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Abstract: Pearl River Mouth Basin (PRMB) is a typical episodically rifting basin, and its sediment records exhibit a multistage infilling process. To build the coupling relationship between the spatial variability of tectonic movement and sediment dispersal pattern, we character the source-to-sink system distribution within continental margin and analysis their dominated factors with quantitative statistical methods. First, we identify the faults and calculate the rifting rate by interpreting the two-dimensional (2D) seismic data and zircon or apatite fission-track data (ZFT/AFT). Accordingly, based on the various trending of the rifting rate evolution, we classified rifting process episodically into three patterns: accelerated rifting decelerated rifting, and uniform rifting. Then, we integrated the data available on detrital zircon U–Pb, rare earth element, and heavy mineral assemblage to identify the responding S2S components associated with the above various rifting processes. Results show that in the first tectonic stage during the early Eocene, the sediments were mainly sourced from an intrabasin provenance area, whereas in the late Eocene to the Oligocene, the paleo-Pearl River provided the sediments to the sink area. We restore the facies association of the sink area by studying the core samples, electric well logs, and three-dimensional (3D) seismic data. During the accelerated and uniform rifting processes, coarse-grained deposited along the boundary faults, which includes the fan delta and subaqueous fans. During decelerated rifting, the depositional environment was dominated by braided channels, meandering channels, and tide-influenced channel accretion. Based on the quantitative analysis the relationship between the grain size of the sediment in each S2S segment and the rifting rate, more fine-grained components were preserved in the decelerated rifting system, while coarse-grained sediments fill the accelerated rifting depression and uniform rifting components. Furthermore, the sediment supply and relative height can influence the volume of the S2S system in

the uniform rifting system. In the decelerated rifting basin, the sediment supply is the major factor associated with the development of S2S, whereas the relative height is the major factor associated with the accelerated rifting basin.

Keywords: North Pearl River Mouth Basin, Source-to-sink system, Detrital zircon U–Pb data, Rifting Process

## 1. Introduction

The Pearl River Mouth Basin (PRMB) (**Fig. 1**) is a typical episodically rifting basin (*Li and Rao., 1994*) that can be attributed to the impact of the convergence of the Pacific, Eurasian, and Indo–Australian plates. During the Paleogene epoch, the PRMB framework was determined by two stages of rifting: the Zhuqiong I and Zhuqiong II phases (*Li and Rao, 1994; Wu et al., 2016; Ge et al., 2017; Shao et al., 2017; Wang et al., 2019*). PRMB is an ideal case that can be studied to explore the infilling process associated with a continental margin in case of an episodically rifting basin, including sediment transport and the sediment dispersal pattern in the sink area (*Wang et al., 2019*). In this study, we aim to establish the infilling process of the episodic rift basin based on the insights obtained from the case study of source-to-sink (S2S) in the Pearl River Mouth Basin.

Previous studies have indicated that the basin structure and the geomorphology change caused by rifting tectonic movement would lead to the spatial and temporal variability during the filling process (*Keen and Dehler., 1993; Ziegler and Cloetingh., 2004; Li et al., 2020; Tang et al., 2020*). *Martin et al., (2009)* and *Paola and Martin., (2012)* have reworked a credible filling process in a simple rifting basin, which characters by a single simple rifting process defined as *Merle (2011)*. However, as to the more complex infilling process in the episodic rift basin, the relation between sediment infilling and the tectonic processes remains unclear, especially with regard to the relation between multiple stages, during which the rifting rate is observed to change. Some studies indicate that the infilling process in various stages is independent of the rifting rate, whereas others indicate that the former process is affected by the latter (*Li and Rao., 1994; Xie. et al., 1996; Mugisha et al., 1997; Shao et al., 2018; Xie et al., 2019*).

Further, we focus on the cause to spatial and temporal variability during the filling process. *Saneyoshi et al., (2006), Cao et al., (2018) and Wu et al., (2019)* have stated that internal factors, such

as the fault stack patterns or rifting rate, would influence the sedimentary process, whereas *Gawthorpe et al.*, (2003), *Pascucci et al.*, (2000), *Juillet et al.*, (2014) and *Favre et al.*, (2015) focused on external factors such as sediment supply or the rework process. In the case of the PMRB, all the aforementioned factors continuously changed during the Eocene to Oligocene epochs (*Wang.*, 2015; *Xie et al.*, 2019). Lots of publishes have also investigated the infilling process with respect to the change in the source-to-sink system (*Li and Rao.*, 1994; *Ren et al.*, 1996; *Jiao et al.*, 1997; *Liu et al.*, 2013; *Wang.*, 2015; *Lin. et al.*, 2018). They rebuild the provenance area(*Wang et al.*, 2019), volcanic activity (*Li and Rao* 1994) and deposition process in the sink area (*Wang.*, 2015; *Xie et al.*, 2019). However, because of data limitation, they did not evaluate the planar distribution of the sediment from the paleo-river during the Eocene to Oligocene epoch.

In this study, we initially clarify the rifting process. Based on previous studies related to study methods (*Li and Rao*, 1994; *Yi et al.*, 2009; *Li et al.*, 2018), we integrated thermochronology data analysis and seismic interpretation to calculate the rifting rate and classify their types. Subsequently, we characterized the regional uplift or subsidence in the northern depression zone (NDZ). Based on these analyses, the NDZ can be divided into three subregions according to the different insights obtained with respect to the rifting process when the rifting rate is varied over time, 1) accelerated rifting, which indicates an increasing extension rate during the rifting process, 2) decelerated rifting which represent a decelerating extension process, and 3) uniform rifting systems, which character by its uniform extension process. Then, as the S2S system is reconstructed, we integrate the heavy mineral assemblage and detrital zircon U–Pb data to estimate the sediment transport distance. Additionally, we can obtain the quantitative parameters of the system spatially and temporally based on the interpreted three-dimensional (3D) seismic data. Subsequently, we explain the dominant factors associated with the change in grain size observed in the S2S system during the infilling process.

## 2. Geological setting

The PRMB is divided into three parts from north to south: northern depression zone (NDZ), central uplift, and southern depression zone (SDZ). As to the NDZ, *Li and Rao*, (1994) point out that the western part show character as several small sags developed with NEE-directional normal faults, while the east part is mostly big sags controlled by the faults boundaries. Thus, we name the east part in

NDZ as Zhu I Depression or Western NDZ, and the west part as Zhu III depression (Pearl River name as *zhuyang* in Chinese, where *zhu*=Pearl, and *jiang*=river). Furthermore, Zhu I Depression, which covers an area of  $4.2 \times 10^4$  with hydrocarbon-rich sag like Huizhou, Enping, Xijiang, can be divided into two parts, as the eastern Zhu I Depression (Eastern NDZ), and the west Zhu I Depression (Central NDZ) according to their locations (**Fig. 1**).

With respect to the form obtained via impact based on the seafloor spreading of the South China Sea, the tectonic stage of PRMB can be divided into two phases (**Fig. 1**): a syn-rifting process during the late Cretaceous or Paleocene to the early Oligocene, and post-rifting from the late Oligocene to present (Li and Rao, 1994; Li et al., 2014 and 2015; He et al., 2017; Shao et al., 2018 Wang et al., 2019; Xie et al., 2019). The syn-rifting stage can be further divided into three phases: Shenhu movement, Zhuqiong I phase tectonic movement, and Zhuqiong II phase tectonic movement (**Fig. 1**). The Shenhu movement can be observed for a short duration and exhibits limited influence (Li and Rao, 1994). Thus, in this study, we focus on the rifting process of the Zhuqiong I and Zhuqiong II phase tectonic movements.

## 2.1 Tectonic stage

Previous studies indicate that the multiple stages of episode rifting in the north PRMB can be attributed to the extension of the paleo-South China Sea and the rotation of the Indochina and Cathaysia blocks (Shao et al., 2017; Cao et al., 2018). Since the Eocene, the corresponding dominant tectonic stress was transferred from the northwest to the southwest direction (**Fig. 2**) (Li and Rao, 1994; Morley., 2016). Furthermore, the relative motion of the Pacific and Asia plates caused the development of NDZ as a wide rifting pattern (Buck., 1991; Engebretson et al., 1984; Suo et al., 2019). The profiles in **Fig. 2** obtained with respect to the interval of the early Eocene shows that several separate sags or half-grabens developed on the NDZ with a high rifting rate. The average rifting rate was 100 m/Ma; the its maximum became 200 m/Ma (Engebretson et al., 1984; Li and Rao, 1994; Morley., 2016; Torsvik et al., 2019).

In the Oligocene, because of the increasing velocity of the Pacific plate subduction (Morley., 2002; Torsvik et al., 2019) and the convergence of the Asian and Indian plates (Tapponnier et al., 1990; Deng et al., 2017; Shao et al., 2017), the rotation of the Cathaysia block led the second rifting process (Jiao

*et al.*, 1997; *Morley.*, 2002; *Lin et al.*, 2004; *Liu et al.*, 2013; *Wang.*, 2015). Thus, when the source-to-sink system shifted from a wide pattern (S2S system have large catchments and wide shelves of low gradient bathymetry) to a narrow pattern (S2S system characterized by steep and short catchments), the spatial location variability of the aforementioned sags or half-grabens in NDZ exhibited a different rifting process (*Buck.*, 1991; *Li and Rao*, 1994).

## 2.2 Sedimentary setting

According to the drilling data obtained in each depression (**Fig. 3**), the Paleogene (from bottom to top) comprises Shenhu Formation ( $E_1s$ ), Wenchang Formation ( $E_2w$ ), Enping Formation ( $E_2e$ ), Zhuhai Formation ( $E_3z$ ). By calibrating the well-log and seismic data (*Wu et al.*, 2016; *Ge et al.*, 2017), the bottom  $E_2w$  is called Tg, the bottom  $E_2e$  is T80, and the bottom  $E_3z$  is T70 (**Fig. 4**).

Shenhu Fm. can be observed in a limited area in PRMB, and the alluvial fan was observed to develop in this interval (*Morley.*, 2016; *Wang et al.*, 2019). The lithology mainly comprises coarse sandstone and fine-grained red gravel. Some volcanic rocks, including the lava, tuff, and volcanic clastic rocks, were observed to develop in the Eastern NDZ in Shenhu Fm. as *Li and Rao (1994)*'s study. Wenchang Fm. was generated in each separate sag during the first rifting stage. Thick mudstone with siderite also developed. *Hu et al.*, (2012), *Peng et al.*, (2017) and *Ge et al.*, (2018) pointed out that the northern and southern depression zones are lacustrine setting in this interval insight from the biomass and trace element data. Enping Fm. can be divided into two members, i.e., top and bottom, according to the difference in lithology. The bottom layers are mainly interbedded sand and mudstone, whereas the upper layer includes thick mudstone or some thin coal layers. The interval of Zhuhai Fm. mostly developed in the late part of the second rifting stage. Gray sandstone with glauconite developed during this interval (*Lin et al.*, 2018).

## 3. Data and method

### 3.1 Research data

The block in PRMB included 1892.9 km of 2D seismic data and 1500 sq. km. of 3D high-resolution seismic data. A total of 21 wells drilled in PRMB were selected, and the positions of the cross-well seismic sections are shown in **Fig. 1c**. The electric well-log curves, including gamma rays, were acquired and processed by Schlumberger. The cored intervals were observed in wells F, E, C, and B

(Fig. 5). The rare earth element (REE) content and heavy mineral analyses in wells F, E, C, B, and M were conducted by the Geological Laboratory of Research Institute of Shenzhen Corporation of China National Offshore Oil Corporation.

The fission-track (FT) analysis of wells L, H, O, P, J and G was conducted by the Institute of High Energy Physics, Chinese Academy of Sciences. The data of well K refer to the study of *Li et al., (2018)*. The sample was covered by muscovite and the reactor irradiated with standard uranium glass UB2 and standard age sample FC3. The radiant thermal neutron flux of the apatite sample was  $5.5 \times 10^{15} \text{ cm}^{-2}$ , and the neutron flux of the zircon samples was  $1.5 \times 10^{15} \text{ cm}^{-2}$ . After irradiation, the external detectors were etched using 40% HF at 20 °C for 20 s. Then, we obtain the FT density and length, as described by *Green et al., (1985)*, through analysis using the Auto Scan system. The sample ages were determined using the zeta calibration method and recommended age standards (*Hurford and Green., 1983; Green et al., 1985*) (**Table 1**). The ZFT central age was  $366 \pm 9.6 \text{ Ma}$ , and the ATF central age was  $381.8 \pm 7.3 \text{ Ma}$ .

U–Pb dating of the four samples (well F 3917.5, well E 4155.5, well C 2580.1, and well B 2581.1m) via LA–ICPMS analysis was conducted by the Chinese Academy of Geological Sciences (**Appendix TableS 1–4**). Laser ablation was performed using the NWR193UC 193-nm deep ultraviolet laser ablation sampling system (Elemental Scientific Lasers, United States). Agilent 7900 inductively coupled plasma mass spectrometry (Agilent, US) was also conducted. 120 detrital zircons from each sample were analyzed with a spot size of 30  $\mu\text{m}$ . Every five analyses were followed by one analysis of standard zircon 91500, and GJ-Common lead correction was conducted using ComPbCorr#3\_15G. The U–Pb age calculations and concordia diagram were completed on IsoplotR software provided by University College London, United Kingdom (<http://pieter-vermeesch.es.ucl.ac.uk/shiny/IsoplotR/>). Only the zircon ages concordant within 90%–110% are discussed in the following.

### 3.2 Research methods

1) A method to reconstruct the rifting process with 2D seismic data and apatite and zircon FT data.

We rebuild the rifting process according to the 2D seismic data interpretation and calculate its rifting rate based on the Apatite fission-track/ Zircon fission-track (AFT/ZFT) data.

In this study, we refer to the thermal history modelling put out by Laslett et al., (1987), and the

AFTslove ® software to simulate the thermal history. We input the parameters, including the single grain age error, number of induced/spontaneous fission tracks, length of the combined track length and the C-axis angle. Then, restricted by the sample's depth and their responding terrestrial heat flow as Jiang et al., (2019), we get the T-t(Temperature-time) path (104 simulation curves for each sample). Finally, we check the simulation results with k-s testing and Age GOF parameter evaluation, which show a credibility simulation with the check value over 5%, and a high-quality simulation with the value over 50%.

As the stable late compaction process in the PRMB (Dong et al., 2009), we can evaluate the rifting rate according to the average fault displacement and average strata thickness. Firstly, as the mudstone and sandstone show various compaction coefficient, we pre-compact the strata thickness using the compaction coefficients of  $0.51 \text{ km}^{-1}$  for mudstone and  $0.27 \text{ km}^{-1}$  for sandstone and calculated average strata thickness is  $H$ (Ma et al., 2019; Wu et al., 2019).

Then, rifting rate is represented as  $\sigma(x,t)$ . The basement-elevated height is  $\eta(x)$ , which can get from the seismic data interpretation. The time of rifting interval is  $T$ . The rifting rate can be calculated as

$$\sigma(x, t) = (\eta(x) + H)/T, \quad (\text{Equation 1})$$

Based on the inversion method applied in previous studies (Yi et al., 2009; Li et al., 2018), we calculated  $\eta(x)$  based on the inversion of AFT/ZFT data (Table 1).  $T$  is time, which can be obtained from the detrital zircon U-Pb data and well seismic calibration.

2) A method to identify the provenance area by combining the heavy mineral assemblage and detrital zircon U-Pb data.

By combining the results of previous studies on the provenance area of the NDZ during the Eocene (Wang et al., 2019; He et al., 2020), we established a mean U-Pb age distribution in the NDZ. By integrating the age data on the basement rocks with the tectonic background, we identified the provenance transfer from the Eocene to the Oligocene. We can infer the provenance based on the chemical activity of rare earth element (REE) by comparing the REE distribution of the fine-grained stone in NDZ and the possible source area. In this study, with regard to the REE pattern distribution around PRMB, we refer to the study conducted by Ma et al. (2016) and Shao et al. (2018). Then, we

combined the heavy mineral assemblage (HMA) with the zircon–tourmaline–rutile (ZTR) index, speculated on the provenance area of the sediment, and evaluated its distance from the dispersal area (Fu et al., 2019).

### 3) Quantitative evaluation of the volume of each segment in the S2S system.

We can determine the amount of quantitative geological information, including sediment composition, infilling process, and sink area distribution, through a detailed analysis of the seismic data (Anell and Midtkandal., 2015; Lin et al., 2018; Zhuo et al., 2019).

The 2D seismic data can provide insights based on which we can rebuild the paleo-morphology during the episodic rifting process. After the seismic interpretation and compaction removal, we reconstruct the geomorphology map of Wenchang Fm. and Enping Fm.

Then, we rebuild the sink area and sedimentary facies association according to the 3D seismic data interpretation. We identified three seismic facies (concave, linear, and sigmoidal) based on their seismic boundaries. They can be interpreted as a channel or sediment pathway, channel distributary or semi-deep lake-deep lake fine-grained deposit, and fan delta or subaqueous delta, respectively. Accordingly, we determine the dispersal area of the S2S system and build the accretion pattern in each sag spatially.

### 4) Analysis of the filling process based on the mass balance theory.

To study the S2S system and simple extension rifting setting, Paola and Martin., (2012) proposed the mass balance theory to recover the infilling process. If compaction is ignored, then the relation between the rafting rate ( $\sigma(x,t)$ ) and the amount of sediment supply ( $Q_{total}$ ) can be shown as

$$Q_{total} = \frac{1}{\chi(x)} \int_0^x (\sigma(x,t) + \eta(x)) dx, \quad (\text{Equation 2})$$

where  $\chi(x)$  is the mass balance coordinate (or mass loss) and  $x$  is the distance from the source to the sink.

Because the fluvial–deltaic system is dominant in the PRMB during the rifting stage (Wu et al., 2016), the relative height is determined by the thickness of the clinoform (Chen et al., 2019; Steel et al., 2019) and the rifting rate, as shown in **Equation 1**. Then, based on the fluvial–deltaic model (Hampson et al., 2014), the sediment migration distance is  $u(x)$ . Thus, **Equation 2** can be rewritten as

$$Q_{total} = \frac{a}{\chi(x)} \cdot u(t) \cdot \sigma(x,t) + b, \quad (\text{Equation 3})$$

where  $a$  is the rifting interval (Eocene to Oligocene) and  $b$  is the thickness of the fine-grained sediment provided via suspension and flocculation.

Further, we can determine the rifting rate (plotted as  $\sigma(x,t)-x$  in the work of *Hampson et al., (2014)*), sediment migration distance ( $u(x)$ ), and amount of sediment supply ( $Q$ ). By inserting all the aforementioned variables into **Equation 3**, we can obtain the relation between the mass balance coordinate (mass loss)  $\chi(x)$  and the sediment migration distance  $x$  (dimensionless); this plot is also called mass extraction profile as defined by *Michael et al. (2014)*.

