the subdomains of \mathcal{T}_h . One of the major advantages of the multidimensional Lagrangian basis (35) built on Fekete points, is that function continuity is easily enforced by equating nodal values of the functions \mathbf{u}_k^{he} shared on the boundary of adjacent subdomains. The associated global numbering results from numbering only once nodes that are counted twice or more times when lying on a vertex or an edge of adjacent subdomains. Let us denote $\tilde{\mathcal{N}}$, the number of global degrees of freedom, that is, the number of distinct nodes of \mathcal{T}_h , and $\mathbf{U}^h \in \mathbb{R}^{n_d \tilde{\mathcal{N}}}$, the vector form associated with the global numbering. Using the preceding results, the discrete variational form of the elastodynamics problem leads to a system of ordinary algebraic differential equations which can be written in standard form as follows,

$$\mathbb{M} \frac{\partial^2}{\partial t^2} \mathbf{U}^h = \mathbb{F}^{\text{ext}} - \mathbb{F}^{\text{int}}(\mathbf{U}^h), \quad (54)$$

where \mathbb{M} denotes the $(n_d \tilde{\mathcal{N}}) \times (n_d \tilde{\mathcal{N}})$ global mass matrix, and $\mathbb{F}^{\text{ext}}, \mathbb{F}^{\text{int}}$ the source and internal force vectors, respectively. The global mass matrix and vector forces are assembled from the element contributions as

$$\mathbb{M} = \mathbf{A}_{e=1}^{n_e} \mathbf{M}^e, \quad \mathbb{F}^{\text{ext}} = \mathbf{A}_{e=1}^{n_e} \mathbf{F}^{\text{ext},e}, \quad \mathbb{F}^{\text{int}} = \mathbf{A}_{e=1}^{n_e} \mathbf{F}^{\text{int},e}, \quad (55)$$

where $\mathbf{A}_{e=1}^{n_e}$ denotes the classical assembling operator, the action of which is the summation of the entries of coincident nodal values, and

$$\mathbf{F}^{\text{ext},e} = (\mathbf{F}_1^{\text{ext},e}, \mathbf{F}_2^{\text{ext},e}), \quad \mathbf{F}^{\text{int},e} = (\mathbf{F}_1^{\text{int},e}, \mathbf{F}_2^{\text{int},e}), \quad (56)$$

where $\mathbf{F}_i^{\text{int},e}$ and $\mathbf{F}_i^{\text{ext},e}$ are element \mathcal{N} -vectors. The internal forces result from the variation of the bilinear form (53) and are written as

$$\mathbf{F}_i^{\text{int},e} = J^e \sum_{jkl=1}^{n_d} (\bar{\mathbf{D}}^{jT} C_{ijkl}^e \mathbf{W} \bar{\mathbf{D}}^l) \mathbf{u}_k^{he}. \quad (57)$$

3.3 Time discretization

The semi-discrete momentum equation is simply enforced at time t_{n+1} using a classical Newmark stepping scheme (Hughes 1987; Zienkiewicz & Taylor 1989),

$$\mathbb{M} \mathbf{A}_{n+1}^h = \mathbb{F}_{n+1}^{\text{ext}} - \mathbb{F}_{n+1}^{\text{int}}(\mathbf{U}_{n+1}^h), \quad (58)$$

$$\mathbf{U}_{n+1}^h = \mathbf{U}_n^h + \Delta t \mathbf{V}_n^h + \Delta t^2 \left[\left(\frac{1}{2} - \beta \right) \mathbf{A}_n^h + \beta \mathbf{A}_{n+1}^h \right], \quad (59)$$

$$\mathbf{V}_{n+1}^h = \mathbf{V}_n^h + \Delta t [(1 - \gamma) \mathbf{A}_n^h + \gamma \mathbf{A}_{n+1}^h], \quad (60)$$

where $\mathbf{U}_{n+1}^h, \mathbf{V}_{n+1}^h$ and \mathbf{A}_{n+1}^h denotes the global displacement, velocity and acceleration fields at time t_{n+1} , respectively. The only member of the classical Newmark family that preserves exactly conservation of total angular momentum is the explicit central difference method obtained for $\beta = 0$ and $\gamma = 1/2$. This scheme is used hereafter for all the numerical simulations. Such an explicit scheme is second-order conditionally stable (Hughes 1987). The Courant condition to be satisfied for time steps is

$$\Delta t \left[\frac{V_p}{\Delta x} \right]_{\max} \leq c_h < 1, \quad (61)$$

where Δt the time step, V_p is the P wave velocity and Δx is the minimum distance between interpolation points. The stability value c_h depends on the mesh geometry. Experience has shown that a value of $c_h = 0.5$ is good enough to keep the simulations on unstructured meshes stable. In contrast with classical SEM, the resolution phase requires now solving the linear system of eq. (58) since the analytical mass matrix \mathbb{M} is no more diagonal. Although this matrix is very sparse (≈ 1 per cent of non-zero entries), it may have full bandwidth depending on mesh connectivity. Since the goal of this study was only to explore the accuracy and the flexibility of unstructured TSEM, no attempt was made here to optimize the conditioning of the global mass matrix. For the iterative resolution of the linear system, a simple preconditioned conjugate gradient method with a Jacobi pre-conditioner was used. In all the numerical examples presented in this work, 5 to 10 iterations of the conjugate gradient algorithm were found satisfactory, for example, with a relative residual error of 10^{-4} , even for long time evolutions. Clearly more evolved approaches remain yet to be explored in the context of elastodynamics, such as the overlapping Schwarz method proposed by Fisher (1997) that may allow less stringent stability criteria for the time stepping.

4 NUMERICAL EXAMPLES

4.1 Bi-periodic elastic wave propagation in an homogeneous medium

4.1.1 A comparison with classical SEM

A simple example of 2-D elastic wave propagation in homogeneous medium is first considered to investigate the long term stability and accuracy of the unstructured TSEM and to compare with classical SEM based upon structured quadrangular elements. The dimensions of the problem are shown in Fig. 2, with P wave velocity $V_p = 3200 \text{ m s}^{-1}$, S wave velocity $V_s = 1847.5 \text{ m s}^{-1}$ and a mass density of 2200 kg m^{-3} . The source is an explosive point source located exactly at the centre of the domain with a Ricker time wavelet of 16 Hz central frequency (f_0). The computational domain is subdivided in a structured grid of 40 by 40 quadrangular elements of 50 m side, which are subdivided using the diagonal of each element to create a mesh of triangular elements as shown in Fig. 2. A polynomial order of 5 is used for the interpolation, and therefore, both global grids, for example, the Gauss–Lobatto grid for quadrangular elements and the Fekete grid for triangular elements, have the same

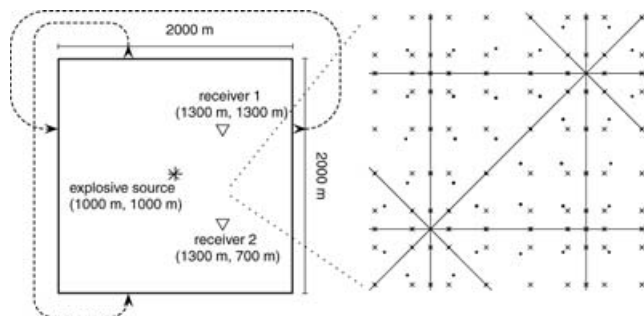


Figure 2. (Left) Schema of the homogeneous domain with bi-periodic boundary conditions. Source and receiver locations are shown. (Right) Detail of structured meshes. Global interpolation points with polynomial order of 5. Fekete points (•) used in this study, Gauss–Lobatto–Legendre points (×) used in classical SEM. Note that both set of points coincide at element's edges.

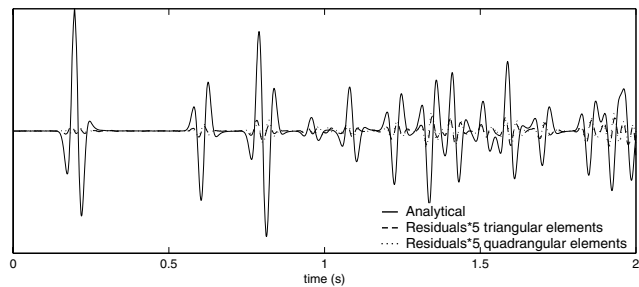


Figure 3. Horizontal component of the displacement field at receiver 1. Residuals between analytical and numerical solutions are amplified by a factor of 5. The vertical component is exactly similar (not shown).

number of 40401 interpolation points. In Fig. 2 both set of interpolation points are shown to coincide at the element edges. The number of points per minimum wavelength $\lambda_{\min} = V_s/f_{\max}$ with $f_{\max} = 2.5 f_0$ is between 4 and 5, which is the accuracy lower limit when using classical SEM (Seriani *et al.* 1992; Komatitsch & Vilotte 1998). Bi-periodic boundary conditions are imposed to propagate waves several times through the grid and a time step $\Delta t = 0.5 \text{ ms}$ is used, corresponding to a Courant number of 0.3. Simulations have been performed on the triangular mesh and on the quadrangular mesh, both up to 2 s total time (4000 time steps). Comparison of the horizontal displacement predicted by the TSEM and the classical SEM for the horizontal component at receiver 1 can be seen in Fig. 3. Comparison with the analytical solution shows that both methods perform well even for waves travelling several times through the computational mesh, for example arrivals later than 0.5 s.

4.1.2 Unstructured triangulation

The main advantage of triangular elements is to resort to unstructured meshes for the discretization of complex geometries. In this section we assess the performance of the TSEM when using an unstructured mesh built with the help of the mesh generator *Triangle* of Shewchuk (1996). It is worth noting here that for homogeneous media, this mesh generator does not seem to be optimal, for example, it does not generate equilateral triangles within an homogeneous medium for bi-periodic boundary conditions. The numerical example of the previous section is repeated here but now using an unstructured mesh shown in Fig. 4. This mesh is composed of 3202 triangles and 40426 global grid points, when using polynomial order of degree 5 for the interpolation within each triangular element (quite similar to the 3200 elements and 40401 global grid points used in the structured case). Bi-periodic boundary conditions are again imposed. Keeping the same source and time parameters as in the structured case, leads to 5 points per minimum wavelength and a Courant number of about 0.3. A snapshot of the displacement field at $t = 0.5 \text{ s}$ is shown Fig. 4 where no S wave is observed even in the case of such an unstructured mesh.

As in the previous example, the horizontal component of the displacement field calculated by the TSEM using the unstructured mesh is shown in Fig. 5 against the analytical solution. The result is quite accurate and it compares well with both structured mesh simulations shown in Fig. 3.

In a second test, both the consistent and the lumped mass TSEM are compared when using the unstructured triangular mesh. The results are shown in Fig. 6 where only the first P arrivals are compared to the analytical solution. The consistent TSEM formulation clearly exhibits much better accuracy than the lumped mass formulation. A

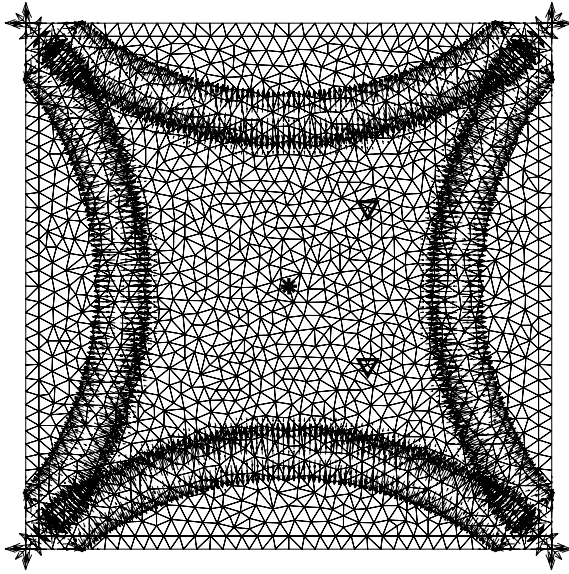


Figure 4. Snapshot of displacement at 0.5 s. Source and receiver locations are also shown. Note the absence of any numerically generated S wave in spite of the mesh irregularity.

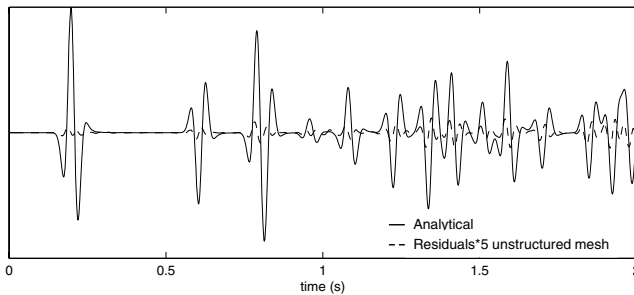


Figure 5. Horizontal component of the displacement field at receiver 1. Residuals between analytical and numerical solution calculated using the unstructured mesh are amplified by a factor of 5.

clear ringing instability after the P wave arrival can be observed in the latter case, a fact that was already noticed by Komatitsch *et al.* (2001). Nevertheless it is worth mentioning that as expected, the computational time is greatly reduced by almost a factor of 5 when using the diagonal mass matrix formulation.

4.2 The Lamb's problem

The Lamb's problem (Lamb 1904) is a classical problem for assessing wave propagation algorithms. It involves elastic wave propagation in an homogeneous elastic half-space due to a point source. When the source is located just below the free surface, three main phases are excited: a direct P wave, a direct S wave and a non-dispersive Rayleigh wave. The physical domain considered here is a homogeneous half-space with a P wave velocity of 3200 m s^{-1} , a S wave velocity of 1847.5 m s^{-1} and a density of 2000 kg m^{-3} . The numerical model has a width of 4000 m and a depth of 2000 m. The vertical point source is located just below the surface, at a computational node located at $x_s = 1500 \text{ m}$ and $z_s = 1950 \text{ m}$, in order to generate a strong Rayleigh wave. The source time function is a Ricker wavelet of 10 Hz central frequency leading to a minimum wavelength of $\lambda_{\min} = 74 \text{ m}$.

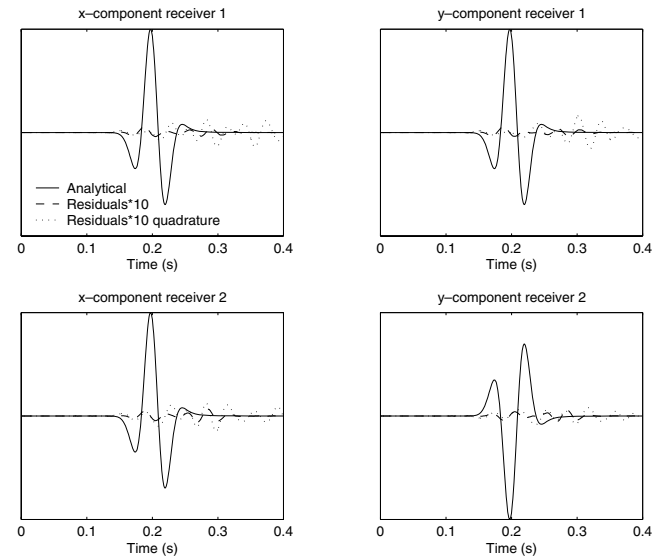


Figure 6. Horizontal x -component (left) and Vertical y -component (right) of the displacement field recorded at receivers 1 (top) and 2 (bottom). Residuals to the analytical solution are amplified by a factor of 10. Note the instabilities that appear after the P wave arrival while using a quadrature rule for the mass matrix calculations.

In order to test the spectral convergence of the TSEM, we have used three different meshes composed of $N_{el} = 628$, 2500 and 6882 triangles, with average triangle edges h of 180 m, 105 m and 65 m, respectively. The polynomial degree in each triangle is chosen from $N = 3, 5, 7$ and 9. Therefore, the spatial resolution goes from 2.4 points per minimum wavelength (for the coarsest mesh with the lowest polynomial degree) up to around 9 points per minimum wavelength (for the finest mesh with the highest polynomial degree). The snapshots of the displacement field at 0.5 s over each computational mesh are shown in Fig. 7. In order to minimize time discretization errors, we fix the Courant number at $c_h = 0.2$ and calculate the time step for each simulation using eq. (61) and the minimum distance between nodal points in the corresponding mesh.

The analytical solution for this problem is calculated using the Cagniard-de Hoop method (de Hoop 1960) for two receivers located at the free surface in (2200, 2000 m) receiver 1, and (2700, 2000 m), receiver 2. It is worth mentioning that the accuracy obtained from the available code to calculate the analytical solution is around 10^{-3} . In Fig. 8 the comparison between the analytical solution and the TSEM simulations for the mesh with $N_{el} = 2500$ and $N = 5, 7$ and 9 are shown. It is clear the rapid convergence to the analytical solution while augmenting the polynomial interpolation degree. This illustrates the high accuracy of the TSEM for simulating Rayleigh wave propagation even in the case of an unstructured mesh, as shown in the zoomed image of Fig. 7.

In the following, the error is calculated as an average of the L_{∞} error in the two components of receivers 1 and 2, that is, the maximum difference between analytical and numerical seismograms in the time window. Fig. 9 shows the semi-log plot of the error as a function of the polynomial degree N for the three different meshes. As expected, the convergence to the analytical solution is exponential in N for this example, confirming that the overall error is still dominated by the spatial discretization.

Let suppose we ask the method to simulate Rayleigh waves for 1 s with an error level around 2 per cent. From Fig. 9, two (h, N) combinations are possible: $h = 105$, $N = 7$, or $h = 65$, $N = 5$.