Based on previous studies, the profile of mass balance coordinate (mass loss)  $\chi(x)$  can serve as an index of grain size distribution (*Martin et al., 2009; Paola. and Martin M., 2012; Michael et al., 2014; Michael et al., 2014*). Thus, we build an identification chart of the aforementioned variable and infilling process based on the S2S system. This identification chart refers to the global continental margin infilling pattern proposed by *Sømme et al. (2013); Gong et al. (2016); Nyberg and Howell (2016); and Nyberg et al. (2018)*. In the chart, the S2S system is classified as proximal and distal provenance area systems. Then, according to the mass balance coordinate (mass loss)  $\chi(x)$ , coarse-grain fan dominated ( $\chi(x) < 0.25$ ), sandy pro-graded delta-dominated ( $0.25 < \chi(x) < 0.75$ ), and reworking sediment-dominated ( $0.75 < \chi(x) < 1.0$ ) data (*Sheets, B. A. et al., 2002; Michael et al., 2014*), we can rebuild the infilling process by responding to different rifting processes. Furthermore, we can evaluate the dominant factors in the infilling process using the volume plotting of each S2S system segment in the bubble chart (*Fu et al., 2019*).

#### 4. Lithofacies identification

The grains of the sediments in the PRMB during the Eocene and Oligocene range from mudstone to fine conglomerate. With respect to the reworking process, we classified the deposit into ten types, namely, massive mudstone (**M**), bioturbated sandstone (**Sb**), muddy strip composite sandstone (**Scm**), deformation sandstone (**Sd**), crossbedding composite sandstone (**Sc**), crossbedding sandstone (**Sc**), massive sandstone (**Sm**), planar crossbedded sandstone (**Sp**), massive gravel (**Gm**), and planar cross bedded gravel (**Gp**). The above lithofacies associations were identified and classified based on the cores from wells F, E, C, and B (**Fig. 5**), and the detail description were added in **Table.2**.

#### 5. Seismic data interpretation

## 5.1 Wenchang “A” Sag in Western NDZ (Section 1)

As shown in profile A (**Fig. 6**), the Wenchang “A” Sag is a typical half-graben controlled by a boundary fault. We divided the sag into three layers, i.e., Wenchang Fm. (Tg–T80), Enping Sag (T80–T70), and Zhuhai Fm. (T70–T60) according to the aforementioned well calibration. The average strata thickness of Wenchang Fm. is 300–700 m. Enping Sag and Zhuhai Fm. exhibit similar thickness values of 300 and 280 m, respectively.

To characterize the infilling process, we select a profile that passes through the center of the Wenchang “A” Sag (section location in **Fig. 1**). In the Wenchang Fm. interval, the seismic continuity event in the Wenchang “A” Sag indicates the development of a fine-grained delta, and we can distinguish four phases of the pro-graded delta from the profile (**Fig. 6**). Considering the volume of this delta, an average thickness of 30–50 m and a pro-graded distance of 100 km can be obtained. Furthermore, in the inner seismic package of the pro-graded delta, we can distinguish between several channels according to the convex seismic facies. These channels developed with later migration and small erosion. The cutoff of these channels indicated a pathway area of 1.3–3 sq. km. In the southern Wenchang “A” Sag profile, we can distinguish between two phases of fan delta (or subaqueous fan) with an average volume of 0.5–1.0 sq. km.

In the Enping Fm. and Zhuhai Fm. interval, we can distinguish between an alluvial delta or fan delta, where each phase has an average volume of 1.5 sq. km. and 0.7 sq. km., respectively.

## 5.2 Enping Sag in Central NDZ (section 2)

As indicated by profile B (**Fig. 7**), Enping Sag is an atypical half-graben. The faults in the south have a displacement of more than 200 m, and the fault in the north can be attributed to syngeneic deposition. The profile can also be divided into three layers (Wenchang Fm., Enping Fm., and Zhuhai Fm.). In the Wenchang Fm. interval, we can distinguish between several seismic packages with a concave or lenticular shape at the bottom. The inner chaotic event shows a fast infilling process, which can be interpreted as a deposited fan delta or alluvial fan. The thickness became 80 m and is related to the volume of these pro-graded sediments. Then, upward to Enping Fm., according to the onlap seismic event in **Fig. 7**, we distinguish between three phases of the delta with an average thickness of 30–50 m.

### 5.3 Huizhou Sag in Eastern NDZ (section 3)

*Fig. 8* is considered as an example to restore the infilling process. We first identified the faults along the slope and calculated the breaking distance at 20 m in Wenchang Fm. and 25 m in Enping Fm. Then, according to the well calibration and seismic reflection, the faults are divided into three layers: Wenchang Fm., Enping Fm., and Zhuhai Fm. In Wenchang Fm., the seismic facies with a clear concave and lenticular boundary exhibit an inner chaotic event, indicating the fast infilling process. Upward to the Enping Fm. interval, a series of pro-graded deltas can be observed from the south and north uplifts. The average thickness in the south is 57 m, whereas that in the north is 35 m.

## 6. Results

### 6.1 Apatite/zircon FT data

Refer to the former research in South China (*Yi et al., 2009; Li et al., 2018*), the FT thermochronometric method in this study can be used to reconstruct the rifting process and prove the paleo-morphology rebuilding. Based on the work conducted by *Yi et al. (2009)*, the cooling temperature of zircon is  $210 \pm 18$  °C and that of apatite is 60 °C–120 °C. The histogram of the fission track in wells O and P show multiple peaks, whereas that of the fission track in wells H, G, J and L is a one-peak pattern (**Fig. 9**), indicating that the thermal flow and rifting process of NDZ are heterogeneous in case of planar distribution.

All the grain ages of wells L, H, and G pass the  $\chi^2$  test (5%); these ages can be calculated as pool age, which is estimated as the ratio of spontaneous track density to induced track density. This indicated that these grains may have annealed thoroughly during the Paleogene. The  $P(\chi^2)$  of wells O and P is less than 5%; these ages were the central age. Based on the thermal flow associated with PRMB (*Yuan et al., 2009; Li et al., 2018*), the grains in wells O and P may not reach the cooling temperature of the apatite and exhibit low thermal flow at the above well location (Enping Sag in Central NDZ).

The average of the AFT in NDZ range from 11.37 to 13.16  $\mu m$ , and its standard deviation ( $\sigma$ ) is 1.14~3.01  $\mu m$ . The inversion results obtained using paired minerals indicate that the cooling rates of wells L, O, and P, J, G, are 1.66, 4.31, 15.25, 1.91, and 2.50 °C/Ma, respectively. Then, as the geothermal gradient in various sags (*Yuan et al., 2009*), the uplifts of wells L in the western NDZ

character by the uplifting rate of 0.038 km/Ma and the calculated basement-elevated height( $\eta(x)$ ) is 0.56 km in the early Eocene and 0.26 km in the late Eocene. The average uplifting rate of Central NDZ (the well O 0.113 km/Ma and P 0.48 km/Ma) is 0.30km/Ma. Well J and G shows the uplifting rate in the Eastern NDZ, which is 0.057 and 0.089 km/Ma, respectively.

## 6.2 U–Pb detrital zircon data

Detrital zircons U-Pb age data are used to constrain the potential source area of sediments deposited in the PRMB during the Eocene and Oligocene. Four samples selected and representative zircon Cathodoluminescence (CL) images are shown on **Fig. 10**. Concordia plots in **Fig.11** and individual age spectrums in **Fig.12**.

The zircon in the late Eocene is colorless and is mostly in an elliptical shape. According to the CL image, the long-axis zircon is 90–120  $\mu\text{m}$ . According to the internal structures, zircon can be classified into three types (**Fig. 10**). The first type is a subangular shape with a length-to-width ratio of 1:1. This type of zircon shows a dark magmatic oscillatory zone that can be observed from the cathodoluminescence (CL) images. This type accounts for 60% of each sample, and the age range is 145–23.3 Ma. The second type is a sub-round shape with a length-to-width ratio of 3:1. This type of zircon shows a clear magmatic oscillatory zone that can be observed in the CL images. The age is 443–145 Ma. The third type is a round shape with a length-to-width ratio of 2:1. The internal structure exhibits homogeneous or patchy zoning, and this type accounts for 20% of all the samples.

The age data associated with wells E, F, C, and B are presented in **Appendix Tables 1–4**. In this study, 345 detrital zircons were considered to be adequate. The zircon age data of the four samples can be classified into four groups: 100–200, 410–500, 250–280, and 2400–2500 Ma (**Fig. 11**).

The zircon of well F at a depth of 3917.5 m is the interval of Enping Fm. The U–Pb Concordia plots (**Fig. 11**) of all the grains display concordances of >90%. Its age spectrum shows that the zircon can be divided into five parts: 30–200, 200–300, 400–500, 600–750, and 750–1000 Ma (**Fig. 12**). Their corresponding peaks are 175, 245, 420, 710, and 880 Ma, respectively (**Fig. 12**). A sample of well E with a depth of 4155.5 m can be observed in Enping Fm., and all the grains show concordances of >90% (**Fig. 11**). Its age can be divided into two parts: 150–400 Ma (80%) and 400–500 Ma (17%). The samples from well C (with a depth of 2581.1 m) and well B (with a depth of 2580.1 m) are in the interval

of Enping Fm. In case of well B, the age spectrum is divided into two groups: 83–150 Ma (35% with a major peak at 120 Ma) and 165–500 Ma (55% with a major peak at 175 Ma).

The thorium-to-uranium (Th/U) ratio can reflect the lithologies of the provenance area. As shown in **Fig. 13**, for the Th/U ratio of the Eocene, we refer to the study conducted by Wang *et al.* (2019), which indicates a range of 0.125–1.36. For the Oligocene, the samples of wells F, E, B, and C in Enping Fm. exhibit Th/U ratios of 0.015–0.165. This condition indicates that a large volume of metamorphic rocks was injected into the sink area during the Oligocene.

### 6.3 Rare earth element (REE) content

In the Enping Fm. interval, the amount of  $\Sigma\text{REE}$  ( $540.9 \times 10^{-6}$ – $993.2 \times 10^{-6}$ ) in the samples from wells E and F is high. The LREE/HREE (Light rare earth/ Heavy rare earth) value is 3.02–6.79, the  $\delta(\text{Eu})$  value is 0.855–0.901, and the  $\delta(\text{Ce})$  value is 0.912–0.975. As indicated by the chondrite-normalized REE distribution patterns (**Fig. 14**), the REE in wells E and F eastern and central of NDZ shows LREE enrichment and HREE deficiency. The Eu content shows a slightly negative anomaly, whereas Ge is normal. The amount of  $\Sigma\text{REE}$  in the samples from wells C and B in the Western NDZ is  $602.2 \times 10^{-6}$ – $722.4 \times 10^{-6}$ . The LREE/HREE value is 1.98–2.66, the  $\delta(\text{Eu})$  value is 0.238–0.996, and the  $\delta(\text{Ce})$  value is 0.940–1.00. Similarly, as indicated by the chondrite-normalized REE distribution patterns (**Fig. 14**), the LREE in wells C and B are enriched, whereas HREE is deficient. The Eu and Ge contents are both normal.

In the *Wenchang Fm.* interval, the REE distribution data are obtained from the study conducted by Shao *et al.* (2018). The REE distribution in case of Eastern and Central NDZ shows that the LREE content is higher than the HREE content and that in case of the Western NDZ shows that the LREE content is less than the HREE content. Generally, the Eu content of the samples from NDZ shows a negative V shape.

### 6.4 Heavy mineral assemblage

#### 1) Heavy mineral assemblage in Eastern and Central NDZ

As shown in **Fig. 15**, the HMA in the Eastern and Central NDZ is observed to vary. In the Xijiang Sag (well E), the HMA comprises zircon–titanite–anatase–tourmaline. The well M in the Huizhou Sag comprises zircon–apatite–magnetite–barite. The sediment of well F has HMA comprising pyrite–

During the Eocene, the ZTR values of wells E, M, and F show a spatial difference and they are 70%, 35%, and 20%, respectively. Up to the Oligocene, wells E, M and F showed a sharply increase in ZTR value and saw a rising of the zircon content, suggesting that an increasing distal sediment was dominant in this interval.

## 2) Heavy mineral assemblage in Western NDZ

The HMA values associated with wells C and B show similar compositions, i.e., zircon–rutile–titanite–biotite. During the Eocene, the average ZTR index of Western NDZ was 30%. In the Oligocene, the average ZTR index increased to 57%. The ZTR index of well C increased drastically to 90%, whereas that of well B changed gradually. This condition indicates that the distal sediment influences Western NDZ and that the sediments may accumulate in some proximal areas as well.

## 7. Discussions

### 7.1 Rifting process reconstruction and classification

As interpreted from the seismic profile presented in **Fig. 16**, we can identify the faults, i.e., F1 to F33. Then, we calculate the average broken displacement from the Eocene to the Oligocene. Accordingly, we classified that the Western NDZ as a uniform rifting system, the Central NDZ (Enping and Xijiang Sags) as a decelerated rifting system, and Eastern NDZ as an accelerated rifting system.

#### 7.1.1 Uniform rifting system

The broken displacement in Wenchang “A” Sag remains at the same level during the rifting process (**Fig.16 a**). When compared with the thickness of T<sub>g</sub>–T<sub>80</sub>, the average strata thickness of T<sub>80</sub>–T<sub>70</sub> (450 m) does not change drastically. As the ZFT inversion results in well L (eastern NDZ), the time-temperature curve in **Fig. 9** reflects a multistage uplifting process in eastern NDZ during 64.9–27.3 Ma. Then, as indicated by the calculation of the rifting rate, the first rifting rate of 180 m/Ma can be observed in the first rifting stage (Eocene) and a rifting rate of 160 m/Ma can be observed in the second stage (Oligocene). Accordingly, this type of episodic rifting process can be referred to as a uniform rifting system.

#### 7.1.2 Decelerated rifting system

The Enping and Xijiang Sags are typical multistage half-grabens, which are controlled by boundary faults (F7, F12, F15, and F20) (**Fig. 10 b and c**). As indicated by the declining trend of the average fault displacement associated with these sags (F7–F20), fewer fault displacements occur in the Oligocene when compared with those in the Eocene. The time-temperature curve of the wells O, and P reflects the thermal evolution and uplift process of the Panyu Uplift (south of the Enping and Xijiang Sags) (**Fig. 9**). **Fig. 16** shows a fast uplifting rate in the first stage and a slow uplifting rate or slight subsidence in the second stage. As indicated by T80 and T70 in the seismic profile of **Figs. 3b and c**, considerable erosion can be observed at the interface. Accordingly, the rifting rates are 155 m/Ma in the Eocene and 90 m/Ma in the Oligocene.

Based on the tectonic characteristics of PRMB and their evolution history (*Li and Rao, 1994*), the center of NDZ is considered to be a decelerated rifting system.

### 7.1.3 Accelerated rifting system

Different from the aforementioned rifting processes, the structural framework of Huizhou Sag is controlled by two boundary faults (F21 and F33) and several sub-faults (F22–F32) (**Fig. 16 d**). According to the time-temperature curve of well G, the uplift rate is gentle in the first stage and accelerates drastically during the Oligocene (**Fig. 9**). Thus, based on the uplift rate and strata thickness, the rifting rate in the Eocene is 55 m/Ma, whereas that in the Oligocene is 110 m/Ma. Furthermore, as indicated by the increasing displacement of the fault, this type of episodic rifting process can be defined as an accelerated rifting system.

## 7.2 Source-to-sink system evolution during the rifting process

### 7.2.1 Provenance identification and its evolution process

#### 1) Provenance area during the early Eocene

##### (1) Wenchang Sag in western NDZ

As shown by the tectonic structure map (**Fig. 1**) and paleomorphology (**Fig. 15**), the Wenchang Sag was surrounded by the Yangchun low uplift in the north and Shenhu uplift in the south during the early Eocene interval. According to the study conducted by *Shao et al. (2016)* and *Wang et al. (2019)*, the ratio of  $Tu/U < 1$  (**Fig. 13**) indicated that the intermediate source mainly dominates the sediments in Wenchang Sag during the early Eocene. The REE distribution shows abnormal Eu content, LREE

enrichment, and HREE deficiency (**Fig. 14**). In comparison, it was considering the REE distribution pattern variety sharply with that in the Cathaysia plate (*Shao et al., 2016*). We speculated that the majority of the sediments are deposited in a proximal uplift area. Furthermore, the low ZTR index (<30%) (**Fig. 15**) can also provide evidence for short-distance transport.

## (2) Enping, Xijiang, and Huizhou Sags in the Central and Eastern NDZ

According to previous studies (*Shao et al., 2016; Liu et al., 2017; Wang et al., 2019*), as shown by the tectonic structure map in **Fig. 1** and the paleomorphology in **Fig. 15**, majority of the sediments during the early Eocene interval were provided by the northern fault terrace zone and the Panyu and Dongsha uplift in the south. The REE distribution pattern and low ZTR index (except for well E in Xijiang Sag) can provide evidence with respect to the proximal provenance area.

## 2) Provenance area during the late Eocene to Oligocene

### (1) Wenchang Sag in Western NDZ

In the age spectrum of wells B and C, the peak ages are 175 and 169 Ma, respectively. When these ages are compared with the peak age distribution in the Cathaysia plate (*Liu et al., 2017*), the peak age is similar to that in the Pearl River, as shown in **Fig. 11**. Besides that, As indicated by the REE distribution, the slightly abnormal Eu value indicated that some sediments are contributed by the upper crust, indicating that some deposits area eroded from the nearby uplift and injected into a proximal area. According to ZTR value in **Fig. 15**, well B and well C shows a variety of trending. Well C has an increasing ZTR value, whereas well B has a low ZTR index (52%). Thus, we speculate that the deposits in Wenchang Sag may involve distal and proximal sediments.

### (2) Enping and Xijiang Sags in Central NDZ

The peak age spectrum of the sediment from the Pearl River (including the northeastern and western Pearl River) and well E in Enping Sag (210 and 450 Ma) (**Fig. 11**) are observed in similar peak values. The ratio of Th/U in well E (**Fig. 13**) shows that some sediment in Enping Sag is the intermediated source from the Cathaysia plate and surrounding uplift. Thus, we infer that more distal sediment from is deposited in the Central NDZ. Besides that, the normal content of Eu and the rising ZTR index can provide evidence to the distal sediment accumulation.

### (3) Huizhou Sag in Eastern NDZ

By comparing the age spectrum in the Huizhou Sag and that in the west Pearl River (**Fig. 11**), well F is observed to exhibit similar age distributions. By combining the age data in the western and northern Pearl River (*Wang et al., 2019*), their peak values (275, 450, and 835 Ma in the western Pearl River and 145 and 450 Ma in the northern Pearl River) are observed to fit well with the grains in well F. Furthermore, the increasing ZTR index indicates that a considerable amount of the sediment is obtained from the distal area.

### 7.2.2 Depositional environment spatial variability in sink area

#### 1) *Depositional environment in the uniform rifting block*

We build the S2S system (**Figs. 17 and 19**) distribution in Eastern NDZ by integrating the aforementioned study into our findings. During the Eocene, the coarse-grained fan infilled to the sag along the NE directional faults. The pro-graded delta was dominant in the gentle south slope (**Fig. 18**). Then, in the Enping Formation, as the geomorphology in **Fig.15** shown, the area of the dispersal area increased during the second rifting process. Upper to Zhuhai Fm., increasing fine-grained sediments were observed in the paleo-Pearl River. Paleogeography map in **Fig.18** shows the faults in the south also targeted coarse-grained sediment, and the distal fine-grained sediments mixed with the proximal coarse-grained fans.