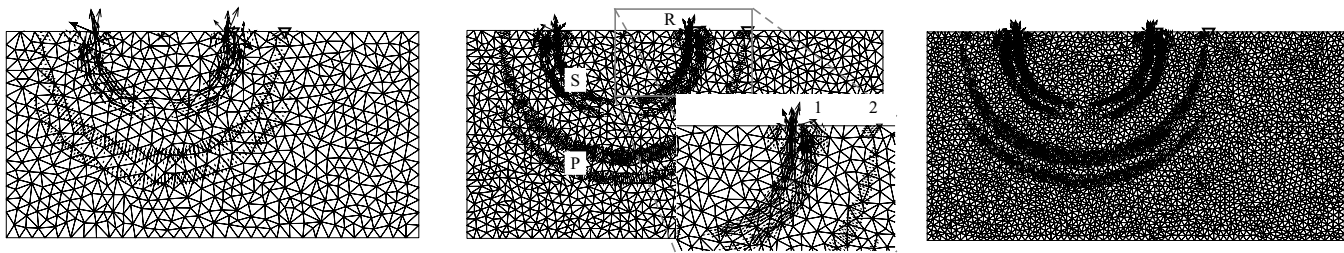


Figure 7. Lamb's problem. Snapshots of the displacement field at 0.5 s on top of the unstructured meshes with (from left to right) 628, 2500 and 6882 elements. The direct P wave (P), S wave (S), and the Rayleigh wave (R) can be seen. Vertical point source location and receivers 1 and 2 are also shown.

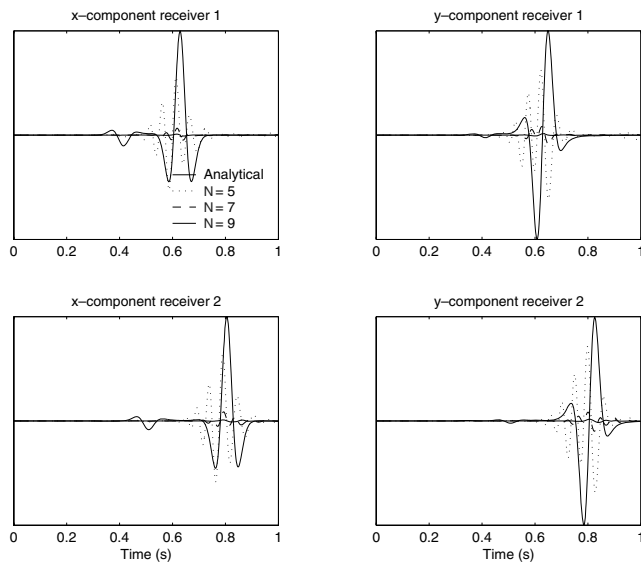


Figure 8. Horizontal x -component (left) and Vertical y -component (right) of the displacement field recorded at receiver 1 (top) and 2 (bottom). Residuals to the analytical solution are amplified by a factor of 5 for $N = 5$ and a factor of 10 for $N = 7$ and 9. The main arrival corresponds to the non-dispersive Rayleigh wave.

Both have similar sampling of the wavefield (around 5.6 points per minimum wavelength) and $\Delta t/s$ (around 0.3 ms). The difference lies on the number of degrees of freedom \tilde{N} in each simulation, a factor directly related to the computational cost of the algorithm. For $(h, N) = (105, 7)$ we obtain 61713, while for $(h, N) = (65, 5)$ we obtain 86531. Therefore, the pair with higher interpolation order in the coarser mesh should be chosen.

5 2-D NUMERICAL SIMULATIONS

More realistic 2-D simulations are now considered to illustrate the ability of the TSEM to take into account complex geometries using unstructured triangulations.

5.1 The elastic wedge problem

The problem considered is the reflection and transmission of a Rayleigh wave at a step of the free surface. This so-called 'elastic wedge problem' (Lapwood 1961; Hudson & Knopoff 1964) can be associated to a fault or a stiff cliff at the free surface. The physical domain is defined here as a heterogeneous quadrangle of 2000 m side separated by one of its diagonals into two different elastic media of different materials properties shown in Table 1. This example

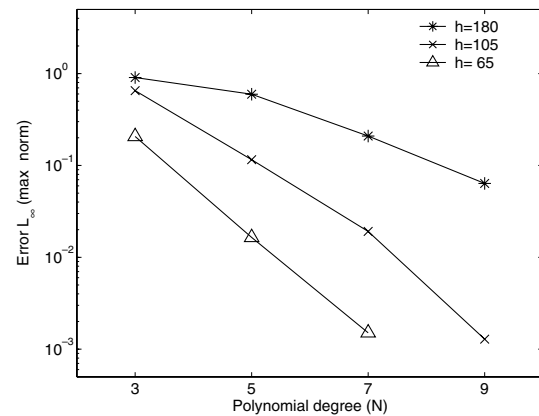


Figure 9. L_∞ error for three different meshes showing the spectral convergence of the method for the Lamb's problem.

Table 1. Physical parameters for the elastic wedge problem.

Parameter		Material 1	Material 2
P -wave velocity	$[\text{m s}^{-1}]$	2500	4000
S -wave velocity	$[\text{m s}^{-1}]$	1250	2000
Density	$[\text{kg m}^{-3}]$	2000	2200
Rayleigh velocity	$[\text{m s}^{-1}]$	1165	1865

illustrates two well-known problems in the simulation of elastic wave propagation: accurate approximation of interface waves; and strong velocity contrasts between elastic media. The physical problem is, therefore, the impinging of a Rayleigh wave into a homogeneous elastic corner, at the upper left of the domain, and into a heterogeneous elastic 45° wedge, at the upper right of the domain. The displacement, velocity and acceleration fields of the unperturbed Rayleigh wave solution are prescribed initially, and computed analytically from the solution of the problem in a homogeneous half-space of Material 1 properties. The time function is chosen here to be a Ricker wavelet with a 20 Hz central frequency. Two snapshots, at $t = 0.25$ s and $t = 1.125$ s, of the displacement field are shown Fig. 10. The computational mesh of 2915 spectral elements is superimposed on the same figure. Unstructured triangulations easily allow for a coarser mesh in the domain of higher seismic velocities, longer wavelengths, and therefore, for a uniform sampling of 5 interpolation points per minimum wavelength. When using a uniform polynomial order of 5 in the whole domain, a natural conforming unstructured mesh is obtained all along the material interface. The total number of global grid points is 29226, and the elastic wavefield is propagated for 1.5 s with a time step of 0.25 ms. In Fig. 10 recording stations placed along both corners are also shown. The

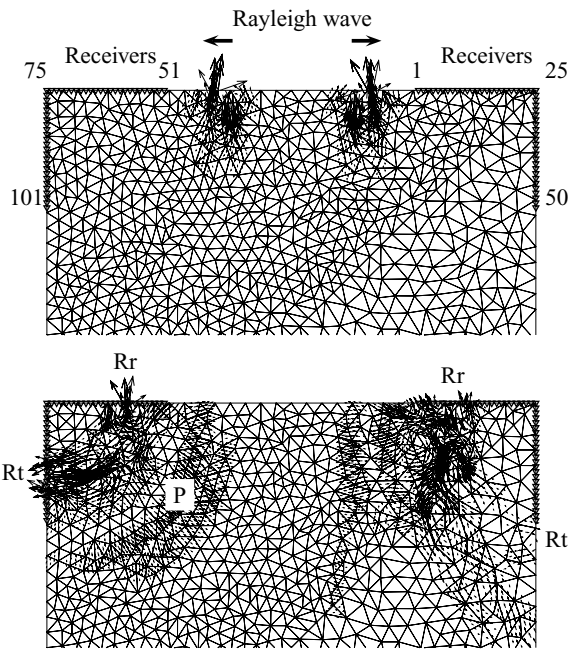


Figure 10. Snapshots of the displacement field at $t = 0.25$ s (top) and $t = 1.125$ s (bottom). In the top one, the incident Rayleigh waves travelling along the top boundary of the model can be seen. In the bottom one, we can identify the reflected Rayleigh waves (Rr), the transmitted Rayleigh waves (Rt) and the Rayleigh to P conversion at the homogeneous corner (P).

corresponding seismograms can be seen in Fig. 11, for the homogeneous corner, and in Fig. 12, for the heterogeneous corner. When the waves hit the corners, complicated patterns of diffracted waves are generated. In the homogeneous (left) corner, it is essentially characterized by a P wave conversion, a reflected Rayleigh wave travelling backwards and a transmitted Rayleigh wave travelling downwards with an inverted phase as predicted by theory (Lapwood 1961; Hudson & Knopoff 1964), and numerically simulated using classical SEM in Komatitsch & Vilotte (1998). It is worth noting here that the Rayleigh wave is non-dispersive as expected and propagates with the right velocity. At the heterogeneous (right) corner, the diffraction pattern is more complicated due to strong reverberations generated at the wedge and to the dispersive characteristic

of the Rayleigh wave in heterogeneous medium. The converted P wave, the transmitted Rayleigh wave, of much lower amplitude than in the homogeneous corner as expected when Material 2 is stiffer than Material 1, and the reflected dispersive Rayleigh wave, can be identified.