#### 2) *Depositional environment in the decelerated rifting block*

The Central NDZ shows the accretion pattern of the decelerated rifting block. During the interval of Wenchang Fm., Central NDZ is controlled by several faults in the south and north. The high-angled faults in the north triggered the development of alluvial deltas. In the Enping Fm., the second rifting process enlarged the dispersal area. Further, plain alluvial and large pro-graded deltas developed. With the rising sea level during the late Oligocene (*Haq and Schutter., 2008; Xie et al., 2019*), the reworking process became dominant, and tide- or wave-influenced delta could be observed. Then, at the end of the second rifting process (*Wang et al., 2019; Xie et al., 2019*), all the sags in the Central NDZ were filled by the distal fine sediment provided by the Pearl River.

#### 3) *Depositional environment in the accelerated rifting block*

The Eastern NDZ is a typical accelerated rifting block exhibiting spatial variation with respect to the accretion pattern. During Wenchang Fm., the separated sag and limited dispersal area lead to the

development of a small scale alluvial fan and pro-graded delta in these areas. In the Enping Fm. interval, different from the west region, the uplift and sharp fault dips caused the formation of more coarse-grained fans or braided deltas. Then, in the Zhuhai Fm., due to the uplift during the end of the second rifting stage, the sediment provided by the Pearl River mixed with the coarse fan. In addition, some carbonated platforms developed with less sediments (**Fig. 18**).

### 7.3 Infilling process insights from the S2S system

*Michael et al.*, (2013) have studied the relation between the mass balance coordinate (or mass loss), grain size distribution, and moving boundary of the coarse-grained sediment. Based on the study on the mass balance coordinate and infilling process (*Hampson et al.*, 2014), the mass balance coordinate  $\chi$  can serve as an index to evaluate the accretion pattern from upstream to downstream (**Fig.17**). Accordingly, after importing the above S2S parameters into **Equation 3**, we can generate the plot of the mass balance coordinate  $\chi$  and its corresponding infilling process (**Fig. 20**).

#### 7.3.1 Infilling process and dominant factors associated with the uniform rifting system

Western NDZ shows an infilling process of the uniform rifting system. In case of the Zhuqiong I stage tectonic movement,  $\chi(x)$  shows a linear relation between the mass balance coordinate and deposition distance.  $\chi(x)$  is 0–0.7, indicating different grain sizes (coarse-grained fan or sandy delta) distributed with a clear boundary. As the depositional environment stated above, a coarse-grained fan is developed in the proximal area, whereas the fine-grained sediment is deposited in the distal region. During the Zhuqiong II stage tectonic movement, the relation between the mass balance coordinate and deposition distance  $\chi(x)$  maintained a linear curve (**Fig. 20**).  $\chi(x)$  was 0.2–0.7, and its decline curve was observed to become gentle. More fine-grained sediments were injected into the depression because of the warm paleoclimate during the Eocene to the Oligocene (*Zachos et al.*, 2008; *Bijl et al.*, 2009). A comparison of the  $\chi(x)$  curve of the two aforementioned rifting stages shows that the infilling process is not significant during the uniform rifting process.

Based on the statistical analysis of the S2S systems (**Table 3**), the following fitting formula can be obtained (**Fig. 20**):

$$V = aA + bQ_{total} + ce^H + m, \quad (\text{Equation 4})$$

where  $V$  is the volume of the sink,  $Q$  is the sediment supply,  $A$  is the provenance area, and  $H$  is the

relative height of the pathway. The terms  $a$ ,  $b$ ,  $c$  in the equation are fitting coefficients. According to the bubble plot in **Fig. 20**, the sediment supply ( $Q_{total}$ ) and relative height ( $H$ ) can influence the volume of the S2S system in the uniform rifting system.

### 7.3.2 Infilling process and dominant factors associated with the decelerated rifting block

The Central NDZ shows the infilling process of the decelerated rifting system. In the first rifting stage (early Eocene), the accretion pattern is similar to that of Western NDZ.  $\chi(x)$  is 0.2–1.0. During the second rifting stage, the curve of  $\chi(x)$  shows an under-concave shape, indicating that more coarse-grained sediments developed in the proximal area and that fine-grained sediments were deposited in limited area. The above comparison shows two curves; more fine-grained sediments accumulated in the second stage when compared with those in the first stage.

The analysis of the sequence stratigraphy showed the decelerating rifting process that resulted in the declining accommodation area from the Eocene to the Oligocene. With the increasing fine-grained sediment provided by the paleo-Pearl River during the Oligocene, the accommodation space was infilled by the fine-grained sediment. The volcanic moment associated with the Xijiang and SDZ and tuff and volcanic clastic rocks can provide fine-grained sediment in the depression (*Sun et al., 2008; Sun et al., 2010*).

Based on a statistical analysis of the S2S systems (**Table 3**), the following fitting formula can be obtained:

$$V = bH + cA \cdot e^{Q_{total}} + m \quad (\text{Equation 5})$$

As shown in **Fig. 20**,  $e^{Q_{total}}$  is the dominant part of the S2S volume in **Equation 5**, and  $c$  and  $m$  are the fitting coefficients. Thus, the sediment supply is the key factor associated with the S2S developed in the decelerated rifting basin. Furthermore, Gawthorpe *et al.* (1994); Chen *et al.* (2019); Zhuo *et al.* (2019) found that the latter rework process, including the tidal or wavy current, reduces the impact factor of the relative height.

### 7.3.3 Infilling process and dominant factors associated with the accelerated rifting block

The Eastern NDZ is a typical accelerated rifting block. In this study, we consider Huizhou Sag as an example. During the first rifting stage,  $\chi(x)$  shows a linear relation between the mass balance coordinate and migration distance. In the second rifting stage presented in **Fig. 20**,  $\chi(x)$  is an up-

concave-shaped curve. As shown by the S2S pattern in **Fig. 19**, during this interval, coarse-grained sediment was dominant during the infilling process, and fine-grained sediment was observed to develop in a limited area.

The analysis of the insights obtained by applying the theory of sequence stratigraphy shows that the accelerating rate during the second rifting stage considerably contributes to the accommodation space. With the sharp increase in accommodation space, mass sediment must be injected into the depression area. Also, according to the paleoflow direction of the paleo-Pearl River, the accelerated rifting blocks are not in the main direction of the sediment supply, resulting in limited distal sediment supply. The HMA in **Fig. 15** also provides evidence of this phenomenon. Thus, the ratio of accommodation space and sediment supply is increasing. According to *Carroll and Bohacs (1999)*, based on the basin classification according to the balance between the sediment supply and accommodation rate, the coarse-grained mass sediment is dominant during the infilling process.

Based on a statistical analysis of the S2S systems (**Table 3**), the following fitting formula can be obtained:

$$V = bA \cdot H + c \ln(Q_{total}) + m. \quad (\text{Equation 6})$$

As shown by the balloon chart in **Fig. 20** and **Equation 6**,  $H$  is the dominant factor in the S2S system volume apart from  $Q_{total}$ .

#### 7.4 S2S system evolution in case of an episodically rifting continental margin basin

Combing previous studies (*Buck., 1991; Brune et al., 2016; Ulvrova et al., 2019*), the accelerated rifting system is characterized by a drastically increasing accommodation space. The decelerated rifting and uniform rifting systems exhibit different evolutionary processes, indicating the decreasing accommodation space in the sink area (*Nottvedt et al., 1995; Gawthorpe and Leeder, 2008*). Based on insights obtained globally, we can distinguish between episodically rifting basins such as the Victoria Land Basin, the Bohai Bay Basin, the East China Sea Basin, the Japanese Sea Basin, which mainly developed during the Cenozoic around the Pacific plate (*Cooper and Davey, 1985; Hu et al., 2001; He and Wang., 2004*), and the West Canada Basin, which developed around the North American plate (*Cooper and Davey, 1985*). We can also distinguish between the three rifting processes associated with these case studies.

*Royden and Keen (1980)* indicated that the rifting process of the decelerated rifting basins could be divided into initial and thermal phases based on a case study conducted in East Canada. As shown by the gentle slope of the depth–age curve, the decelerated rifting basin provides only limited amount of space during the second thermal stage. Thus, the sediment supply may be the dominant factor that influences the development of the S2S system. *Cochran (1983)* demonstrated that fine-grained sediments fill the basin during the second stage of the rifting process.

Based on the aforementioned observations, relative height is considered to be the dominant factor associated with the accelerated rifting process. *Ren et al. (2002)* and *Li et al. (2009)* presented an ideal case study of the East China Sea Basin, indicating a steep depth–age curve. By comparing the results of a sedimentology study conducted in the East China Sea (*Li et al., 2018; Zhang et al., 2018*) and the Huizhou Sag examined in this study, we find that the coarse-grained S2S system developed during the accelerated rifting process and that relative height is a dominant factor during sediment transportation.

## 8. Conclusions

In this study, we recovered the S2S system in the PRMB during the rifting interval and evaluated the infilling process using mass balance theory.

1) Based on the 2D seismic fault interpretation and FT inversion, we classified the episodic rifting into three systems: a uniform rifting system in Wenchang “A” Sag (Western NDZ), a decelerated rifting system in the Enping and Xijiang Sags (Central NDZ), and an accelerated rifting system in the Huizhou Sag (Eastern NDZ).

2) We evaluated the amount of sediment provided from the source area by integrating the U-Pb data, REE data and heavy mineral data associated with the provenance area. During the early Eocene, NDZ sediments were deposited in a proximal area. Upper to the late Eocene and Oligocene, we speculated that more sediments from the paleo-Pearl River were injected into the dispersion area.

3) In case of the uniform rifting system, the proximal coarse-grained fan was dominant during the first rifting stage, whereas the fine-grained sediment from the proximal area infilled the sag during the second rifting stage. In case of the decelerated rifting system, we considered the coarse-grained sediment from the proximal area transferred to the fine-grained sediment from the distal area. The infilling process of the accelerated rifting system exhibited a filling process similar those exhibited by

the two aforementioned types. During the second stage, the fine-grained sediment provided by the Pearl River and the proximal fan delta could be observed in the sag. As to the dominated factors, in the decelerated rifting basin, the sediment supply was the major factor associated with S2S development, whereas the relative height was the major factor in case of the accelerated rifting basin.

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## Figure Captions

### Fig. 1

Tectonic division of the Pearl River Mouth Basin (PRMB). PRMB can be divided into five parts: northern fault terrace zone, northern depression zone (NDZ), central uplift zone, southern depression zone (SDZ), and southern–northern fault zone. The red dot line indicates 2D seismic profiles, whereas the orange dot line shows the location of 3D profiles. B is a generalized stratigraphic column; The

Shenhu (E<sub>1s</sub>), Wenchang (E<sub>2w</sub>), Enping (E<sub>2e</sub>), Zhuhai (E<sub>3z</sub>), Zhujiang (N<sub>1z</sub>), and Haijiang (N<sub>2h</sub>) formations are presented from the bottom to the top. The sea levels based on the work conducted by *Haq and Schutter. (2008)*, and the tectonic stage is based on the study conducted by *Li and Rao, (1994)*; *Shao et al. (2018)*; and *Wang et al. (2019)*. F,m stands for formation, M.b. is the member, SBF is the seismic reflection boundary, and Tec is the tectonic stage.

### Fig. 2

Seismic profile around the PRMB. The polar stereographic projection indicates the faults in the northwest part of the basin developed in the northwest direction and those in the east part developed in the northern direction. In the SDZ, the main faults developed in the northeast direction.

### Fig. 3

Geological map of PRMB at present time(a) and the tectonic movement stage division(b) (*Li and Rao, 1994*). The age dating of the granite refer to the study of (*Wang et al., 2017*; *Wang et al., 2019*; *Suo et al., 2019*). As indicated by the profile, the Paleocene to the Eocene indicates the interval of the first rifting stage, whereas the Oligocene corresponds to the second rifting stage.

### Fig. 4

Collection of lithofacies description and grain size of the wells D, B, E, F, I, J, K, M, and Q, indicating the late Eocene to the Oligocene stratigraphic units in the PRMB. Wells D and B belong to Zhu III depression (Western NDZ). Wells E, F, I, and X are located in Zhu I Depression (Eastern and Central NDZ). Wells K, M, and Q show the strata in Zhu II depression (ZIID).

### Fig. 5

Lithofacies templates. Six types of lithofacies associations are provided on the right side and detail description in **Table.2**.

### Fig. 6

3D seismic profile of Wenchang Sag and its interpretation.

### Fig. 7

3D seismic profile of Enping Sag and its interpretation.

### Fig. 8

3D seismic profile of Huizhou Sag and its interpretation.

**Fig. 9**

a-c shows the frequency of the fission-track distribution and relation between the relative height and ZFT age value. On the right are the representative plots of the fission track. Dark gray shading indicates the better-fitting cooling paths obtained from Monte Carlo trials. Light gray shading outlines the population of “acceptable” defined by a less stringent goodness-of-fit criterion of 0.05.

**Fig. 10**

Representative zircon (CL) images. The small white circles represent the sites of U–Pb age analyses, and the measured ages are shown in Ma.

**Fig. 11**

Zircon U–Pb age spectra of the Paleocene sediments in wells C, B, E, and F. The potential source areas are the northeastern Pearl River, western Pearl River, Panyu Uplift, and Hainan island (*Liu et al., 2017; Shao et al., 2017; Wang et al., 2019*).

**Fig. 12**

Concordia plot of the detrital zircon of wells E(a), F(b), B(c), and C(d). The data influenced by the case of Pb loss and inclusion have been deleted. Only analyses with concordances of >90% are included.

**Fig. 13**

Intersection diagrams between the ratio of Th/U and the age distribution. (a) presents the data of Eocene (*Wang et al., 2019*), whereas (b) shows the data of Oligocene.

**Fig. 14**

REE distribution pattern of NDZ. The REE data are standardized with the chordate.

**Fig. 15**

Paleomorphology of NDZ during the Eocene (a) and Oligocene (b). All the well locations and their corresponding HMA are presented as a pie chart. In the left column are the HMA and ZTR index of the wells C, B, E, F, and M.

**Fig. 16**

Tectonic framework of PRMB as a 2D seismic profile and its interpretation (the profile location is in **Fig. 1**). We calculated the broken displacement associated with each profile. Wenchang Sag shows

a typical half-graben, and its fault displacement does not exhibit a drastic change. The fault displacement in the Enping and Xijiang Sags show a decreasing trend, whereas that in the Huizhou Sag increases from the Eocene to the Oligocene. Thus, we classified the rifting process into three stages: uniform, decelerated, and accelerated rifting systems.

### Fig. 17

Various S2S patterns and their corresponding infilling pattern with multiprovenance. The charts below the S2S patterns reflect the relation between the migration distance and mass balance coordinate  $\chi$ . In this study, the mass balance coordinate (mass loss)  $\chi(x)$  can be classified into three parts: dominated by a coarse-grain fan ( $\chi(x) < 0.25$ ), dominated by sandy pro-graded delta ( $0.25 < \chi(x) < 0.75$ ), and dominated by reworking sediments ( $0.75 < \chi(x) < 1.0$ ). The curve ( $\chi(x)$ ) has three patterns to show various infilling patterns: a linear relation, an under-concave shape, and a down-concave shape. According to previous research (*Paola. and Martin M., 2012; Michael et al., 2013; Hampson et al., 2014*), the different curves can quantitatively present the various infilling processes.

### Fig. 18

The pattern of evolution of the three-stage infilling process from the Eocene to the late Oligocene. A separate sag developed during the first rifting stage. The mass sediment is deposited in a proximal area. With the extension of the basin, more distal sediment was injected into the DNZ during the second rifting stage.

### Fig. 19

Facies association distribution of PRMB. The facies distribution in SDZ is based on the work conducted by *Mi et al. (2008)*. The Miocene facies association (d) is modified from *Huang and Wang (2006) and Liu et al. (2016)*.

### Fig. 20

The evolution of mass balance coordinate (mass loss)  $\chi(x)$  during the two-stage tectonic movement. From left to right are the two-stage rifting model modified from *Michael et al. (2013)*, the mass balance coordinate (mass loss)  $\chi(x)$  curve, and balloon pilots. In the two-stage rifting model, we show the three types of rifting process: (a) is the uniform rifting system, (b) is the decelerated rifting basin, and (c) is the accelerated rifting system.

## **Table Caption**

### **Table 1**

Apatite/zircon FT data of the Pearl River Mouth Basin.

### **Table 2**

Facies association descriptions.

### **Table 3**

Parameters of the S2S system. The data used in this study were statistically obtained based on the seismic information. We obtained the dip angle with a dip along the slope. The provenance area was determined as the truncation area of the seismic package. The dispersal areas were calculated according to the truncation of the seismic events.

## **Appendix Table Caption**

### **Appendix Table 1**

The detrital zircon age date in well E at a depth of 4155.5 m.

### **Appendix Table 2**

The detrital zircon age date in well F at a depth of 3917.5 m.

### **Appendix Table 3**

The detrital zircon age date in well C at a depth of 2580.1 m.

### **Appendix Table 4**

The Detrital zircon age date in well B at a depth of 2581.2 m.

Table 1

| S     | L    | in              | A                  | $\rho$         | $\rho_i$       | $\rho_d$           | F                  | D                       | D                 | T              | L $\pm$                 |                              |
|-------|------|-----------------|--------------------|----------------|----------------|--------------------|--------------------|-------------------------|-------------------|----------------|-------------------------|------------------------------|
| amp   | ith. | terval          | FT/Z               | $\rho_s (N_s)$ | $\rho_i (N_i)$ | $\rho_d (N_d)$     | $(\chi^2)$         | par/ $\mu$              | per/ $\mu$        | $\pm\Delta T/$ | $\Delta L(n)/\mu$       |                              |
| le    |      |                 | FT                 | $/(10^6c$      | $/(10^6c$      | $/(10^6c$          |                    | m                       | m                 | Ma             | m                       |                              |
| No.   |      |                 |                    | $m^{-2})$      | $m^{-2})$      | $m^{-2})$          |                    |                         |                   |                |                         |                              |
|       |      |                 |                    |                |                | 5.                 |                    |                         |                   |                |                         |                              |
| ell L | W    | G<br>ranit<br>e | J<br>urassi<br>c   | A<br>FT        | 7              | 2<br>.17(1<br>907) | 3<br>.09(2<br>710) | 720<br>( 678<br>2<br>0) | $\epsilon$<br>.95 | 1              | 7<br>6.4 $\pm$ 2.<br>3  | 11.<br>63 $\pm$ 3.0<br>1(34) |
| ell L | W    | G<br>ranit<br>e | J<br>urassi<br>c   | Z<br>FT        | 7              | 7<br>.61(2<br>615) | 2<br>.06(7<br>08)  | 0.<br>219(4<br>881)     | $\epsilon$        |                | 1<br>30.6 $\pm$<br>6.8  |                              |
| ell H | W    | D<br>iorite     | C<br>retace<br>ous | A<br>FT        |                | 1<br>4.22(<br>80)  | 1<br>9.38(<br>109) | 5.<br>720(6<br>780)     | $\epsilon$<br>.89 | 1              | 7<br>9.7 $\pm$ 1<br>1.9 | 12.<br>36 $\pm$ 1.9(<br>23)  |
| ell H | W    | D<br>iorite     | C<br>retace<br>ous | Z<br>FT        |                | 6<br>.64(3<br>32)  | 2<br>.34(1<br>17)  | 0.<br>219(4<br>881)     | 7<br>2            |                | 1<br>00.6 $\pm$<br>11.2 |                              |
| ell O | W    | D<br>iorite     | C<br>retace<br>ous | A<br>FT        | 6              | 1<br>3.48(<br>557) | 2<br>0.41(<br>842) | 5.<br>720(6<br>780)     | $\epsilon$<br>.85 | 1<br>.55       | 0<br>1.8 $\pm$ 4.<br>2  | 13.<br>16 $\pm$ 1.5<br>7     |
| ell P | W    | G<br>neis<br>s  | T<br>riassic       | A<br>FT        |                | 2<br>0.15(<br>529) | 1<br>7.33(<br>455) | 5.<br>720(6<br>708)     | $\epsilon$<br>.78 | 1<br>.5        | 0<br>25.8 $\pm$<br>8.5  |                              |
|       | W    | G<br>T          | T<br>Z             |                |                | 7                  | 2                  | 0.                      | $\epsilon$        |                | 1                       |                              |

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**TABLE 2**

| <b>Facies Association</b> | <b>Lithofacies</b>         | <b>Main sedimentary features</b>                                                                                                                                  | <b>depositional environment</b>                                                                                                |
|---------------------------|----------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------|
| A (LFA)                   | <b>Sm-Sc-<br/>Scc-Scm</b>  | Moderately sorted homogeneous sandstone in bottom and regularly lamellar crossing bedding in the top                                                              | Bidirectional traction flow deposited (Tidal environment)                                                                      |
| B (LFB)                   | <b>Sc-Gm-Sp</b>            | Planar cross-bedded gravel in the middle, and the planar crossbedding at the top                                                                                  | Braided flow traction                                                                                                          |
| C (LFC)                   | <b>Sb-Sc-Sm-<br/>Sp-Sm</b> | Coarsening upward sandstone. Mud clast and deformed structure can be distinguished in the bottom, and the coarse-grained sandstone crossbedding in the upper part | Meandering rivers setting ( <i>Maill., 1978</i> )                                                                              |
| D (LFD)                   | <b>Sc-Gp-Sd-<br/>M</b>     | Imbricate-supported gravel in the middle. The mud layer and deformation at the top                                                                                | Short-term high-density and high Froude-number traction flow ( <i>Reid and Frostick., 1987</i> ) (Short-term flooding setting) |
| E (LFE)                   | <b>Sm-M-Sb-<br/>M-Sm</b>   | Multi-layers of the moderately sorted fine-grained sediment with cross bedding and the mudstone                                                                   | Semi-deep lake setting                                                                                                         |
| F (LFF)                   | <b>M-Sd-Sb</b>             | Mass mudstone in the bottom, and fine-grained climbing-ripple laminations in the middle. Compound-graded bedding fine sand and parallel-                          | <i>Bouma (1962)</i> sequence or Deep-water setting                                                                             |

waved bedding sandstone in the

Journal Pre-proofs  
upper part.

Gravel-supported conglomerate

with regular imbedded layers. Upper

to the top, matrix-supported

conglomerate shows an imbricated

orientation

Coarse-grained

debris flow

Lithofacies

**Gp-Gm-**

G (LFG)

**(Gm)**

**TABLE 3**

| Block            | No. | pro-<br>graded<br>delta/F<br>an | F<br>m.        | Av<br>e. Dip<br>Angle | Provan<br>ce Area | Evaluati<br>on height | Sink<br>Area/km <sup>2</sup> | Pathw |                             |
|------------------|-----|---------------------------------|----------------|-----------------------|-------------------|-----------------------|------------------------------|-------|-----------------------------|
|                  |     |                                 |                |                       |                   |                       |                              | ay    | Cut<br>Area/km <sup>2</sup> |
| Wencha<br>ng Sag | D1  |                                 | E <sub>2</sub> | 2.3                   | 2009.5            | 560.21                | 829.3                        |       | 5.44                        |
|                  |     | w                               | 5              | 2                     |                   |                       | 1                            |       |                             |
|                  | D2  |                                 | E <sub>2</sub> | 2.7                   | 1882.2            | 604.80                | 1295.                        |       | 5.62                        |
|                  |     | w                               | 5              | 9                     |                   |                       | 25                           |       |                             |
|                  | D3  |                                 | E <sub>2</sub> | 2.2                   | 1789.5            | 534.73                | 1162.                        |       | 5.46                        |
|                  |     | w                               | 5              | 7                     |                   |                       | 74                           |       |                             |
|                  | D4  |                                 | E <sub>2</sub> | 4.5                   | 1970.7            | 169.47                | 565.4                        |       | 4.52                        |
|                  | w   | 5                               | 0              |                       |                   | 4                     |                              |       |                             |
|                  | D5  |                                 | E <sub>2</sub> | 2.8                   | 1798.9            | 213.36                | 580.5                        |       | 4.33                        |
|                  |     | w                               | 3              | 1                     |                   | 9                     |                              |       |                             |
|                  | D6  |                                 | E <sub>2</sub> | 1.6                   | 1729.5            | 337.05                | 953.7                        |       | 3.97                        |
|                  |     | e                               | 2              | 3                     |                   | 8                     |                              |       |                             |
|                  | D7  |                                 | E <sub>2</sub> | 1.9                   | 1884.9            | 397.02                | 580.6                        |       | 3.26                        |

|           |       |     |        |        |  |       |       |
|-----------|-------|-----|--------|--------|--|-------|-------|
|           | e     | 2   | 4      |        |  | 2     |       |
|           | $E_2$ | 1.9 | 2002.1 |        |  | 569.5 |       |
| <b>D8</b> |       |     |        | 238.61 |  |       | 3.52  |
|           | e     | 2   | 3      |        |  | 8     |       |
|           | $E_3$ | 0.8 | 1787.8 |        |  | 530.5 |       |
| <b>D9</b> |       |     |        | 233.96 |  |       | 3.08  |
|           | z     | 8   | 6      |        |  | 3     |       |
|           | $E_3$ | 0.8 | 1768.6 |        |  | 215.8 |       |
| <b>D1</b> |       |     |        | 155.97 |  |       | 3.47  |
| <b>0</b>  | z     | 8   | 1      |        |  | 8     |       |
|           | $E_3$ | 0.2 | 2006.0 |        |  | 1042. |       |
| <b>D1</b> |       |     |        | 137.06 |  |       | 3.10  |
| <b>1</b>  | z     | 1   | 3      |        |  | 86    |       |
|           | $E_2$ | 5.5 | 1370.6 |        |  | 499.8 |       |
| <b>D1</b> |       |     |        | 633.16 |  |       | 12.56 |
|           | w     | 2   | 9      |        |  | 1     |       |
|           | $E_2$ | 0.9 | 1419.4 |        |  | 363.4 |       |
| <b>D2</b> |       |     |        | 88.67  |  |       | 3.17  |
|           | w     | 2   | 1      |        |  | 1     |       |
|           | $E_2$ | 2.1 | 1619.3 |        |  | 441.1 |       |
| <b>D3</b> |       |     |        | 107.24 |  |       | 7.72  |
|           | w     | 1   | 8      |        |  | 2     |       |
|           | $E_2$ | 1.9 | 1110.4 |        |  | 446.6 |       |
| <b>D4</b> |       |     |        | 123.51 |  |       | 4.06  |
|           | w     | 2   | 2      |        |  | 2     |       |
|           | $E_2$ | 0.8 |        |        |  | 565.9 |       |
| <b>D5</b> |       |     | 934.56 | 159.15 |  |       | 3.38  |
|           | e     | 2   |        |        |  | 0     |       |
|           | $E_2$ | 0.8 |        |        |  | 637.9 |       |
| <b>D6</b> |       |     | 984.13 | 149.51 |  |       | 3.77  |
|           | e     | 3   |        |        |  | 3     |       |
|           | $E_2$ | 0.7 | 2046.2 |        |  | 576.2 |       |
| <b>D7</b> |       |     |        | 132.51 |  |       | 4.05  |
|           | e     | 9   | 3      |        |  | 8     |       |
|           | $E_3$ | 0.7 | 2337.2 |        |  | 747.8 |       |
| <b>D8</b> |       |     |        | 122.15 |  |       | 3.29  |
|           | z     | 3   | 6      |        |  | 2     |       |
|           | $E_3$ | 0.6 | 2769.4 |        |  | 850.2 |       |
| <b>D9</b> |       |     |        | 126.77 |  |       | 3.81  |
|           | z     | 8   | 7      |        |  | 9     |       |
|           | $E_3$ | 0.5 | 3557.1 |        |  | 814.0 |       |
| <b>D1</b> |       |     |        | 138.32 |  |       | 4.43  |

**Enping  
Sag**

|                | 0         | z     | 8   | 4 |        | 7      |       |
|----------------|-----------|-------|-----|---|--------|--------|-------|
|                |           | $E_2$ | 2.0 |   | 934.56 | 313.36 | 455.0 |
| <b>D1</b>      | w         | 2     |     |   |        |        | 9.61  |
|                |           | $E_2$ | 2.5 |   | 984.13 | 337.05 | 410.1 |
| <b>D2</b>      | w         | 5     |     |   |        |        | 8.98  |
|                |           | $E_2$ | 2.8 |   | 934.56 | 397.02 | 403.3 |
| <b>D3</b>      | w         | 6     |     |   |        |        | 8.53  |
|                |           | $E_2$ | 2.8 |   | 984.13 | 313.36 | 525.7 |
| <b>D4</b>      | w         | 6     |     |   |        |        | 7.93  |
|                |           | $E_2$ | 3.1 |   | 934.56 | 337.05 | 710.1 |
| <b>D5</b>      | w         | 1     |     |   |        |        | 7.75  |
| <b>Huizhou</b> |           | $E_2$ | 2.8 |   | 1110.4 |        | 686.4 |
| <b>Sag</b>     | <b>D6</b> | e     | 4   | 2 |        | 397.02 | 7.93  |
|                |           | $E_2$ | 2.9 |   | 1619.3 |        | 677.4 |
| <b>D7</b>      | e         | 1     | 8   |   |        | 213.36 | 9.34  |
|                |           | $E_2$ | 2.5 |   | 2337.2 |        | 756.8 |
| <b>D8</b>      | e         | 4     | 6   |   |        | 337.05 | 8.03  |
|                |           | $E_2$ | 2.8 |   | 2769.4 |        | 621.5 |
| <b>D9</b>      | e         | 9     | 7   |   |        | 397.02 | 9.67  |
|                |           | $E_3$ | 2.6 |   | 3557.1 |        | 784.2 |
| <b>0</b>       | <b>D1</b> | z     | 8   | 4 |        | 413.36 | 9.65  |
|                |           | $E_3$ | 2.8 |   | 3557.1 |        | 784.3 |
| <b>1</b>       | <b>D1</b> | z     | 5   | 4 |        | 413.36 | 8.41  |

**Appendix Table1 The Detrital zircon age date in Well E at the dePbh of 4155.5m**

Journal Pre-proofs

|         | $U^{235}$ | $U^{235}$ | $U^{238}$ | $U^{238}$ | Rho ( $Pb^{207}/U^{235}$ VS $Pb^{206}/U^{238}$ ) |
|---------|-----------|-----------|-----------|-----------|--------------------------------------------------|
| Well E- |           |           |           |           |                                                  |
| 1       | 165.7     | 5.7       | 160.3     | 2.4       | 0.19574                                          |
| Well E- |           |           |           |           |                                                  |
| 2       | 168.5     | 3.9       | 165.1     | 2         | 0.29057                                          |
| Well E- |           |           |           |           |                                                  |
| 3       | 166       | 11        | 165.3     | 2.7       | 0.013669                                         |
| Well E- |           |           |           |           |                                                  |
| 4       | 175.9     | 5.2       | 162.9     | 2.7       | 0.096242                                         |
| Well E- |           |           |           |           |                                                  |
| 5       | 171.6     | 4.5       | 167.7     | 2.2       | -0.08418                                         |
| Well E- |           |           |           |           |                                                  |
| 6       | 282       | 5.5       | 209.9     | 2         | 0.3539                                           |
| Well E- |           |           |           |           |                                                  |
| 7       | 179.6     | 4.6       | 156.8     | 1.9       | 0.30152                                          |
| Well E- |           |           |           |           |                                                  |
| 8       | 174.1     | 3.3       | 149.8     | 1.4       | 0.25652                                          |
| Well E- |           |           |           |           |                                                  |
| 9       | 168       | 4         | 164.1     | 1.7       | 0.15752                                          |
| Well E- |           |           |           |           |                                                  |
| 10      | 212.9     | 3.8       | 206.8     | 1.9       | 0.31966                                          |
| Well E- |           |           |           |           |                                                  |
| 11      | 195       | 14        | 119.7     | 3.6       | 0.51888                                          |
| Well E- |           |           |           |           |                                                  |
| 12      | 148.4     | 6.6       | 153.6     | 2.1       | 0.14649                                          |

|         |       |     |       |     |           |
|---------|-------|-----|-------|-----|-----------|
| Well E- |       |     |       |     |           |
| 13      | 400   | 11  | 429.7 | 4.3 | 0.20967   |
| Well E- |       |     |       |     |           |
| 14      | 164.1 | 9.3 | 164.8 | 2.5 | 0.18944   |
| Well E- |       |     |       |     |           |
| 15      | 151   | 12  | 145   | 3.4 | -0.046765 |
| Well E- |       |     |       |     |           |
| 16      | 997   | 20  | 1002  | 15  | 0.27452   |
| Well E- |       |     |       |     |           |
| 17      | 155.3 | 4.3 | 151.5 | 1.8 | 0.31334   |
| Well E- |       |     |       |     |           |
| 18      | 170.2 | 4.2 | 157.9 | 1.7 | 0.27419   |
| Well E- |       |     |       |     |           |
| 19      | 152.3 | 4.7 | 149   | 1.7 | 0.0048404 |
| Well E- |       |     |       |     |           |
| 20      | 156.4 | 3.4 | 152.8 | 1.4 | 0.20135   |
| Well E- |       |     |       |     |           |
| 21      | 435.9 | 8   | 434.3 | 4.9 | 0.30965   |
| Well E- |       |     |       |     |           |
| 22      | 430   | 11  | 436.8 | 4.8 | 0.33766   |
| Well E- |       |     |       |     |           |
| 23      | 156.8 | 5.2 | 160.2 | 2   | 0.10962   |
| Well E- |       |     |       |     |           |
| 24      | 603   | 27  | 194   | 3   | 0.80949   |
| Well E- |       |     |       |     |           |
| 25      | 163.2 | 8.8 | 159.2 | 2.3 | 0.026785  |
| Well E- |       |     |       |     |           |
| 26      | 172   | 6.9 | 164   | 2.1 | 0.2745    |

|         |       |     |       |     |             |
|---------|-------|-----|-------|-----|-------------|
| Well E- |       |     |       |     |             |
| 27      | 163.2 | 4.1 | 162.3 | 1.9 | 0.26816     |
| Well E- |       |     |       |     |             |
| 28      | 169   | 6.1 | 163.4 | 2.5 | 0.11848     |
| Well E- |       |     |       |     |             |
| 29      | 2452  | 16  | 2499  | 24  | 0.46806     |
| Well E- |       |     |       |     |             |
| 30      | 216.3 | 5.6 | 163.3 | 1.6 | -0.00014542 |
| Well E- |       |     |       |     |             |
| 31      | 448   | 13  | 458.6 | 5.2 | -0.078676   |
| Well E- | 3354. |     |       |     |             |
| 32      | 1     | 10  | 3191  | 20  | 0.74904     |
| Well E- |       |     |       |     |             |
| 33      | 166.1 | 4.4 | 167.1 | 2   | 0.16262     |
| Well E- |       |     |       |     |             |
| 34      | 774.1 | 9.2 | 681.6 | 6.8 | 0.41531     |
| Well E- |       |     |       |     |             |
| 35      | 158.9 | 5.3 | 150.8 | 1.7 | -0.018948   |
| Well E- |       |     |       |     |             |
| 36      | 153.9 | 4.5 | 151.2 | 1.7 | 0.22939     |
| Well E- |       |     |       |     |             |
| 37      | 167.6 | 9.8 | 153.3 | 3.5 | 0.34635     |
| Well E- |       |     |       |     |             |
| 38      | 162   | 6.2 | 154.1 | 2.1 | 0.13535     |
| Well E- |       |     |       |     |             |
| 39      | 163.2 | 4.9 | 164.4 | 1.9 | 0.28495     |
| Well E- |       |     |       |     |             |
| 40      | 372   | 28  | 126.3 | 2.3 | 0.80089     |

|         |       |     |       |     |          |
|---------|-------|-----|-------|-----|----------|
| Well E- |       |     |       |     |          |
| 41      | 159.5 | 4.5 | 150.7 | 1.7 | 0.22056  |
| Well E- |       |     |       |     |          |
| 42      | 788   | 14  | 784.5 | 8.1 | 0.018967 |
| Well E- |       |     |       |     |          |
| 43      | 544   | 11  | 428.5 | 4.3 | 0.085874 |
| Well E- |       |     |       |     |          |
| 44      | 183.3 | 5.1 | 162.9 | 1.7 | 0.15961  |
| Well E- |       |     |       |     |          |
| 45      | 432.2 | 9.5 | 433.7 | 5   | 0.12316  |
| Well E- |       |     |       |     |          |
| 46      | 152.6 | 5.6 | 157.6 | 1.9 | 0.12058  |
| Well E- |       |     |       |     |          |
| 47      | 195.3 | 5.8 | 157.1 | 2   | 0.28496  |
| Well E- |       |     |       |     |          |
| 48      | 149.8 | 5.7 | 146.5 | 2.2 | 0.12956  |
| Well E- |       |     |       |     |          |
| 49      | 274   | 11  | 160.3 | 1.9 | 0.46903  |
| Well E- |       |     |       |     |          |
| 50      | 650   | 11  | 616.1 | 7.8 | 0.40343  |
| Well E- |       |     |       |     |          |
| 51      | 2722  | 25  | 2677  | 35  | 0.82474  |
| Well E- |       |     |       |     |          |
| 52      | 156   | 3.8 | 153.9 | 1.7 | 0.30122  |
| Well E- |       |     |       |     |          |
| 53      | 1072  | 12  | 976.3 | 9.8 | 0.45734  |
| Well E- |       |     |       |     |          |
| 54      | 233.8 | 7.2 | 196.2 | 5   | 0.43533  |

|         |       |     |       |     |           |
|---------|-------|-----|-------|-----|-----------|
| Well E- |       |     |       |     |           |
| 55      | 219   | 12  | 155   | 5   | 0.038475  |
| Well E- |       |     |       |     |           |
| 56      | 189.2 | 5.6 | 151.5 | 1.8 | 0.23473   |
| Well E- |       |     |       |     |           |
| 57      | 165.7 | 7.7 | 154   | 2.9 | 0.0098553 |
| Well E- |       |     |       |     |           |
| 58      | 171.8 | 9.2 | 151.7 | 2.4 | 0.18594   |
| Well E- |       |     |       |     |           |
| 59      | 151.5 | 5.6 | 152.4 | 2.2 | 0.28114   |
| Well E- |       |     |       |     |           |
| 60      | 195.6 | 5.6 | 152.9 | 1.7 | 0.2323    |
| Well E- |       |     |       |     |           |
| 61      | 389.6 | 9.7 | 170.6 | 2.2 | 0.42791   |
| Well E- |       |     |       |     |           |
| 62      | 246.4 | 5.8 | 154.2 | 1.7 | 0.26066   |
| Well E- |       |     |       |     |           |
| 63      | 152.2 | 3.6 | 147.2 | 1.8 | 0.43509   |
| Well E- |       |     |       |     |           |
| 64      | 175.9 | 5   | 133.7 | 1.6 | 0.38403   |
| Well E- |       |     |       |     |           |
| 65      | 204.7 | 5.3 | 163.5 | 1.6 | 0.20468   |
| Well E- |       |     |       |     |           |
| 66      | 210.2 | 7.1 | 155.1 | 2.1 | -0.23976  |
| Well E- |       |     |       |     |           |
| 67      | 167   | 4.6 | 161.4 | 2   | 0.16369   |
| Well E- |       |     |       |     |           |
| 68      | 160   | 16  | 149.8 | 5.8 | 0.16491   |

|         |       |     |       |     |          |
|---------|-------|-----|-------|-----|----------|
| Well E- |       |     |       |     |          |
| 69      | 155.8 | 5.8 | 149.7 | 1.7 | 0.2817   |
| Well E- |       |     |       |     |          |
| 70      | 171   | 14  | 153.3 | 3   | 0.28974  |
| Well E- |       |     |       |     |          |
| 71      | 229.2 | 8.4 | 150.1 | 1.8 | 0.1906   |
| Well E- |       |     |       |     |          |
| 72      | 167.3 | 7.6 | 160.2 | 2.1 | 0.024542 |
| Well E- |       |     |       |     |          |
| 73      | 168.1 | 4.7 | 165.3 | 2.3 | 0.22936  |
| Well E- |       |     |       |     |          |
| 75      | 157.9 | 4.6 | 148.7 | 1.6 | 0.21955  |
| Well E- |       |     |       |     |          |
| 76      | 444   | 37  | 147.8 | 3   | 0.83587  |
| Well E- |       |     |       |     |          |
| 77      | 165.9 | 5.9 | 165.2 | 2.1 | 0.20289  |
| Well E- |       |     |       |     |          |
| 78      | 169.4 | 5.3 | 169.5 | 2.2 | 0.22138  |