5.2 Elastic scattering by a cylinder in a homogeneous half-space

This example illustrates the scattering of a plane wave by an elastic cylinder buried in a homogeneous half-space. Such an example appears frequently in non-destructive testing and near surface seismic studies (cavities, gas inclusions). An analytical solution can be obtained from the expansion of the displacement field in series of Bessel functions, as detailed in the Appendix, and used to assess the accuracy of the TSEM built on an unstructured triangulation. From the numerical point of view, the main difficulty lies on meshing the curved internal interface, specially in the case of two media with high velocity contrast where both an accurate approximation of the body and the interface waves are mandatory. In order to illustrate the flexibility of an unstructured triangulation, three cases are considered here: first, a stiff cylindrical inclusion is included within a more compliant elastic space; second, a compliant cylindrical inclusion is embedded in a stiffer elastic space; and finally a more compliant inclusion is included in a stiffer elastic space in order to test the accuracy of the TSEM for extremely high velocity contrasts. In the first case the physical model is a circular inclusion of 500 m diameter with $V_p = 3000$ m s⁻¹, $V_s = 1732$ m s⁻¹ and $\rho = 2$ kg m⁻³, embedded in a more compliant elastic half-space of 2000 m by 2000 m with $V_p = 2000$ m s⁻¹, $V_s = 1155$ m s⁻¹ and $\rho = 1$ kg m⁻³. These parameters were borrowed from Priolo *et al.* (1994) who studied a two quarter space problem, that is two elastic half-spaces in contact along a vertical material discontinuity, with special emphasis in the simulation of the interface wave travelling along the vertical interface, a geometry that is well suited for classical SEM based on a quadrangular mesh. Here the scattering by an elastic cylinder of a plane wave travelling downwards is considered. In this problem, an interface wave is expected to travel along the circular boundary of the buried cylinder. The triangulation in this example is composed of 3402 triangles, with a total number of 42 846 global Fekete points when using a polynomial degree of

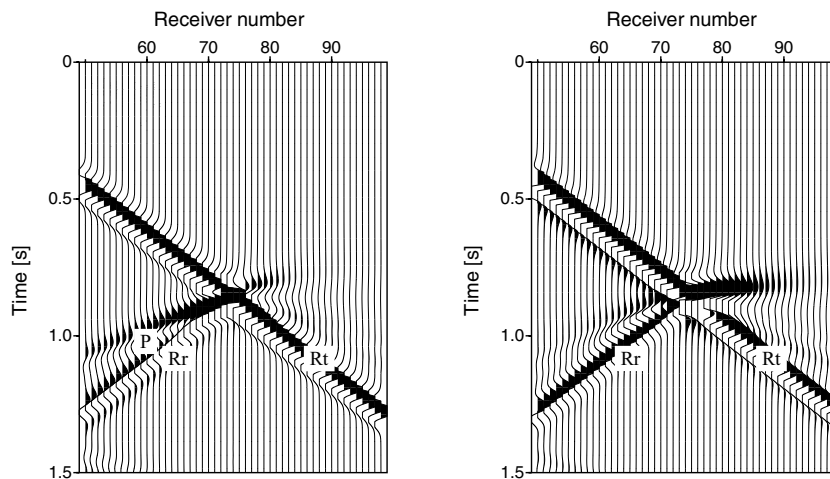


Figure 11. Seismograms of horizontal (left) and vertical component (right) of the displacement field recorded at the homogeneous corner. We identify the main events of Fig. 10.

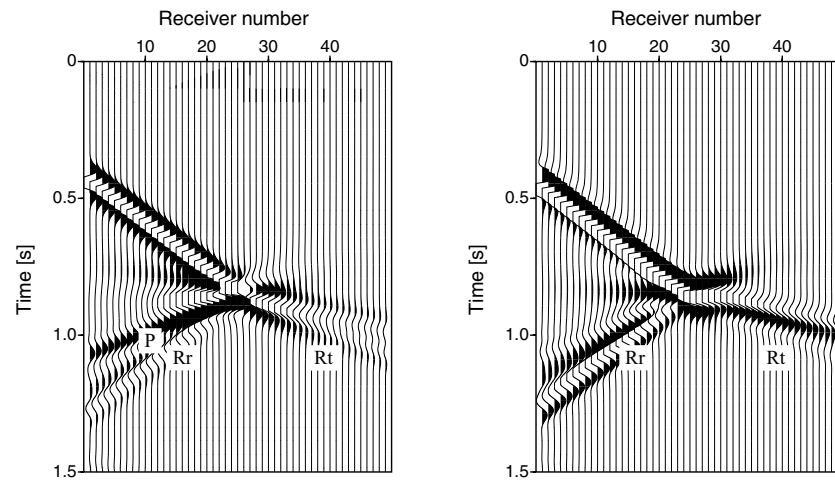


Figure 12. Seismograms of horizontal (left) and vertical component (right) of the displacement field recorded at the wedge corner. Note the dispersive characteristic of the transmitted (Rt) and reflected (Rr) Rayleigh waves.

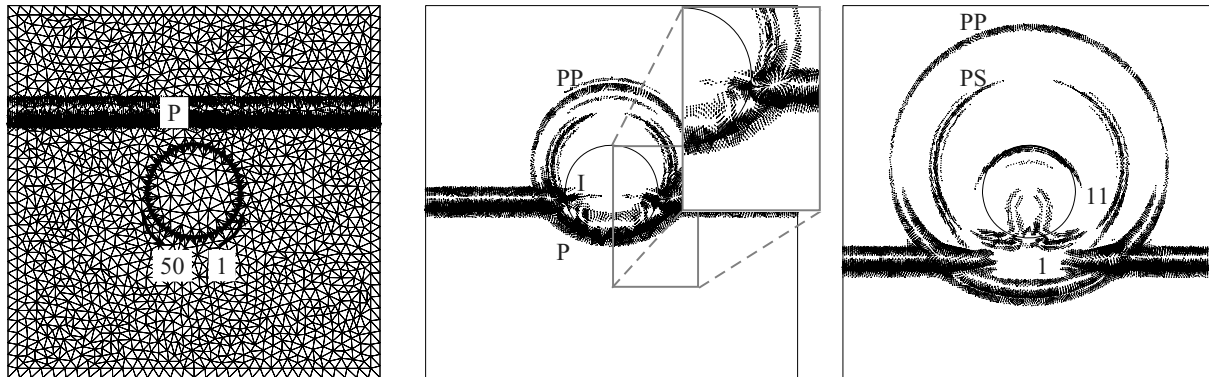


Figure 13. Snapshots of the scattered displacement field by the elastic cylinder over the computational mesh at $t = 0.04$ s (left), $t = 0.24$ s (middle) and $t = 0.44$ s (right). The main scattered waves can be seen, I: interface wave, PP: P wave reflected at the cylinder, PS: P to S conversion at the cylinder. Receivers along the interface are indicated by filled triangles in the leftmost snapshot.

order 5 for the interpolation. Using unstructured triangulation, with a maximum area criteria, uniform sampling of the wavefield can be easily achieved both within the elastic cylinder and the homogeneous space. Periodic boundary conditions in the left and right boundaries allow to simulate an incoming horizontal plane wave travelling downwards. The plane wave, with a P polarization and a Ricker wavelet modulation of 16 Hz central frequency, is prescribed by an initial displacement, velocity and acceleration fields. Along the curved interface, the sampling is about 4.5 interpolation points per minimum S wavelength. The wave field is propagated during 0.6 s using a time step of 0.2 ms, leading to a Courant number of the order of 0.2. Snapshots of the displacement field, at $t = 0.04$ s, 0.24 s and 0.44 s, are shown in Fig. 13. The incoming P plane wave travelling downwards, the PP reflection generated at the cylinder and the strong interface wave can be identified in the snapshot at $t = 0.24$ s. These events can also be seen in Fig. 14, where the displacement seismograms recorded at receivers located all along the interface are displayed. The P wave arrival can be identified with a kind of sinusoidal moveout, as well as the interface wave that exhibits a linear moveout as long as the receivers are equispaced along the circular interface. It is worth noting here the lack of numerical artefacts even though the circular interface is only approximated by straight-sided triangular elements. Accuracy of the TSEM for this problem, can be assessed when comparing with the analytical

solution at receivers on the circular interface located at (1000 m, 750 m) for receiver 1 and (1237.8 m, 922.4 m) for receiver 11. These receivers are displayed in the rightmost snapshot of Fig. 13. The normalized analytical solution for each component of the displacement field and residuals computed using the numerical solution, amplified by a factor of 10 are displayed in Fig. 15. The L_∞ error is computed and shown on top of each seismogram. An error of less than 2 per cent for all the arrivals is observed for both receivers.