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**Appendix Table2 The Detrital zircon age date in Well F at the dePbh of 3917.5m**

Journal Pre-proofs

|         | $U^{235}$ | $U^{235}$ | $U^{238}$ | $U^{238}$ | Rho ( $Pb^{207}/U^{235}$ VS $Pb^{206}/U^{238}$ ) |
|---------|-----------|-----------|-----------|-----------|--------------------------------------------------|
| Well F- |           |           |           |           |                                                  |
| 1       | 136.1     | 6.7       | 134.1     | 1.8       | -0.029002                                        |
| Well F- |           |           |           |           |                                                  |
| 2       | 1880      | 12        | 1901      | 14        | 0.47298                                          |
| Well F- |           |           |           |           |                                                  |
| 3       | 444       | 10        | 452.5     | 5.4       | 0.15649                                          |
| Well F- | 2424.     |           |           |           |                                                  |
| 4       | 7         | 12        | 2360      | 21        | 0.59456                                          |
| Well F- |           |           |           |           |                                                  |
| 5       | 2749      | 13        | 2714      | 22        | 0.65017                                          |
| Well F- | 2626.     |           |           |           |                                                  |
| 6       | 9         | 12        | 2601      | 23        | 0.66477                                          |
| Well F- |           |           |           |           |                                                  |
| 7       | 139.4     | 6.1       | 140       | 2         | -0.041381                                        |
| Well F- |           |           |           |           |                                                  |
| 8       | 156.8     | 6         | 158       | 1.9       | -0.040785                                        |
| Well F- |           |           |           |           |                                                  |
| 9       | 118.3     | 3.7       | 117.3     | 1.3       | 0.17285                                          |
| Well F- |           |           |           |           |                                                  |
| 10      | 1438      | 15        | 1446      | 13        | 0.29409                                          |
| Well F- |           |           |           |           |                                                  |
| 11      | 165       | 6.2       | 159.8     | 1.9       | 0.090403                                         |
| Well F- |           |           |           |           |                                                  |
| 12      | 961       | 12        | 964.5     | 9.9       | 0.34396                                          |

|         |        |     |       |     |          |
|---------|--------|-----|-------|-----|----------|
| Well F- |        |     |       |     |          |
| 13      | 775    | 17  | 780.8 | 9.8 | 0.097811 |
| Well F- |        |     |       |     |          |
| 14      | 1087   | 16  | 1099  | 11  | 0.16551  |
| Well F- |        |     |       |     |          |
| 15      | 131.5  | 6.8 | 135.2 | 1.9 | -0.10939 |
| Well F- |        |     |       |     |          |
| 16      | 1055   | 19  | 1060  | 11  | 0.17088  |
| Well F- |        |     |       |     |          |
| 17      | 438.4  | 9.3 | 432.3 | 5   | 0.24424  |
| Well F- |        |     |       |     |          |
| 18      | 151    | 5.6 | 158.1 | 2   | 0.077932 |
| Well F- |        |     |       |     |          |
| 19      | 974    | 12  | 983.4 | 8.9 | 0.37888  |
| Well F- |        |     |       |     |          |
| 20      | 768    | 17  | 783.4 | 9.7 | 0.20129  |
| Well F- |        |     |       |     |          |
| 21      | 106    | 20  | 102.7 | 4.5 | 0.053367 |
| Well F- |        |     |       |     |          |
| 22      | 514    | 13  | 511   | 5.9 | 0.17424  |
| Well F- |        |     |       |     |          |
| 23      | 2114.3 | 12  | 2086  | 16  | 0.50425  |
| Well F- |        |     |       |     |          |
| 24      | 430.7  | 10  | 442.1 | 4.2 | 0.07075  |
| Well F- |        |     |       |     |          |
| 25      | 258.2  | 7.5 | 247.2 | 2.8 | 0.18683  |
| Well F- |        |     |       |     |          |
| 26      | 2091   | 15  | 2110  | 20  | 0.51858  |

|         |       |     |       |     |           |
|---------|-------|-----|-------|-----|-----------|
| Well F- |       |     |       |     |           |
| 27      | 890.1 | 9.0 | 901.5 | 7.4 | 0.43050   |
| Well F- |       |     |       |     |           |
| 28      | 421   | 15  | 433.5 | 4.9 | 0.18115   |
| Well F- |       |     |       |     |           |
| 29      | 233.7 | 7.6 | 234.4 | 2.8 | 0.25301   |
| Well F- |       |     |       |     |           |
| 30      | 338   | 13  | 327.9 | 4   | 0.055294  |
| Well F- |       |     |       |     |           |
| 31      | 244.7 | 7.6 | 248.4 | 2.5 | 0.079539  |
| Well F- |       |     |       |     |           |
| 32      | 2472  | 14  | 2413  | 21  | 0.46501   |
| Well F- |       |     |       |     |           |
| 33      | 107.2 | 5.3 | 99.1  | 1.4 | 0.054909  |
| Well F- |       |     |       |     |           |
| 34      | 143.9 | 6.8 | 140.5 | 2.2 | 0.14204   |
| Well F- |       |     |       |     |           |
| 35      | 422   | 11  | 428.1 | 4.2 | 0.17184   |
| Well F- |       |     |       |     |           |
| 36      | 219   | 11  | 227.1 | 3   | 0.072977  |
| Well F- |       |     |       |     |           |
| 37      | 93.4  | 5.3 | 96.8  | 1.4 | -0.020744 |
| Well F- |       |     |       |     |           |
| 38      | 939   | 14  | 925.7 | 9.6 | 0.18859   |
| Well F- |       |     |       |     |           |
| 39      | 435.6 | 8.6 | 433.1 | 4.2 | 0.13007   |
| Well F- |       |     |       |     |           |
| 40      | 106   | 6.6 | 111.1 | 1.9 | 0.050421  |

|         |       |     |       |     |           |
|---------|-------|-----|-------|-----|-----------|
| Well F- |       |     |       |     |           |
| 41      | 434   | 11  | 434.7 | 3.1 | 0.10902   |
| Well F- |       |     |       |     |           |
| 42      | 943   | 25  | 942   | 12  | 0.045344  |
| Well F- |       |     |       |     |           |
| 43      | 2046  | 14  | 1838  | 18  | 0.60328   |
| Well F- |       |     |       |     |           |
| 44      | 2399  | 22  | 2333  | 24  | 0.38295   |
| Well F- |       |     |       |     |           |
| 45      | 441.6 | 9   | 438.5 | 4.6 | 0.28933   |
| Well F- |       |     |       |     |           |
| 46      | 150.2 | 6.7 | 146.3 | 1.8 | 0.090626  |
| Well F- |       |     |       |     |           |
| 47      | 444.3 | 9.5 | 436.4 | 4.5 | 0.27234   |
| Well F- |       |     |       |     |           |
| 48      | 1977  | 13  | 1967  | 15  | 0.4805    |
| Well F- |       |     |       |     |           |
| 49      | 1856  | 10  | 1849  | 14  | 0.57819   |
| Well F- |       |     |       |     |           |
| 50      | 166.4 | 6.9 | 166.9 | 2.2 | 0.004421  |
| Well F- | 1329. |     | 1268. |     |           |
| 51      | 3     | 9.4 | 3     | 8.5 | 0.46091   |
| Well F- |       |     |       |     |           |
| 52      | 137.4 | 7.3 | 139.1 | 2.1 | -0.009018 |
| Well F- |       |     |       |     |           |
| 53      | 986   | 11  | 967.4 | 7.6 | 0.28445   |
| Well F- |       |     |       |     |           |
| 54      | 800   | 16  | 784.9 | 7.3 | 0.25501   |

|         |       |     |       |     |            |
|---------|-------|-----|-------|-----|------------|
| Well F- |       |     |       |     |            |
| 55      | 302.0 | 9.5 | 302.0 | 4.2 | 0.19743    |
| Well F- |       |     |       |     |            |
| 56      | 439   | 12  | 444.8 | 5.1 | 0.21985    |
| Well F- |       |     |       |     |            |
| 57      | 698.2 | 7.5 | 704.4 | 6.2 | 0.40134    |
| Well F- |       |     |       |     |            |
| 58      | 144.5 | 8.6 | 145.9 | 2.6 | 0.073232   |
| Well F- |       |     |       |     |            |
| 59      | 155.2 | 6   | 157.5 | 2.1 | 0.078864   |
| Well F- |       |     |       |     |            |
| 60      | 156.2 | 10  | 159   | 2.4 | -0.0049717 |
| Well F- |       |     |       |     |            |
| 61      | 1461  | 13  | 1413  | 15  | 0.70695    |
| Well F- |       |     |       |     |            |
| 62      | 115.7 | 5.3 | 111.7 | 1.5 | 0.083661   |
| Well F- |       |     |       |     |            |
| 63      | 237.6 | 8   | 235.1 | 3   | 0.17525    |
| Well F- |       |     |       |     |            |
| 64      | 85.4  | 4.4 | 84.2  | 1.3 | 0.13501    |
| Well F- |       |     |       |     |            |
| 65      | 94.2  | 3.8 | 96.9  | 1.3 | 0.1212     |
| Well F- |       |     |       |     |            |
| 66      | 118.9 | 5.2 | 117   | 1.6 | 0.10087    |
| Well F- |       |     |       |     |            |
| 67      | 927   | 12  | 936   | 8.8 | 0.32514    |
| Well F- |       |     |       |     |            |
| 68      | 1632  | 13  | 1612  | 15  | 0.23777    |

|         |       |     |       |     |          |
|---------|-------|-----|-------|-----|----------|
| Well F- |       |     |       |     |          |
| 69      | 804   | 15  | 801.0 | 9.2 | 0.42019  |
| Well F- |       |     |       |     |          |
| 70      | 260   | 16  | 256   | 4.5 | 0.24832  |
| Well F- |       |     |       |     |          |
| 71      | 704   | 12  | 712.4 | 7   | 0.22154  |
| Well F- |       |     |       |     |          |
| 72      | 778   | 20  | 774   | 9.5 | 0.15619  |
| Well F- |       |     |       |     |          |
| 73      | 815   | 22  | 819.1 | 9.4 | 0.063996 |
| Well F- |       |     |       |     |          |
| 74      | 270   | 11  | 264   | 4.8 | 0.29728  |
| Well F- |       |     |       |     |          |
| 75      | 462.2 | 8.8 | 462.9 | 4.4 | 0.2684   |
| Well F- |       |     |       |     |          |
| 76      | 2455  | 12  | 2421  | 17  | 0.44087  |
| Well F- |       |     |       |     |          |
| 77      | 164   | 16  | 145.8 | 4.7 | 0.34718  |
| Well F- |       |     |       |     |          |
| 78      | 30.5  | 2   | 31.54 | 0.5 | 0.1033   |
| Well F- |       |     |       |     |          |
| 79      | 938   | 22  | 928   | 12  | 0.10857  |
| Well F- |       |     |       |     |          |
| 80      | 2456  | 15  | 2454  | 21  | 0.3745   |
| Well F- |       |     |       |     |          |
| 81      | 283   | 11  | 285.8 | 3.5 | 0.11729  |
| Well F- |       |     |       |     |          |
| 82      | 278   | 12  | 282.8 | 3.6 | 0.041945 |

Well F-

|    |     |     |       |   |         |
|----|-----|-----|-------|---|---------|
| 83 | 904 | 9.0 | 972.9 | 0 | 0.41009 |
|----|-----|-----|-------|---|---------|

Well F-

|    |     |    |       |     |         |
|----|-----|----|-------|-----|---------|
| 84 | 721 | 12 | 714.2 | 6.3 | 0.39427 |
|----|-----|----|-------|-----|---------|

Well F-

|    |     |    |       |     |          |
|----|-----|----|-------|-----|----------|
| 85 | 444 | 18 | 452.2 | 6.2 | 0.082263 |
|----|-----|----|-------|-----|----------|

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Journal Pre-proofs

**Appendix Table3 The Detrital zircon age date in Well C at the dePbh of 2580.1m**

Journal Pre-proofs

|      | $U^{235}$ | $U^{235}$ ) | $U^{238}$ | $U^{238}$ ) | Rho ( $Pb^{207}/U^{235}VS$<br>$Pb^{206}/U^{238}$ ) |
|------|-----------|-------------|-----------|-------------|----------------------------------------------------|
| Well |           |             |           |             |                                                    |
| C-1  | 152.7     | 6.8         | 151.7     | 2.2         | 0.10412                                            |
| Well |           |             |           |             |                                                    |
| C-2  | 217       | 12          | 144.9     | 2.1         | 0.26575                                            |
| Well |           |             |           |             |                                                    |
| C-3  | 150.7     | 7.4         | 150.9     | 2.5         | 0.25865                                            |
| Well |           |             |           |             |                                                    |
| C-4  | 165       | 13          | 143.6     | 3.4         | 0.14849                                            |
| Well |           |             |           |             |                                                    |
| C-5  | 158.5     | 8.3         | 153.3     | 2.6         | 0.004028                                           |
| Well |           |             |           |             |                                                    |
| C-6  | 145.6     | 5.3         | 151.5     | 2.2         | 0.10029                                            |
| Well |           |             |           |             |                                                    |
| C-7  | 164.3     | 7.1         | 152.5     | 2.2         | 0.16166                                            |
| Well |           |             |           |             |                                                    |
| C-8  | 155.7     | 7.3         | 154.3     | 2.7         | 0.084617                                           |
| Well |           |             |           |             |                                                    |
| C-9  | 148.1     | 10          | 155.2     | 2.8         | 0.11854                                            |
| Well |           |             |           |             |                                                    |
| C-10 | 154.1     | 4.3         | 152.7     | 1.9         | 0.16494                                            |
| Well |           |             |           |             |                                                    |
| C-11 | 165       | 10          | 152.4     | 3.8         | 0.3283                                             |
| Well |           |             |           |             |                                                    |
| C-12 | 185.4     | 7.8         | 148.9     | 2.3         | 0.27263                                            |

|      |       |     |       |     |          |
|------|-------|-----|-------|-----|----------|
| Well |       |     |       |     |          |
| C-13 | 154.8 | 7.7 | 151.2 | 2.9 | 0.2393   |
| Well |       |     |       |     |          |
| C-14 | 158.1 | 5.6 | 151.6 | 2.1 | 0.41119  |
| Well |       |     |       |     |          |
| C-15 | 156.9 | 3.7 | 148.1 | 1.8 | 0.34509  |
| Well |       |     |       |     |          |
| C-16 | 1051  | 17  | 1052  | 18  | 0.63805  |
| Well |       |     |       |     |          |
| C-17 | 155.5 | 7   | 154.2 | 2.3 | 0.14186  |
| Well |       |     |       |     |          |
| C-18 | 179   | 13  | 153   | 4.1 | 0.14686  |
| Well |       |     |       |     |          |
| C-19 | 809   | 26  | 211   | 3.7 | 0.7308   |
| Well |       |     |       |     |          |
| C-20 | 146.8 | 4.7 | 150.9 | 1.9 | 0.24862  |
| Well |       |     |       |     |          |
| C-21 | 159.5 | 7.3 | 150.6 | 3   | 0.17871  |
| Well |       |     |       |     |          |
| C-22 | 158.3 | 5.2 | 157.5 | 2.2 | 0.14064  |
| Well |       |     |       |     |          |
| C-23 | 262.9 | 6.7 | 256.6 | 3.1 | 0.12386  |
| Well |       |     |       |     |          |
| C-24 | 133.5 | 3.5 | 100.6 | 2.1 | 0.61182  |
| Well |       |     |       |     |          |
| C-25 | 158.5 | 4.4 | 153.2 | 2.1 | 0.19748  |
| Well |       |     |       |     |          |
| C-26 | 152.8 | 7.2 | 151.5 | 2.2 | 0.027579 |

|      |       |     |       |     |           |
|------|-------|-----|-------|-----|-----------|
| Well |       |     |       |     |           |
| C-27 | 159   | 5.7 | 155.7 | 2.4 | 0.21222   |
| Well |       |     |       |     |           |
| C-28 | 158.1 | 4.6 | 151.5 | 1.8 | 0.20468   |
| Well |       |     |       |     |           |
| C-29 | 150.3 | 5.2 | 153.6 | 2.1 | 0.11189   |
| Well |       |     |       |     |           |
| C-30 | 152.9 | 5.4 | 155.3 | 2   | 0.18985   |
| Well |       |     |       |     |           |
| C-31 | 152.4 | 6.5 | 155.3 | 2.3 | -0.028276 |
| Well |       |     |       |     |           |
| C-32 | 160.5 | 8.4 | 154.8 | 2.2 | 0.20486   |
| Well |       |     |       |     |           |
| C-33 | 146.1 | 6.8 | 155.2 | 2.2 | 0.055897  |
| Well |       |     |       |     |           |
| C-34 | 163   | 6.1 | 154.7 | 2.4 | 0.13231   |
| Well |       |     |       |     |           |
| C-35 | 292   | 17  | 281.7 | 5.8 | 0.16108   |
| Well |       |     |       |     |           |
| C-36 | 337   | 13  | 159.7 | 2.6 | 0.13301   |
| Well |       |     |       |     |           |
| C-37 | 114.9 | 4.2 | 114.7 | 1.6 | 0.22461   |
| Well |       |     |       |     |           |
| C-38 | 156   | 11  | 158.4 | 2.9 | 0.018326  |
| Well |       |     |       |     |           |
| C-39 | 154.9 | 6.1 | 154.1 | 2.1 | 0.10318   |
| Well |       |     |       |     |           |
| C-40 | 157.2 | 5.9 | 154.9 | 2.1 | 0.12826   |

|      |       |     |       |     |           |
|------|-------|-----|-------|-----|-----------|
| Well |       |     |       |     |           |
| C-41 | 492.4 | 11  | 490   | 5.7 | 0.38409   |
| Well |       |     |       |     |           |
| C-42 | 156.1 | 5.3 | 155.8 | 2.1 | 0.1871    |
| Well |       |     |       |     |           |
| C-43 | 165.2 | 4.6 | 153   | 1.9 | 0.35908   |
| Well |       |     |       |     |           |
| C-44 | 164.3 | 5.9 | 152.9 | 2.1 | 0.23104   |
| Well |       |     |       |     |           |
| C-45 | 485.1 | 9.2 | 495.1 | 5.6 | 0.35531   |
| Well |       |     |       |     |           |
| C-46 | 158.2 | 6.9 | 158.3 | 2.3 | 0.060993  |
| Well |       |     |       |     |           |
| C-47 | 159.8 | 5   | 158.4 | 2.3 | 0.15823   |
| Well |       |     |       |     |           |
| C-48 | 154   | 6.7 | 157.6 | 2.4 | -0.071891 |
| Well |       |     |       |     |           |
| C-49 | 456.8 | 7.9 | 456.2 | 4.9 | 0.3462    |
| Well |       |     |       |     |           |
| C-50 | 168.5 | 7   | 160.6 | 3.6 | 0.30921   |
| Well |       |     |       |     |           |
| C-51 | 161   | 4   | 156   | 1.9 | 0.22201   |
| Well |       |     |       |     |           |
| C-52 | 170.5 | 6.9 | 155.7 | 2.4 | 0.16501   |
| Well |       |     |       |     |           |
| C-53 | 273   | 7.3 | 264.3 | 3.2 | 0.11396   |
| Well |       |     |       |     |           |
| C-54 | 161.9 | 5.7 | 160.2 | 2.1 | 0.12102   |

|      |       |     |       |     |           |
|------|-------|-----|-------|-----|-----------|
| Well |       |     |       |     |           |
| C-55 | 227   | 11  | 150   | 2.5 | 0.19009   |
| Well |       |     |       |     |           |
| C-56 | 155.4 | 7.1 | 150.9 | 2.4 | 0.046622  |
| Well |       |     |       |     |           |
| C-57 | 285   | 14  | 268.1 | 7.8 | 0.27921   |
| Well |       |     |       |     |           |
| C-58 | 189.9 | 6.9 | 157.1 | 2   | 0.13141   |
| Well |       |     |       |     |           |
| C-59 | 633   | 19  | 183   | 2.6 | 0.3727    |
| Well |       |     |       |     |           |
| C-60 | 149.3 | 7.7 | 157.1 | 2.5 | -0.078435 |
| Well |       |     |       |     |           |
| C-61 | 158.7 | 7.3 | 154.3 | 2.6 | -0.042675 |
| Well |       |     |       |     |           |
| C-62 | 153.2 | 6.6 | 152.7 | 2.1 | -0.045565 |
| Well |       |     |       |     |           |
| C-63 | 156.4 | 4.5 | 154.2 | 2   | 0.24869   |
| Well |       |     |       |     |           |
| C-64 | 156   | 6.4 | 155.1 | 2.2 | 0.15118   |
| Well |       |     |       |     |           |
| C-65 | 111.2 | 5.4 | 111.7 | 2.3 | 0.15172   |
| Well |       |     |       |     |           |
| C-66 | 153.2 | 4.4 | 152.1 | 2   | 0.17424   |
| Well |       |     |       |     |           |
| C-67 | 153   | 4.4 | 152.1 | 1.9 | 0.24534   |
| Well |       |     |       |     |           |
| C-68 | 161   | 15  | 153.5 | 5.2 | 0.5589    |

|      |       |     |       |     |           |
|------|-------|-----|-------|-----|-----------|
| Well |       |     |       |     |           |
| C-69 | 110.4 | 4.1 | 111.4 | 1.7 | 0.19932   |
| Well |       |     |       |     |           |
| C-70 | 173.4 | 5.6 | 150.2 | 2   | 0.304     |
| Well |       |     |       |     |           |
| C-71 | 154.1 | 7.3 | 150.7 | 2.5 | 0.096665  |
| Well |       |     |       |     |           |
| C-72 | 160.1 | 5.1 | 151.1 | 2.4 | 0.089637  |
| Well |       |     |       |     |           |
| C-73 | 154.4 | 4.7 | 156.9 | 1.9 | 0.17726   |
| Well |       |     |       |     |           |
| C-74 | 120.8 | 5.3 | 111.4 | 1.9 | 0.1055    |
| Well |       |     |       |     |           |
| C-75 | 144   | 8.5 | 155.7 | 2.6 | 0.10633   |
| Well |       |     |       |     |           |
| C-76 | 153.1 | 5.1 | 148.5 | 2   | -0.035399 |
| Well |       |     |       |     |           |
| C-77 | 147.1 | 5.2 | 138.4 | 2   | 0.33871   |
| Well |       |     |       |     |           |
| C-78 | 246   | 19  | 106.2 | 3.7 | 0.69298   |
| Well |       |     |       |     |           |
| C-79 | 149.3 | 6.7 | 156.4 | 2.4 | 0.024926  |
| Well |       |     |       |     |           |
| C-80 | 154.4 | 6.3 | 154.3 | 2.3 | 0.17582   |
| Well |       |     |       |     |           |
| C-81 | 146.3 | 7.2 | 149.6 | 2.3 | 0.10577   |
| Well | 1239. |     |       |     |           |
| C-82 | 8     | 14  | 1233  | 14  | 0.24855   |

|      |       |     |       |     |          |
|------|-------|-----|-------|-----|----------|
| Well |       |     |       |     |          |
| C-83 | 565.2 | 9.0 | 590.7 | 0.5 | 0.51235  |
| Well | 1089. |     |       |     |          |
| C-84 | 8     | 13  | 1082  | 13  | 0.47024  |
| Well |       |     |       |     |          |
| C-85 | 171.2 | 7.5 | 156.3 | 2.5 | 0.14269  |
| Well |       |     |       |     |          |
| C-86 | 234.1 | 5   | 221.9 | 2.8 | 0.38338  |
| Well |       |     |       |     |          |
| C-87 | 144.6 | 8.5 | 154.2 | 2.6 | 0.11286  |
| Well |       |     |       |     |          |
| C-88 | 163.6 | 7.7 | 159.2 | 2.5 | 0.070388 |
| Well |       |     |       |     |          |
| C-89 | 151   | 6.1 | 150.5 | 2.2 | 0.12064  |
| Well |       |     |       |     |          |
| C-90 | 156.5 | 5.8 | 155.5 | 2.1 | 0.10844  |

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**Appendix Table4 The Detrital zircon age date in Well B at a dePbh of 2581.1m**

Journal Pre-proofs

|         | $U^{235}$ | $2\sigma(U^{235})$ | $U^{238}$ | $2\sigma(U^{238})$ | Rho ( $Pb^{207}/U^{235}VS$<br>$Pb^{206}/U^{238}$ ) |
|---------|-----------|--------------------|-----------|--------------------|----------------------------------------------------|
| Well B- |           |                    |           |                    |                                                    |
| 1       | 256.8     | 5.5                | 257       | 3                  | 0.31433                                            |
| Well B- |           |                    |           |                    |                                                    |
| 2       | 514       | 15                 | 517.2     | 6.7                | 0.26838                                            |
| Well B- |           |                    |           |                    |                                                    |
| 3       | 160.1     | 6.5                | 154.7     | 2.1                | 0.088934                                           |
| Well B- |           |                    |           |                    |                                                    |
| 4       | 120.4     | 7.7                | 118.1     | 2.1                | 0.041076                                           |
| Well B- |           |                    |           |                    |                                                    |
| 5       | 154.3     | 9.6                | 154.8     | 2.7                | 0.068807                                           |
| Well B- |           |                    |           |                    |                                                    |
| 6       | 151.1     | 5.5                | 152.7     | 1.8                | 0.21063                                            |
| Well B- |           |                    |           |                    |                                                    |
| 7       | 152       | 6.7                | 152.6     | 2.3                | 0.028421                                           |
| Well B- |           |                    |           |                    |                                                    |
| 8       | 147.2     | 3.3                | 146.8     | 1.9                | 0.41794                                            |
| Well B- |           |                    |           |                    |                                                    |
| 9       | 113.7     | 4.4                | 112.2     | 1.5                | 0.16471                                            |
| Well B- |           |                    |           |                    |                                                    |
| 10      | 126.4     | 8.6                | 129.8     | 2.4                | 0.044932                                           |
| Well B- |           |                    |           |                    |                                                    |
| 11      | 157.3     | 4.5                | 153.9     | 1.8                | 0.18988                                            |
| Well B- |           |                    |           |                    |                                                    |
| 12      | 154.6     | 8.4                | 149.4     | 2.4                | 0.010026                                           |

|         |       |     |       |     |           |
|---------|-------|-----|-------|-----|-----------|
| Well B- |       |     |       |     |           |
| 13      | 153.4 | 6.6 | 150   | 2.2 | -0.044433 |
| Well B- |       |     |       |     |           |
| 14      | 155.5 | 6.6 | 157.1 | 2.4 | 0.0011161 |
| Well B- |       |     |       |     |           |
| 15      | 160.8 | 6.2 | 154.6 | 2.1 | 0.14127   |
| Well B- |       |     |       |     |           |
| 16      | 165.4 | 5.5 | 163.6 | 2.6 | 0.18778   |
| Well B- |       |     |       |     |           |
| 17      | 156.7 | 4.3 | 153.8 | 2   | 0.22712   |
| Well B- |       |     |       |     |           |
| 18      | 150.1 | 6.5 | 154.2 | 2.2 | 0.091504  |
| Well B- |       |     |       |     |           |
| 19      | 158.6 | 6.8 | 153.3 | 2.2 | 0.085955  |
| Well B- |       |     |       |     |           |
| 20      | 152.9 | 4.1 | 150.6 | 2   | 0.30177   |
| Well B- |       |     |       |     |           |
| 21      | 156.6 | 6.3 | 156.9 | 2.3 | 0.028828  |
| Well B- |       |     |       |     |           |
| 22      | 158.4 | 7.6 | 160.5 | 2.7 | 0.19981   |
| Well B- |       |     |       |     |           |
| 23      | 164.5 | 9.4 | 158.9 | 2.5 | 0.091353  |
| Well B- |       |     |       |     |           |
| 24      | 123.1 | 9.3 | 119.7 | 2.3 | -0.018192 |
| Well B- |       |     |       |     |           |
| 25      | 161.4 | 5.6 | 157.9 | 2   | 0.056426  |
| Well B- |       |     |       |     |           |
| 26      | 155.9 | 4.9 | 154   | 2   | 0.023727  |

|         |       |     |       |     |           |
|---------|-------|-----|-------|-----|-----------|
| Well B- |       |     |       |     |           |
| 27      | 104.1 | 0.7 | 104.2 | 2   | -0.033010 |
| Well B- |       |     |       |     |           |
| 28      | 165.8 | 5.2 | 159.3 | 1.9 | 0.13786   |
| Well B- |       |     |       |     |           |
| 29      | 121.9 | 9.1 | 122.1 | 2.4 | 0.14114   |
| Well B- |       |     |       |     |           |
| 30      | 121   | 10  | 125.5 | 2.3 | 0.11655   |
| Well B- |       |     |       |     |           |
| 31      | 162.2 | 6.4 | 155.2 | 2.3 | 0.049175  |
| Well B- |       |     |       |     |           |
| 32      | 159.9 | 8.7 | 160.2 | 2.4 | 0.18671   |
| Well B- |       |     |       |     |           |
| 33      | 166.3 | 3.9 | 157.1 | 1.7 | 0.34102   |
| Well B- |       |     |       |     |           |
| 34      | 153.7 | 4.4 | 152.6 | 1.8 | 0.23184   |
| Well B- |       |     |       |     |           |
| 35      | 163.8 | 5.5 | 162   | 2   | 0.051079  |
| Well B- |       |     |       |     |           |
| 36      | 156.5 | 4.6 | 156.4 | 1.8 | -0.036668 |
| Well B- |       |     |       |     |           |
| 37      | 314   | 11  | 256.6 | 3.7 | 0.17362   |
| Well B- |       |     |       |     |           |
| 38      | 161   | 6.8 | 155.1 | 2   | -0.021977 |
| Well B- |       |     |       |     |           |
| 39      | 159.6 | 8   | 161.3 | 2.4 | 0.16092   |
| Well B- |       |     |       |     |           |
| 40      | 148.2 | 5.9 | 155   | 2   | -0.027001 |

|         |       |     |       |     |            |
|---------|-------|-----|-------|-----|------------|
| Well B- |       |     |       |     |            |
| 41      | 127.8 | 7.2 | 120.7 | 2.3 | 0.1168     |
| Well B- |       |     |       |     |            |
| 42      | 157.5 | 8.3 | 154.5 | 2.2 | -0.0032929 |
| Well B- |       |     |       |     |            |
| 43      | 155   | 10  | 119.1 | 2.2 | 0.0064158  |
| Well B- |       |     |       |     |            |
| 44      | 146.3 | 7.4 | 151.9 | 2.4 | 0.18071    |
| Well B- |       |     |       |     |            |
| 45      | 179.4 | 5.5 | 176.1 | 2   | 0.2199     |
| Well B- |       |     |       |     |            |
| 46      | 160.6 | 6.7 | 152.9 | 1.9 | 0.041994   |
| Well B- |       |     |       |     |            |
| 47      | 130.1 | 5.2 | 128.7 | 1.5 | 0.09287    |
| Well B- |       |     |       |     |            |
| 48      | 116.2 | 8.1 | 119.9 | 2.1 | 0.030523   |
| Well B- |       |     |       |     |            |
| 49      | 153.4 | 8   | 154   | 2.4 | 0.21461    |
| Well B- |       |     |       |     |            |
| 50      | 152   | 6.6 | 152.2 | 2.1 | 0.028025   |
| Well B- |       |     |       |     |            |
| 51      | 123.7 | 9.7 | 119.1 | 2.7 | 0.018176   |
| Well B- |       |     |       |     |            |
| 52      | 151.4 | 4.9 | 152.5 | 2   | 0.1739     |
| Well B- |       |     |       |     |            |
| 53      | 150   | 4.3 | 148.7 | 1.7 | 0.16887    |
| Well B- |       |     |       |     |            |
| 54      | 155.5 | 5.8 | 155.2 | 2.6 | 0.094782   |

|         |       |     |       |     |           |
|---------|-------|-----|-------|-----|-----------|
| Well B- |       |     |       |     |           |
| 55      | 155.5 | 6.1 | 152.4 | 2.0 | 0.10404   |
| Well B- |       |     |       |     |           |
| 56      | 123.6 | 6.7 | 123.9 | 2.3 | -0.099418 |
| Well B- |       |     |       |     |           |
| 57      | 162.2 | 6.2 | 161.3 | 2.5 | 0.27309   |
| Well B- |       |     |       |     |           |
| 58      | 148.4 | 3.6 | 150.3 | 2.1 | 0.26268   |
| Well B- |       |     |       |     |           |
| 59      | 154.6 | 6.9 | 158.5 | 2.8 | 0.20458   |
| Well B- |       |     |       |     |           |
| 60      | 113.5 | 5.3 | 113   | 1.9 | 0.14798   |
| Well B- |       |     |       |     |           |
| 61      | 233.9 | 9.3 | 238   | 3.8 | 0.28797   |
| Well B- |       |     |       |     |           |
| 62      | 158.8 | 4.7 | 154   | 2.2 | 0.20432   |
| Well B- |       |     |       |     |           |
| 63      | 166.6 | 7.9 | 156.8 | 3.1 | 0.14802   |
| Well B- |       |     |       |     |           |
| 64      | 156.7 | 6.4 | 152.6 | 2.4 | 0.14015   |
| Well B- |       |     |       |     |           |
| 65      | 113.5 | 4.9 | 113.3 | 1.9 | 0.12314   |
| Well B- |       |     |       |     |           |
| 66      | 159.6 | 7   | 155.1 | 2.5 | 0.21887   |