In the second case, the physical parameters are interchanged to obtain a more compliant cylindrical inclusion in a stiffer elastic space. The triangulation is now refined within the cylindrical inclusion, where the wave speeds are slower, in order to obtain a uniform sampling of the wavefield within the whole domain. The resulting triangulation is composed of 2370 triangles with a total number of 29 946 global interpolation points using again a polynomial degree of order 5 for the interpolation. The triangulation is shown in the leftmost panel of Fig. 16. The incident wave field is the same as in the previous example with periodic boundary conditions. Same time-stepping parameters as before are used and the total simulation time is 0.65 s. In Fig. 16 snapshots of the displacement field, at $t = 0.02$ s, 0.20 s and 0.28 s, are shown with the main phases identified in the seismograms of Fig. 17. The incident wave front is delayed by the cylindrical inclusion. Comparing again with the analytical

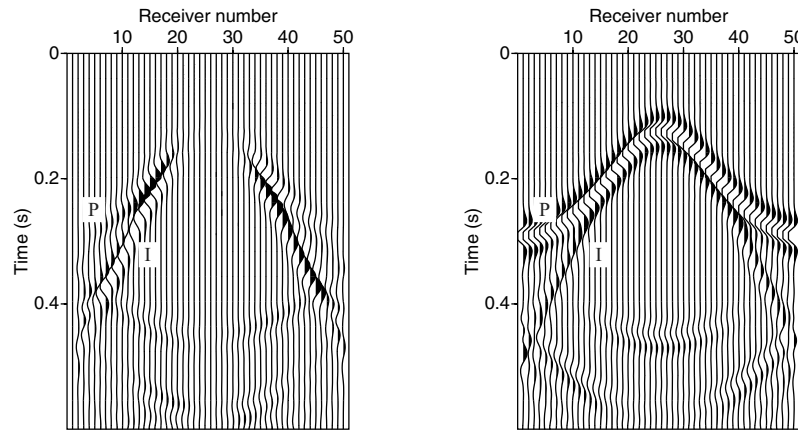


Figure 14. Seismograms of horizontal (left) and vertical component (right) of the displacement field recorded at the receivers located all along the circular interface (stiff inclusion). *P*: direct *P* wave arrival, *St*: Stoneley wave travelling along the circular interface.

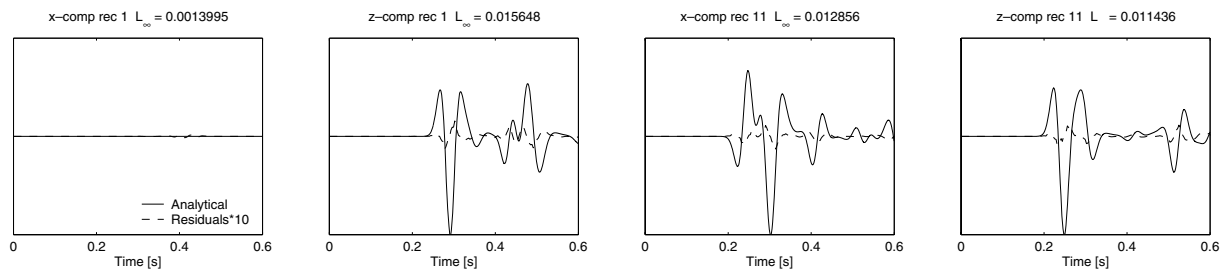


Figure 15. Horizontal x-component and vertical z-component of the displacement field recorded at receivers 1 and 11 (stiff inclusion). Residuals are amplified by a factor of 10. As expected, there is no energy in the horizontal component of receiver 1 placed on the cylinder axis. The arrival around 0.3 s at receiver 11 corresponds to the interface wave.

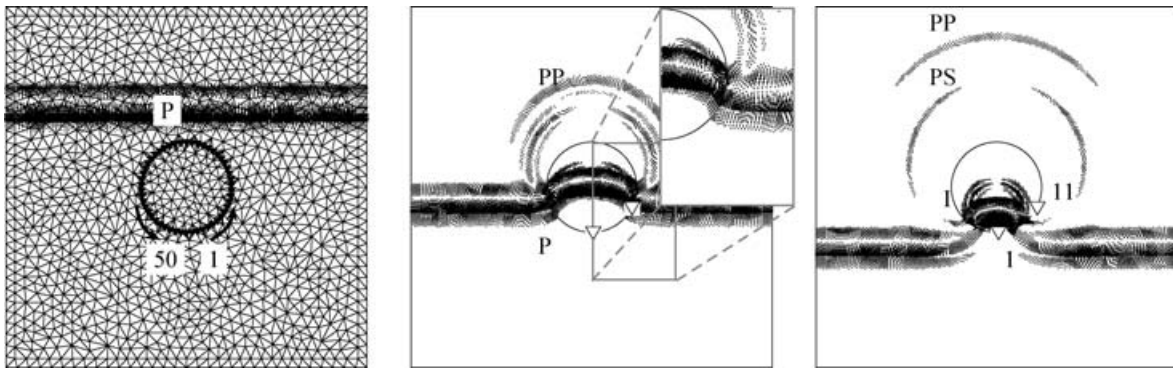


Figure 16. Snapshots of the scattered displacement field by the elastic cylinder over the computational mesh at $t = 0.02$ s (left), $t = 0.20$ s (middle) and $t = 0.28$ s (right). The main scattered waves can be seen, *I*: interface wave, *PP*: *P* wave reflected at the cylinder, *PS*: *P* to *S* conversion at the cylinder. Receivers along the interface are indicated by filled triangles in the leftmost snapshot.

solution at the same receivers used for the first case, Fig. 18, ensures an error of less than 2 per cent between the analytical and numerical solutions.

In the third case, a much higher velocity contrast between the compliant cylindrical inclusion and the surrounding space is created by using $V_p = 4000$ m s⁻¹, $V_s = 2310$ m s⁻¹ and $\rho = 2$ kg m⁻³ for the elastic space and $V_p = 1400$ m s⁻¹, $V_s = 600$ m s⁻¹ and $\rho = 1$ kg m⁻³ for the inclusion. The incident wavefield is the same as in the previous examples with periodic boundary conditions. In order to keep a similar Courant number of 0.2, the time step must be reduced to 0.112 ms for this simulation due to the strong mesh refinement in the cylindrical inclusion. In Fig. 19 snapshots of the displacement field,

at $t = 0.0$ s, 0.2 s and 0.3 s, are shown with the main phases identified in the seismograms of Fig. 20. It is interesting to note in Fig. 21 similar error levels as in the previous case (less than 2 per cent), showing the robustness of the method to deal with such strong velocity contrast within the elastic medium.

5.3 Elastic half-space with free-surface and interface topographies

The flexibility of an unstructured triangulation for wave propagation simulation can be illustrated when considering wave propagation in a layered 2-D elastic domain with arbitrary topography of the free

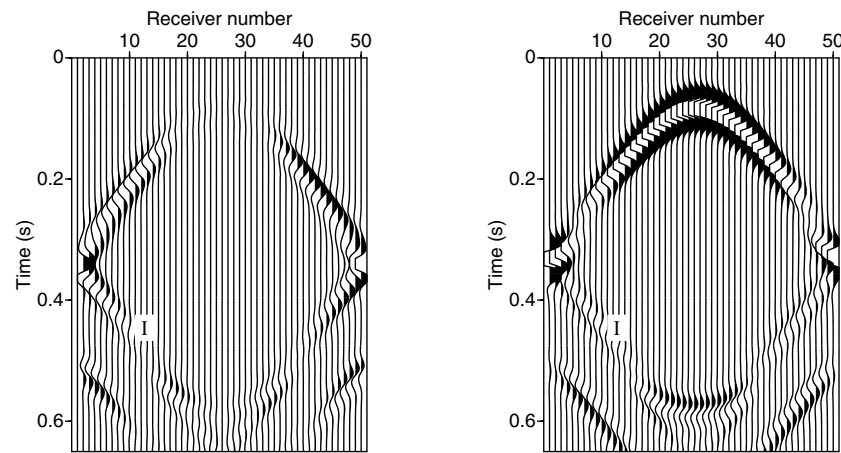


Figure 17. Seismograms of horizontal (left) and vertical component (right) of the displacement field recorded at the receivers located all along the circular interface (compliant inclusion). I: interface wave.

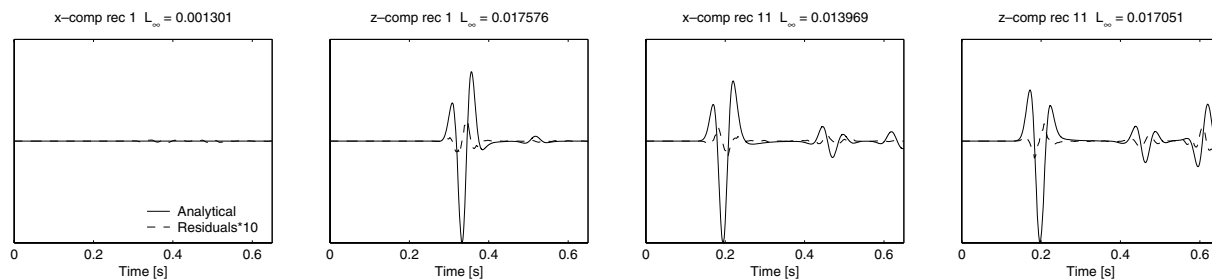


Figure 18. Horizontal x-component and vertical z-component of the displacement field recorded at receivers 1 and 11 (compliant inclusion). Residuals are amplified by a factor of 10. There is no significant energy in the horizontal component on the cylinder axis.