---

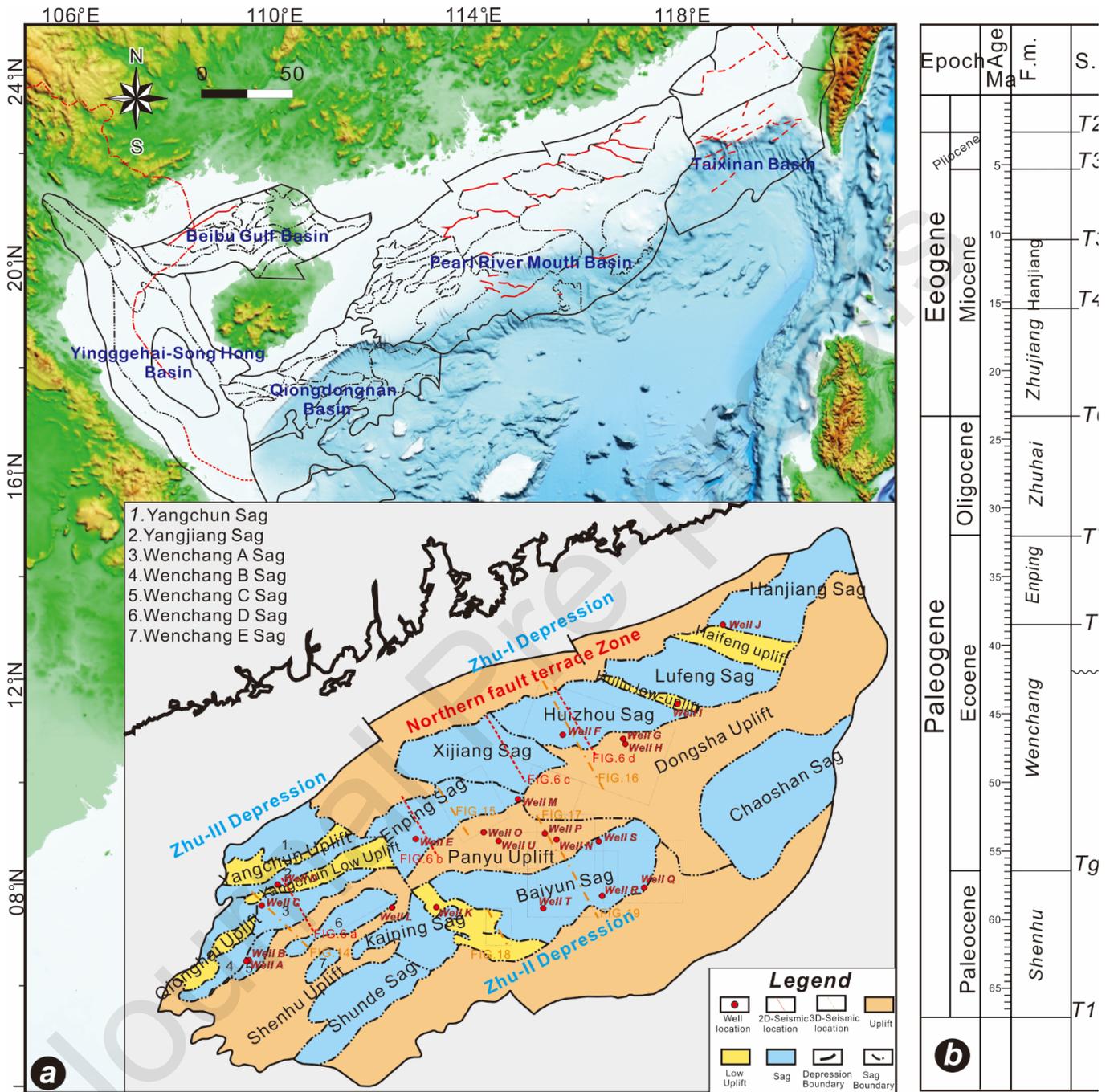
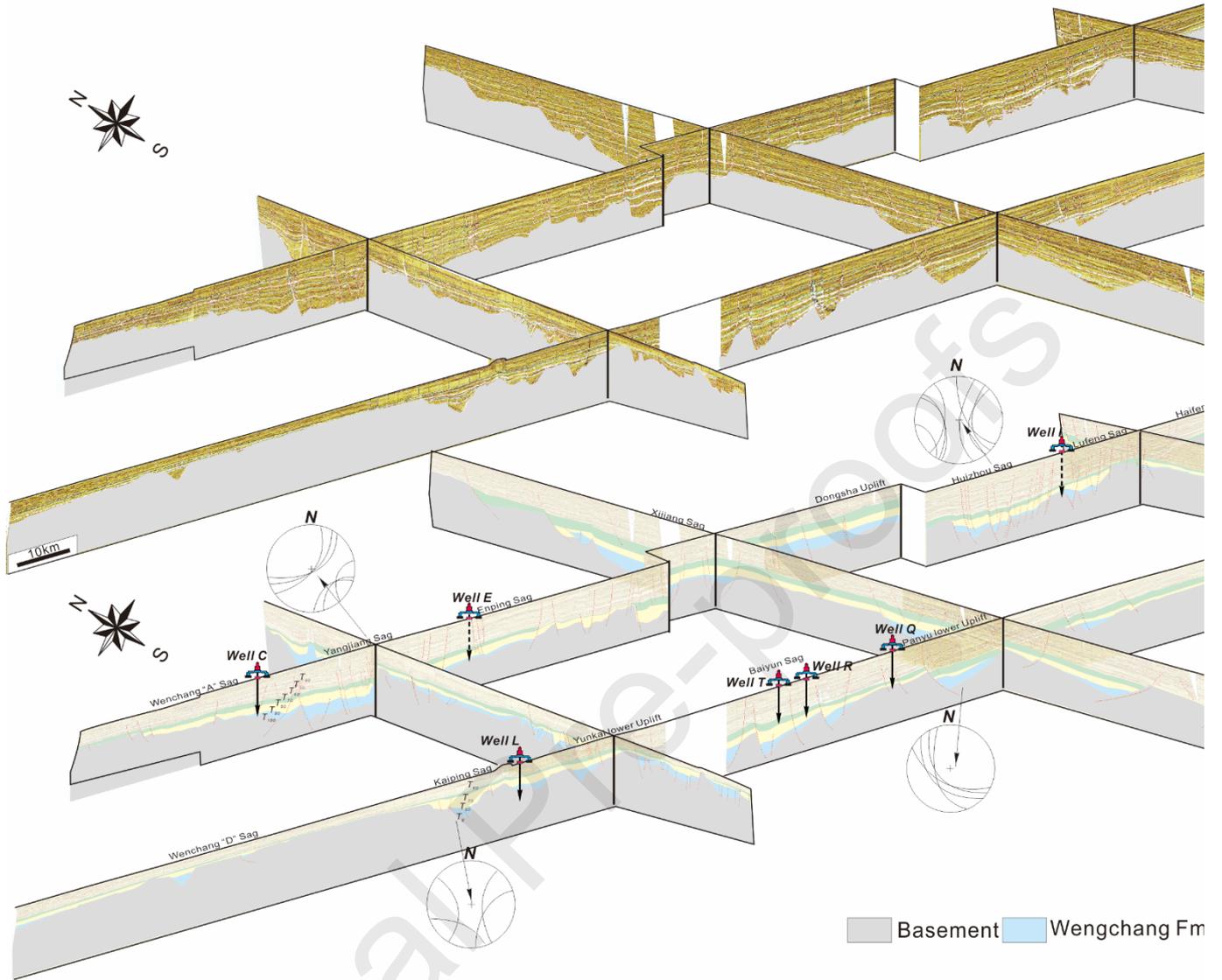


FIG 1



**FIG 2**

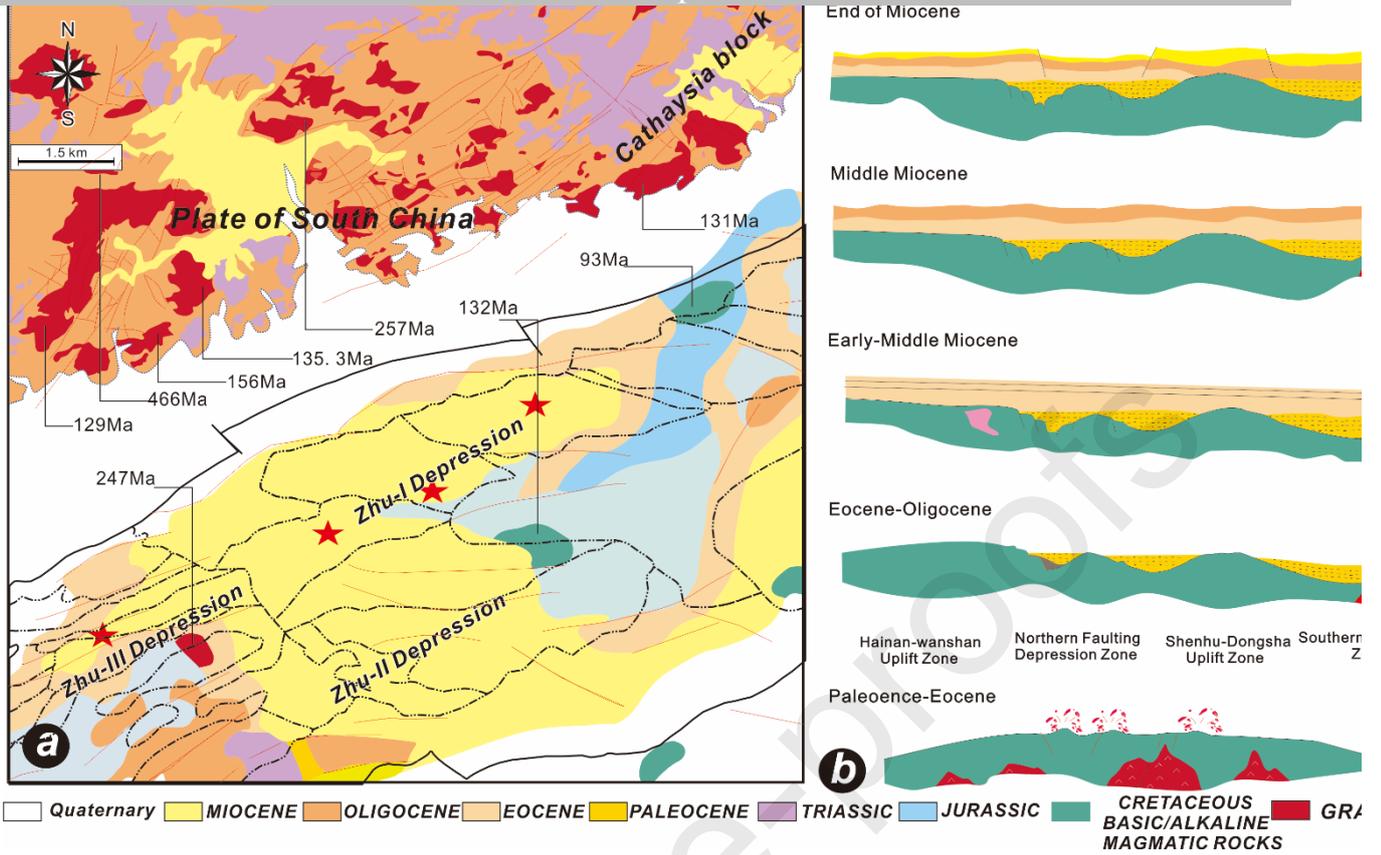
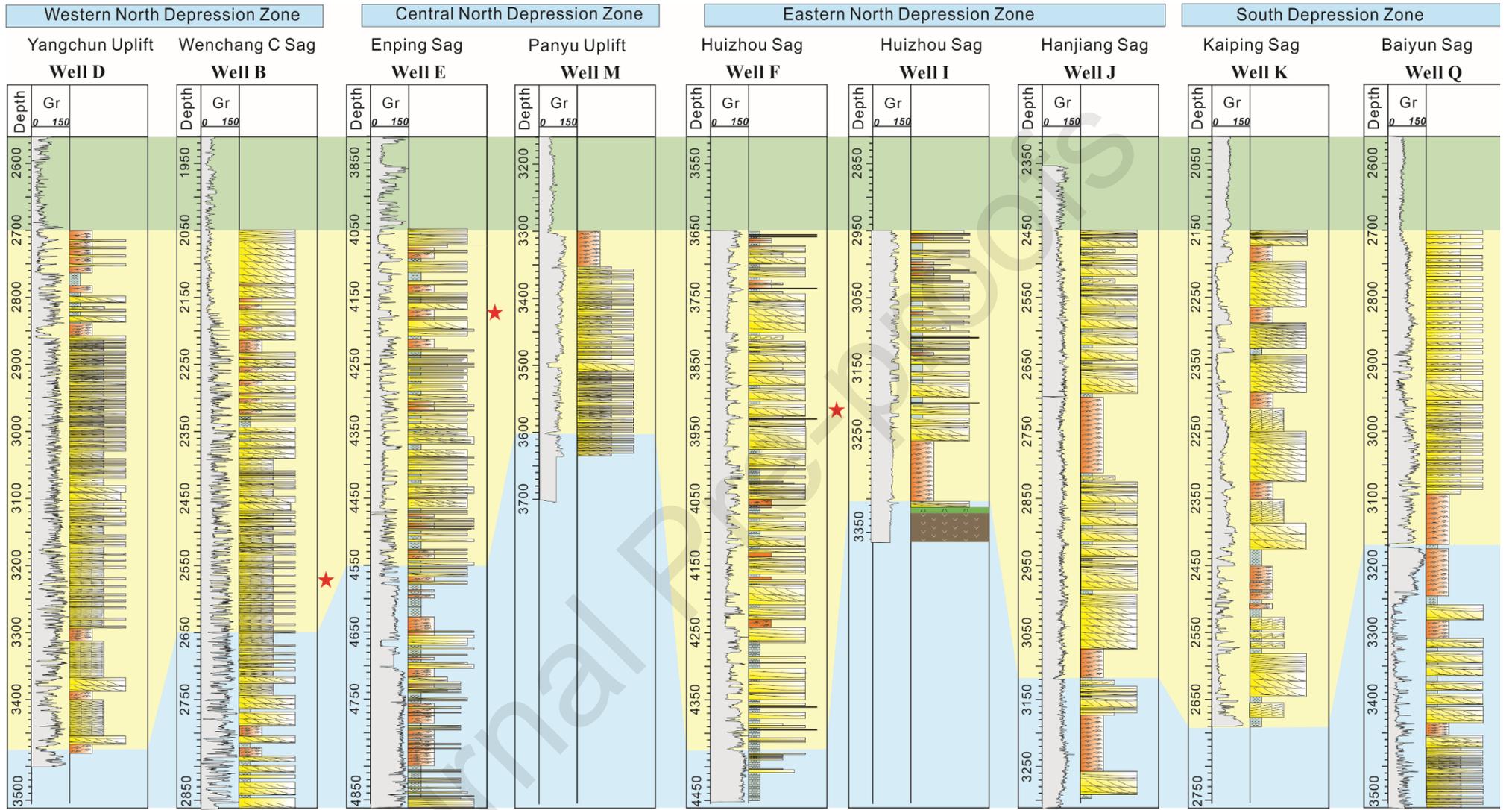