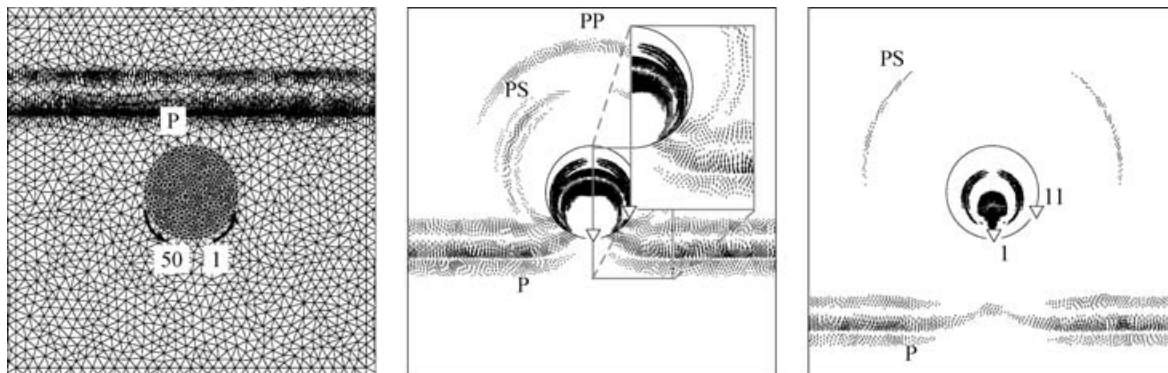


Figure 19. Snapshots of the scattered displacement field by the elastic cylinder over the computational mesh at $t = 0.0$ s (left), $t = 0.2$ s (middle) and $t = 0.3$ s (right). Note the difference in wavelength between the inclusion and the surrounding medium. Receivers along the interface are indicated by filled triangles in the leftmost snapshot.

surface and internal material interfaces. In the example considered here, an upper layer is considered as filled by some kind of alluvial deposit made of soft materials. An extensive study of the seismic response of such an alluvial basin is beyond the scope of this paper and the interested reader can be referred to Sánchez-Sesma *et al.* (1993). The main interest here is to illustrate the geometrical flexibility and the enhanced mesh adaptivity provided by the use of an unstructured triangulation. The TSEM built on an unstructured triangulation allows enhanced geometrical flexibility as well as the possibility of spatial mesh refinement in a rather natural and easy way. According to the wave velocity variations in the model, the element size

can be locally reduced to keep uniform sampling of the wavefield. However, one should keep in mind that for small spectral elements, the distance between interpolation points may become prohibitively small with regard to the Courant number and conditional stability of an explicit time-stepping scheme. A consideration that should also be kept in mind while using highly deformed quadrangles.

The spatial triangulation is again obtained here using a maximum area constraint, as provided by the meshing software *Triangle*, in order to obtain at least five interpolation points per minimum wavelength within the whole domain. Material parameters, as well as some other relevant parameters, are summarized in Table 2. An

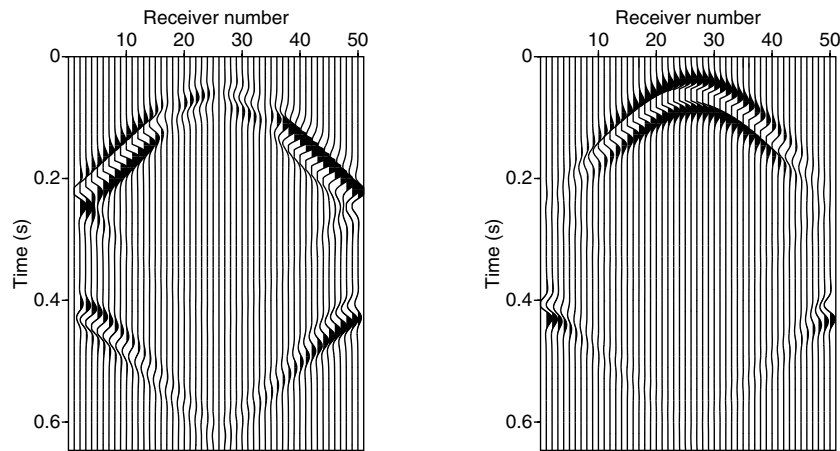


Figure 20. Seismograms of horizontal (left) and vertical component (right) of the displacement field recorded at the receivers located all along the circular interface.

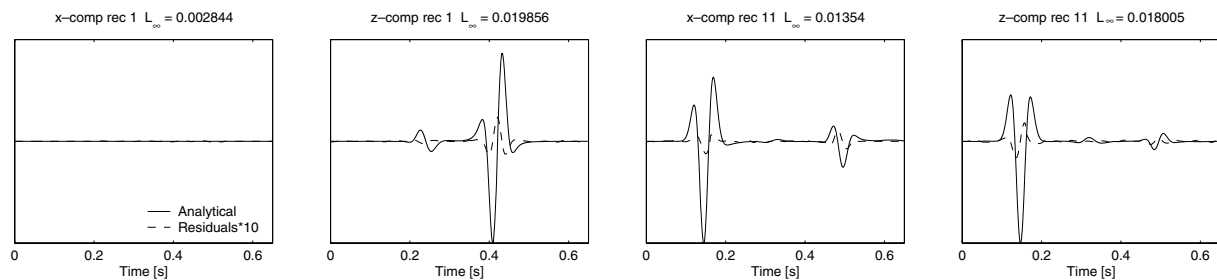


Figure 21. Horizontal x -component and vertical z -component of the displacement field recorded at receivers 1 and 11 (compliant inclusion with high velocity contrast). Residuals are amplified by a factor of 10.

Table 2. Physical and mesh parameters for the elastic layered medium. The Δ edge size (last row) is an average of all the triangle edges in the corresponding layer.

Parameter		Alluvial	Upper	Lower
P -wave velocity	$[\text{m s}^{-1}]$	1300	2800	4000
S -wave velocity	$[\text{m s}^{-1}]$	750	1616	2310
Density	$[\text{kg m}^{-3}]$	1200	2200	2500
Minimum wavelength	$[\text{m}]$	30	65	92
Δ edge size	$[\text{m}]$	32	60	100

explosive point source, with a Ricker time function of 10 Hz central frequency, is located in the upper layer just below the free surface so as to excite a strong Rayleigh wave along the curved topography. The dimension of the numerical domain has a width extension of 2500 m and an average depth of 1600 m. The discretization is made of 2418 triangles, and a polynomial degree of order 5 is used for the interpolation within each triangles. The numerical mesh shown in the upper-left panel of Fig. 22 is artificially extended to the left, right and bottom boundaries in order avoid spurious reflections. This can also be achieved in a more elegant way, using Perfectly Matched Layers as proposed by Komatitsch & Tromp (2003) and Festa & Vilotte (2005). The time step in this simulation is $\Delta t = 0.25$ ms, leading to a Courant number of 0.35 in the upper layer. Typical snapshots of the displacement field are displayed in Fig. 22 together with the unstructured mesh refined towards the upper layer and especially within the soft alluvial basin. The main observed phases here are: a strong Rayleigh wave propagating along the topography, a direct P wave, together with a PP phase generated at the free surface, a

converted PS wave at the surface topography, and a strong head-wave that propagates downwards into the medium. In the snapshot at $t = 0.4$ s, bottom-left panel, a Rayleigh to body wave conversion can be observed. Such a conversion is likely to happen when the Rayleigh wave reaches a strong curvature change of the surface topography (Jih *et al.* 1988; Komatitsch & Vilotte 1998). Within the alluvial valley, the refracted wave (Pr) can be seen travelling along the bottom of the alluvial basin with the P wave velocity of the upper layer, as well as a high amplification of the incoming Rayleigh wave. When considering the line of receivers shown in the upper-left panel of Fig. 22 and located at the surface of the alluvial basin, the previous phases can be identified directly from the displacement seismograms, as shown in Fig. 23.

6 CONCLUSIONS

In this study, a TSEM is investigated within the context of elastic wave propagation in complex geological media. Extension of spectral methods to problems defined on non-tensor-product domains, like the n_d -simplex, is an important issue in computational seismology. This would allow expanding the applicability of the SEM to complex geological structures together with improving mesh adaptivity capability. Moreover, using n_d -simplex spectral elements allows the use of existing software for automated unstructured mesh generation used by modern geological modellers.

For the sake of completeness, we reviewed some of the actual issues on the formulation of such schemes. On n_d -simplex subdomains, spectral expansion of the solution can be achieved when resorting to the Dubiner's orthogonal basis that results from a

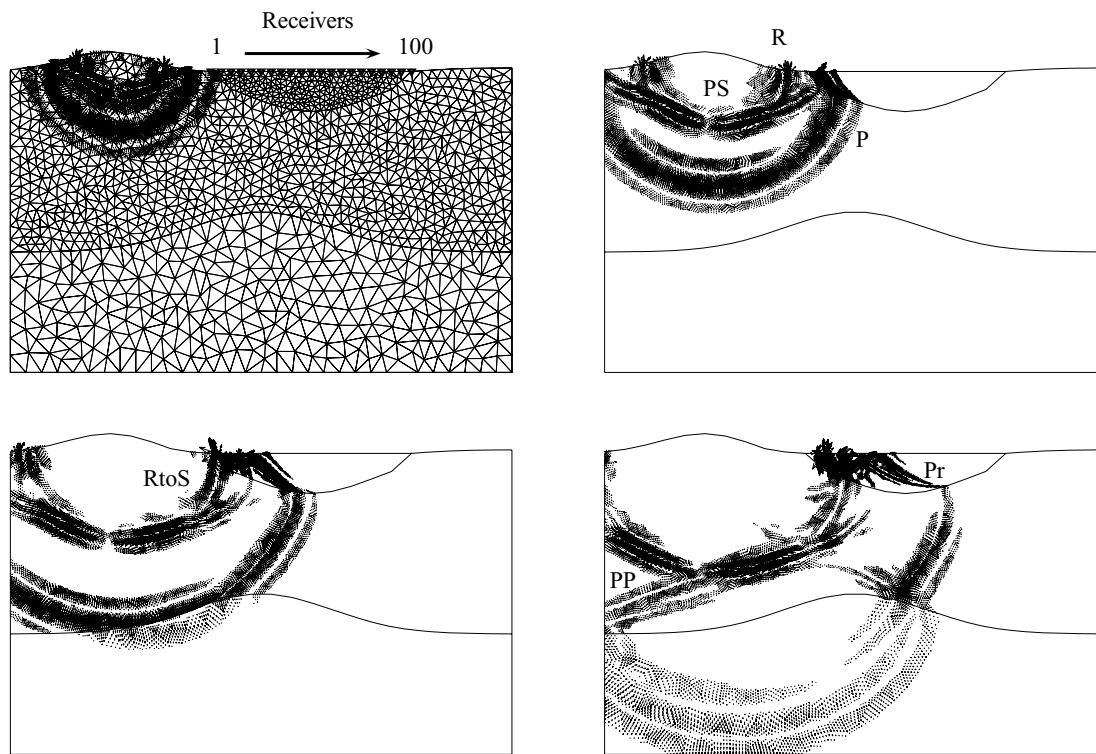


Figure 22. Snapshot of the displacement field in the layered elastic half-space at 0.2 s, 0.3 s, 0.4 s, 0.5 s (from top left to bottom right). Some main wave fronts are identified: *P* direct *P* wave (*P*), converted *P* to *S* at the free surface (*PS*), Rayleigh wave (*R*), Rayleigh to *S* wave conversion (*RtoS*), refracted *P* wave (*Pr*). The numerical mesh, the source and the receiver line location can be seen in the top-left snapshot.

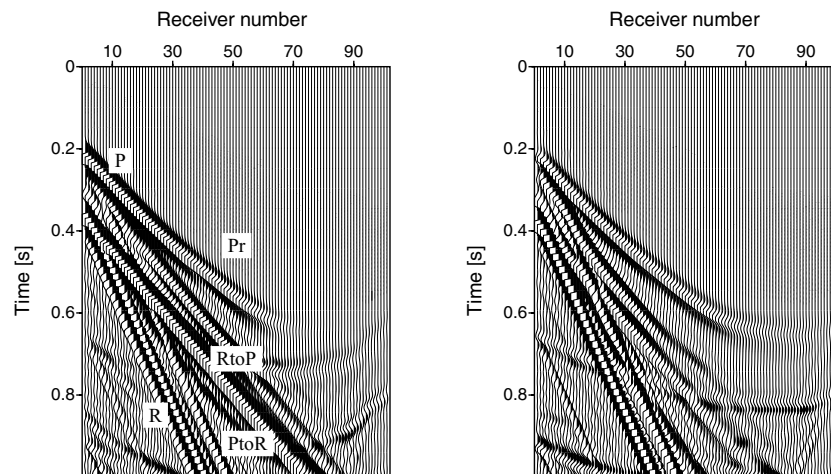


Figure 23. Seismograms of the horizontal (left) and vertical component (right) of the displacement field recorded at the top of the alluvial valley. Some main events are identified: direct *P* wave (*P*), refracted *P* wave at the bottom of the alluvial valley (*Pr*), Rayleigh wave (*R*), Rayleigh to body wave conversion (*RtoP*) and *P* to Rayleigh conversion (*PtoR*) at the valley's tip.

warped tensor product of Jacobi polynomials associated with a local collapsed coordinate system. Such a construction can be seen as a generalization of the classical tensor product construction in use with classical SEM built on tensor product domains. This orthogonal polynomial basis can be shown to be the solution of a Sturm–Liouville eigenvalue problem defined on the reference simplex, and therefore, to achieve spectral accuracy. Based on this orthogonal basis, a TSEM can be constructed by resorting, as in classical SEM, to a multivariate Lagrangian interpolation designed to enforce in a natural way the C^0 continuity requirement between subdomains

of the triangulation. Today, even though no optimal set of points is known for interpolation on a non-tensor product-domain, such a multivariate Lagrangian interpolation can be built based on the set of Fekete points that are shown to endow good interpolation properties and to maximize the number of points on the boundary of the subdomains. In these boundaries, Fekete points turn out to coincide with the classical GLL points used in classical SEM. However, in contrast with the GLL set of points defined on tensor product domains, Fekete points do not define an optimal quadrature formula in the sense that the associated Newton–Cotes quadrature formula only

integrates exactly polynomials of \mathbb{P}_N . This is clearly a minimal result that does not allow for the extension of the SEM collocated formulation to non-tensor product domains. As a consequence, the resulting consistent mass matrix is not diagonal, a feature that adds significant computational complexity for explicit time-stepping schemes typically used within the seismological community. Resorting to a lumped mass matrix in TSEM implies a significant accuracy loss that in some cases can even destroy the spectral convergence of the method. Moreover, there is no tensor product structure associated with Fekete points and the computation of spatial derivatives requires some careful analysis in order to avoid a prohibitive $\mathcal{O}(N^{2n_d})$ asymptotic scaling. As it is, the TSEM is attractive enough to explore its possible use for numerical simulation of elastic wave propagation in seismology. A preliminary exploration is done in this paper through classical canonical examples and relevant 2-D elastic wave problems. Numerical results presented here do show the high accuracy and the geometrical flexibility of the TSEM. Comparison with classical SEM built on quadrangular grids shows that TSEM does share the same level of accuracy and stability. Surface and interface waves are shown to be accurately modelled even in the case of complex topography with the TSEM. Numerical results for specific problems such as 2-D elastic wave scattering by a cylinder embedded in a homogeneous half-space clearly illustrates the enhanced geometrical flexibility and mesh adaptivity of the TSEM and strongly suggests its use in computational seismology.

Although this paper does not address issues on efficient computational implementations of TSEM, nor precise comparisons in terms of computational costs between classical SEM and TSEM, it should be emphasized that without specific improvements, TSEM remains more expensive than classical SEM. Therefore, there is today clearly room for improvements of the TSEM.

Regarding the computational implementation of the TSEM presented here, the actual cost associated with derivative computations may be significantly reduced when resorting to efficient factorization techniques that exploit the symmetries inherent to the Fekete nodal set and a careful ordering of the nodes. This is clearly emphasized in the work of Hesthaven & Teng (2000), where such a careful implementation is shown to lead to a drastic reduction of the derivative computational costs that compare well with those obtained in classical SEM.

Another issue is related to the improvement of efficient strategies that can cope with the sparse global mass matrix resulting from the lack of an accurate quadrature formula associated with the Fekete nodal set. In the time domain, there is some room for improvements mainly with regard to the iterative resolution of the algebraic system that results from an explicit time discretization, therefore, governed by the mass matrix; or a semi-implicit time discretization, governed by a Helmholtz matrix. In this direction efficient iterative solvers using conjugate gradients preconditioned by the additive overlapping Schwarz method, introduced by Dryja & Widlund (1987) and extensively used by Fisher and co-authors (Fisher 1997; Lottes & Fisher 2005) in the context of computational fluid mechanics with SEM, remain to be explored for elastic wave propagation in the time domain, see also Pasquetti *et al.* (2005). Even though numerical results do suggest stability scaling in $\mathcal{O}(N^{-2})$ for the time step of the explicit time stepping in two dimensions, exploring in this context semi-implicit time stepping may be interesting. In the spectral domain, investigating the use of TSEM is of particular interest since a Helmholtz problem has to be solved for each frequency and eventually multiple sources. The geometrical flexibility and the spectral accuracy of the TSEM, in conjunction with an overlapping Schwarz iterative method, appear quite attractive with important implications

for exploration geophysics. In both cases, an important related issue is to investigate the conditioning property of the TSEM for elastic wave simulation.

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APPENDIX A: ANALYTICAL SOLUTION FOR THE INCIDENCE OF PLANE P WAVES UPON AN ELASTIC CYLINDRICAL INCLUSION

This solution is well known after the classical work by Jing & Truell (1956). It was summarized later by Pao & Mow (1973) and can be obtained after the expansion of potentials in polar coordinates. Recently Liu *et al.* (2000) presented the treatment for viscoelastic materials and choose to give explicitly the coefficients of the

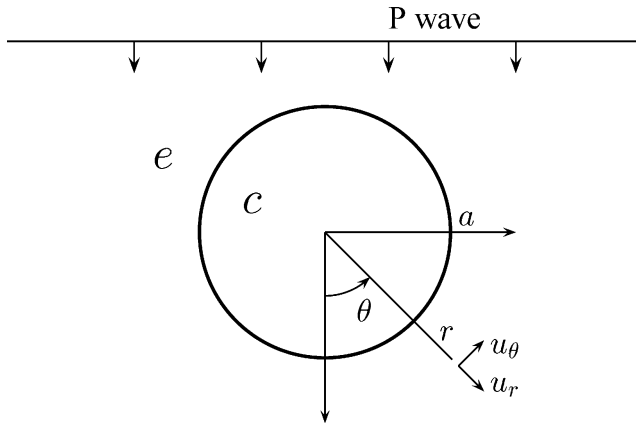


Figure A1. Incoming plane P wave upon the elastic cylindrical inclusion.

expansions. Here, we give the coefficients for the displacements and the relevant stress components as in Pao & Mow (1973) with slight modifications to account for our particular example.

With reference to Fig. (A1) consider the incoming plane wave $u_z^{(0)} = \exp(-iq_e z) \exp(i\omega t)$, $u_x^{(0)} = 0$, with q_e the P wavenumber in the region e . It can be shown that the corresponding scalar potential is simply $\Phi^{(0)} = \frac{1}{q_e} \exp(-iq_e z) \exp(i\omega t)$, which can be expanded using Neumann's expansion in a series of Bessel functions which are series of solutions of the elastic equation. In what follows we neglect the stationary term $\exp(i\omega t)$. In order to consider the waves scattered out and refracted within the cylinder, we use the potentials Φ for P waves and Ψ for S waves, both in the exterior region e and within the interior region c :

$$\Phi^e = \sum_{n=0}^{\infty} B_n^{(0)} J_n(q_e r) \cos(n\theta) + \sum_{n=0}^{\infty} B_n H_n^{(2)}(q_e r) \cos(n\theta), \quad (A1)$$

$$\Psi^e = \sum_{n=1}^{\infty} C_n H_n^{(2)}(k_e r) \sin(-n\theta), \quad (A2)$$

$$\Phi^c = \sum_{n=0}^{\infty} D_n J_n(q_c r) \cos(n\theta), \quad (A3)$$

$$\Psi^c = \sum_{n=1}^{\infty} E_n J_n(k_c r) \sin(-n\theta), \quad (A4)$$

where $B_n^{(0)} = (i/q_e)(-i)^n \varepsilon_n$, with $\varepsilon_n = 1$ for $n = 0$ and $\varepsilon_n = 2$ for $n \geq 1$ (Neumann's factor) are the coefficients of the incoming P wave, the P and S wavenumbers are $q_{(e,r)} = \omega/V_{p(e,r)}$, $k_{(e,r)} = \omega/V_{s(e,r)}$, respectively, and J_n are the Bessel functions of the first kind, Y_n the Bessel functions of the second kind, and $H_n^{(2)} = J_n - iY_n$ the Hankel functions of the second kind (Abramowitz & Stegun 1972).

These potentials give the displacement fields in cylindrical coordinates by means of

$$u_r = \frac{\partial \Phi}{\partial r} + \frac{1}{r} \frac{\partial \Psi}{\partial \theta}, \quad (A5)$$

$$u_\theta = \frac{1}{r} \frac{\partial \Phi}{\partial \theta} - \frac{\partial \Psi}{\partial r}. \quad (A6)$$

Substituting the potentials (A2) and (A4) in these equations, and using the notation of Pao & Mow (1973), we obtain

$$u_r^e = \frac{1}{r} \left[\sum_{n=0}^{\infty} (B_n^{(0)} E_{71}^{(1)}(q_e r, n) + B_n E_{71}^{(2)}(q_e r, n) + C_n E_{72}^{(2)}(k_e r, n)) \cos(n\theta) \right], \quad (A7)$$

$$u_r^c = \frac{1}{r} \left[\sum_{n=0}^{\infty} (D_n E_{71}^{(1)}(q_c r, n) + E_n E_{72}^{(1)}(k_c r, n)) \cos(n\theta) \right], \quad (A8)$$

$$u_\theta^e = \frac{1}{r} \left[\sum_{n=1}^{\infty} (B_n^{(0)} E_{81}^{(1)}(q_e r, n) + B_n E_{81}^{(2)}(q_e r, n) + C_n E_{82}^{(2)}(k_e r, n)) \sin(-n\theta) \right], \quad (A9)$$

$$u_\theta^c = \frac{1}{r} \left[\sum_{n=1}^{\infty} (D_n E_{81}^{(1)}(q_c r, n) + E_n E_{82}^{(1)}(k_c r, n)) \sin(-n\theta) \right], \quad (A10)$$

where

$$E_{71}^{(i)}(z, n) = E_{82}^{(i)}(z, n) = n C_n^{(i)}(z) - z C_{n+1}^{(i)}(z), \quad (A11)$$

$$E_{72}^{(i)}(z, n) = E_{81}^{(i)}(z, n) = n C_n^{(i)}(z), \quad (A12)$$

and the functions $C_n^{(i)}$ are

$$C_n^{(i)}(z) = \begin{cases} J_n(z) & i = 1, \\ H_n^{(2)}(z) & i = 2. \end{cases}$$

The needed coefficients B_n , C_n , D_n , E_n for both the exterior and the interior expansions are obtained from the fulfilment of boundary conditions of continuity of displacements and tractions at the interface $r = a$. The relevant stress components for the cylinder are given in terms of the potentials as

$$\sigma_{rr} = \lambda \nabla^2 \Phi + 2\mu \left[\frac{\partial^2 \Phi}{\partial r^2} + \frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial \Psi}{\partial \theta} \right) \right], \quad (A13)$$

$$\sigma_{r\theta} = \mu \left[2 \left(\frac{1}{r} \frac{\partial^2 \Phi}{\partial r \partial \theta} - \frac{1}{r^2} \frac{\partial \Phi}{\partial \theta} \right) + \frac{1}{r^2} \frac{\partial^2 \Psi}{\partial \theta^2} - r \frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial \Psi}{\partial r} \right) \right]. \quad (A14)$$

After substitution of potentials (A2) and (A4), and using again Pao & Mow (1973) notation, we obtain

$$\sigma_{rr}^e = \frac{2\mu_e}{r^2} \left[\sum_{n=0}^{\infty} (B_n^{(0)} E_{11}^{(1)}(q_e r, n) + B_n E_{11}^{(2)}(q_e r, n) + C_n E_{12}^{(2)}(k_e r, n)) \cos(n\theta) \right], \quad (A15)$$

$$\sigma_{rr}^c = \frac{2\mu_c}{r^2} \left[\sum_{n=0}^{\infty} (D_n E_{11}^{(1)}(q_c r, n) + E_n E_{12}^{(1)}(k_c r, n)) \cos(n\theta) \right], \quad (A16)$$

$$\sigma_{r\theta}^e = \frac{2\mu_e}{r^2} \left[\sum_{n=1}^{\infty} (B_n^{(0)} E_{41}^{(1)}(q_e r, n) + B_n E_{41}^{(2)}(q_e r, n) + C_n E_{42}^{(2)}(k_e r, n)) \sin(-n\theta) \right], \quad (\text{A17})$$

$$\sigma_{r\theta}^c = \frac{2\mu_c}{r^2} \left[\sum_{n=1}^{\infty} (D_n E_{41}^{(1)}(q_c r, n) + E_n E_{42}^{(1)}(k_c r, n)) \sin(-n\theta) \right], \quad (\text{A18})$$

where

$$E_{11}^{(i)}(z, n) = \left[\left(n^2 - n - \left(\frac{V_p}{V_s} \right)^2 \frac{z^2}{2} \right) C_n^{(i)}(z) + z C_{n+1}^{(i)}(z) \right], \quad (\text{A19})$$

$$E_{12}^{(i)}(z, n) = [(n^2 - n) C_n^{(i)}(z) - n z C_{n+1}^{(i)}(z)], \quad (\text{A20})$$

$$E_{41}^{(i)}(z, n) = E_{12}^{(i)}(z, n), \quad (\text{A21})$$

$$E_{42}^{(i)}(z, n) = \left[\left(n^2 - n - \frac{z^2}{2} \right) C_n^{(i)}(z) + z C_{n+1}^{(i)}(z) \right]. \quad (\text{A22})$$

It is convenient to express the continuity conditions at the cylinder interface as

$$\left. \begin{aligned} u_r^e &= u_r^c, \\ \sigma_{rr}^e &= \sigma_{rr}^c, \\ u_\theta^e &= u_\theta^c, \\ \sigma_{r\theta}^e &= \sigma_{r\theta}^c \end{aligned} \right\} \quad \text{at } r = a. \quad (\text{A23})$$

This leads to a linear system of order 4 for each n (for $n = 0$ the order is 2, which means there are only P waves for $n = 0$) to retrieve the expansion coefficients B_n , C_n , D_n and E_n . After solving the system, and using (A7) and (A9), we obtain the displacement field in cylindrical coordinates which can be transformed to the original Cartesian axis via

$$u_x = u_r \sin \theta + u_\theta \cos \theta, \quad (\text{A24})$$

$$u_z = u_r \cos \theta - u_\theta \sin \theta. \quad (\text{A25})$$

We find that adding up to 80 terms in the sums (A7) and (A9) are sufficiently enough for our purposes. The final synthetic seismograms are obtained after convolution with a Ricker wavelet spectrum and Fourier transforming back to the time domain using the FFT.