FIG 3



★ Detrital Zircon D

FIG 4

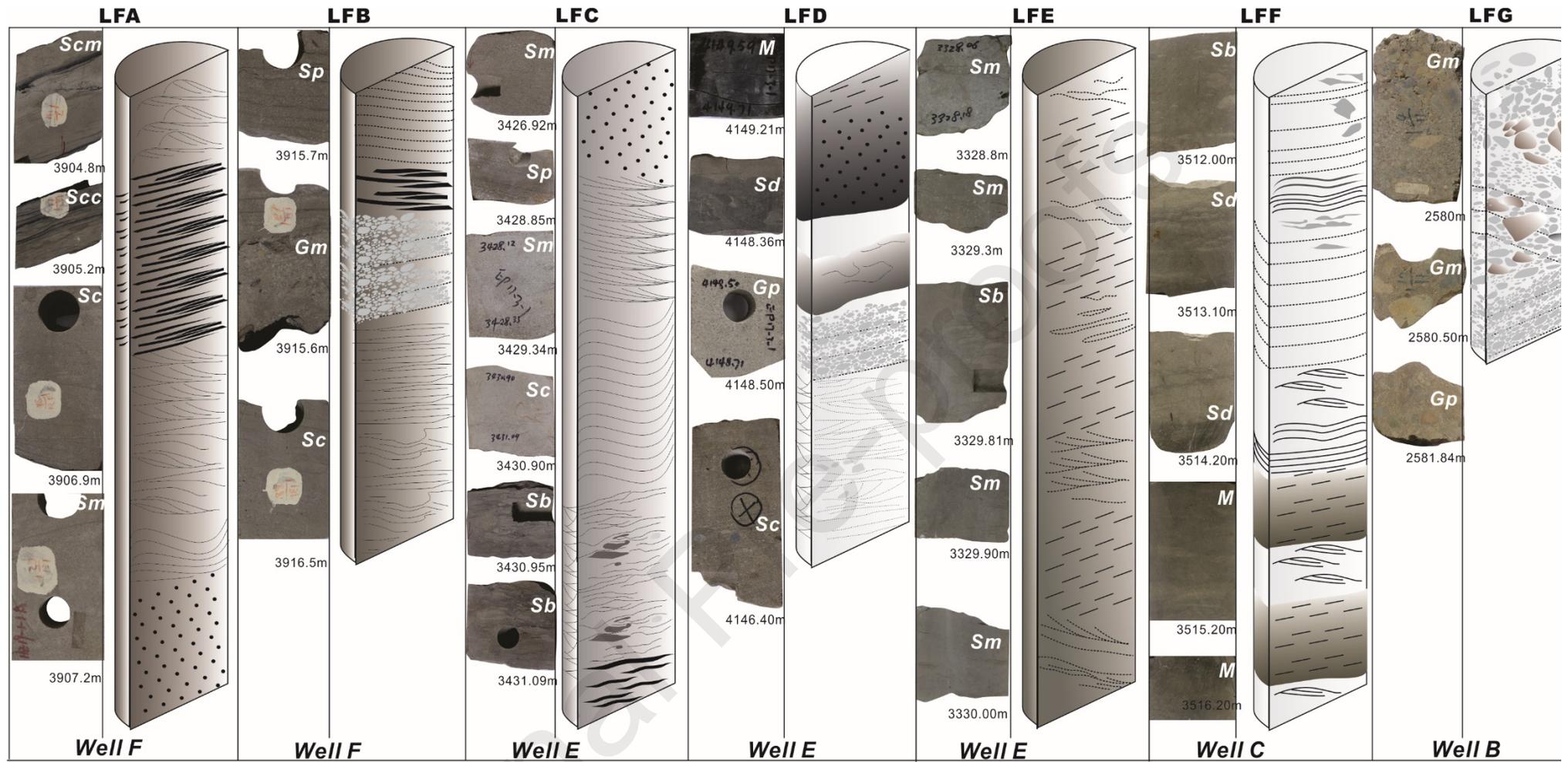


FIG 5

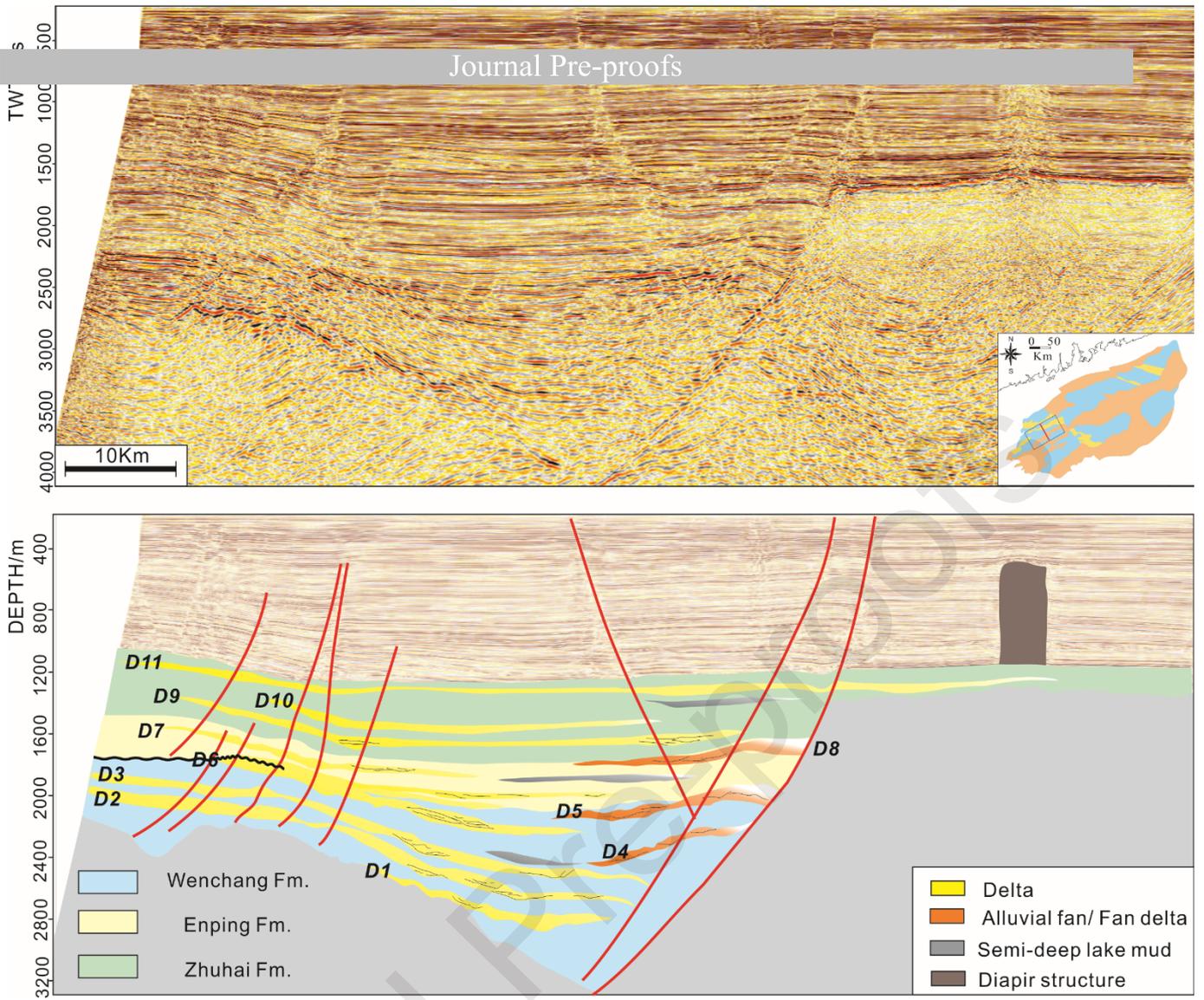
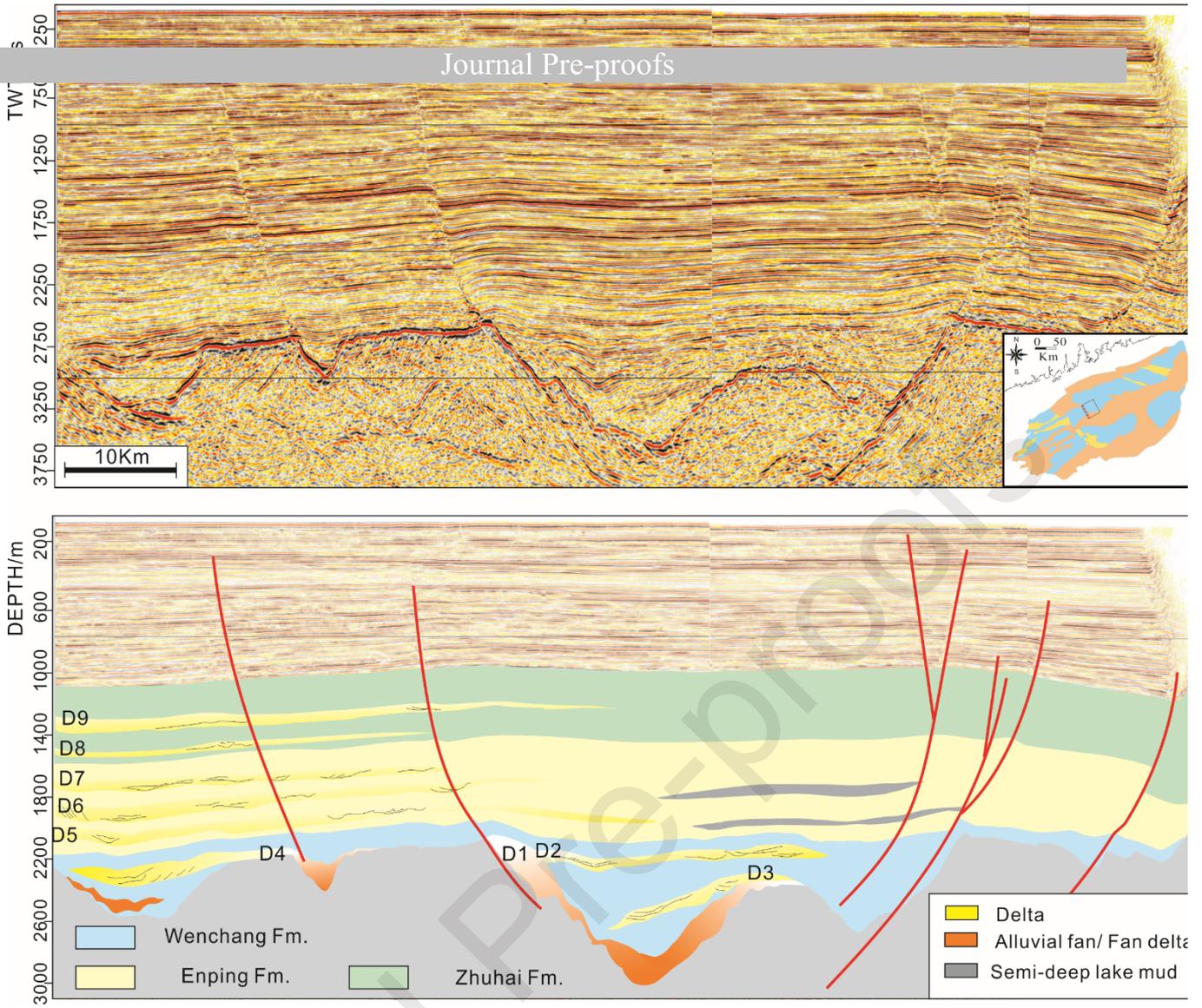
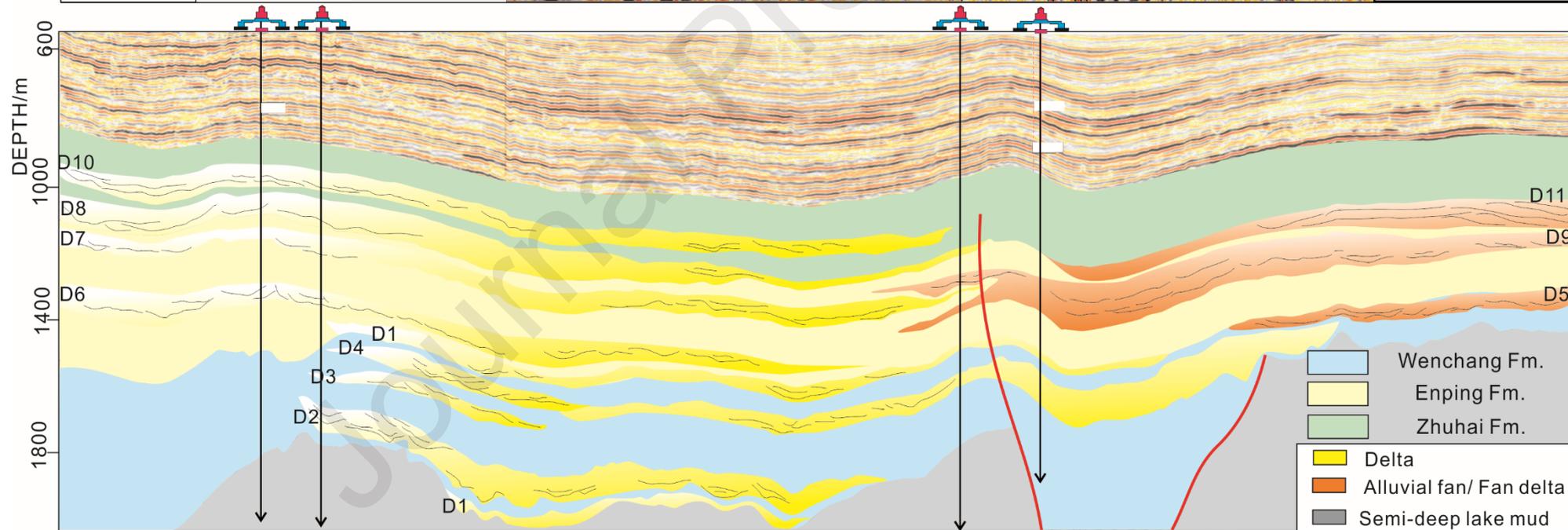
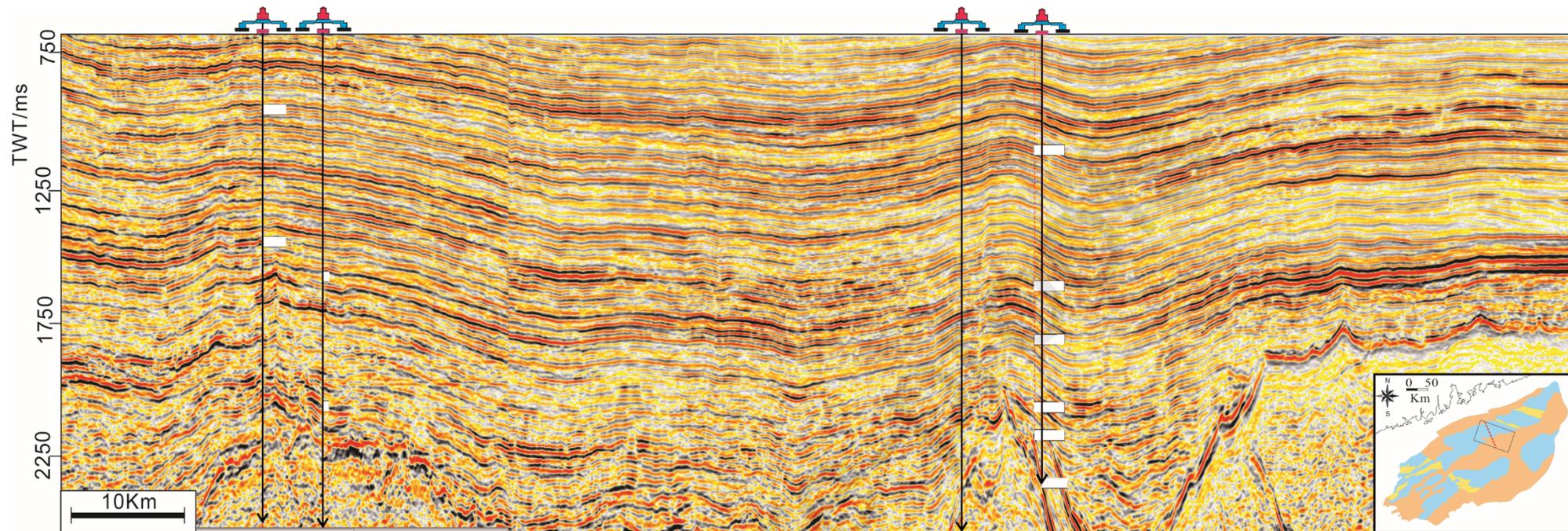


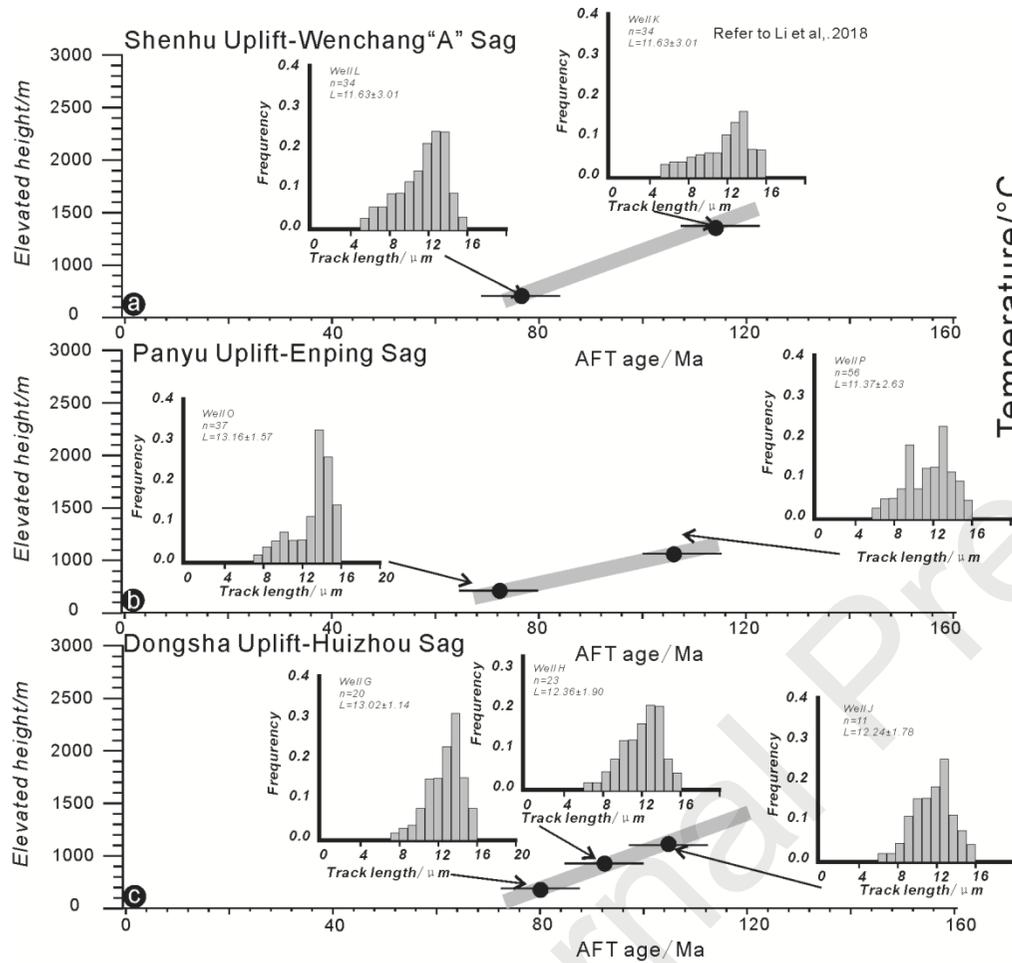
FIG 6



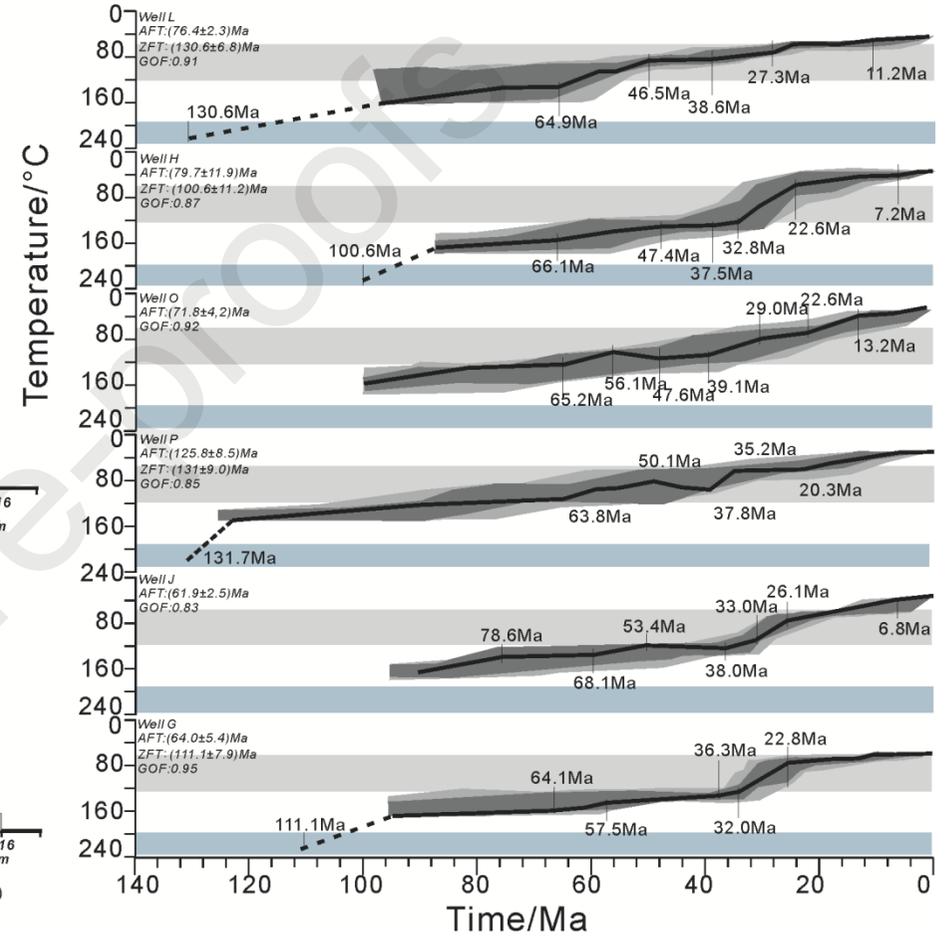
**FIG 7**

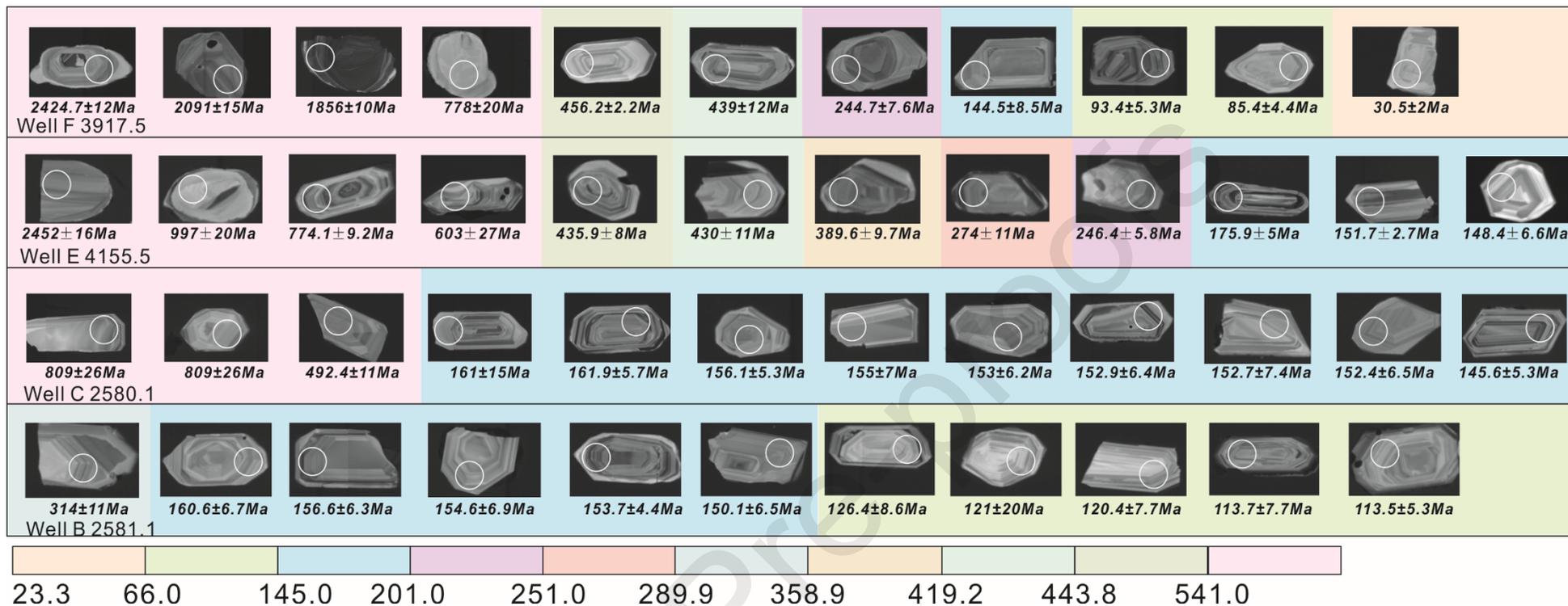


**FIG 8**

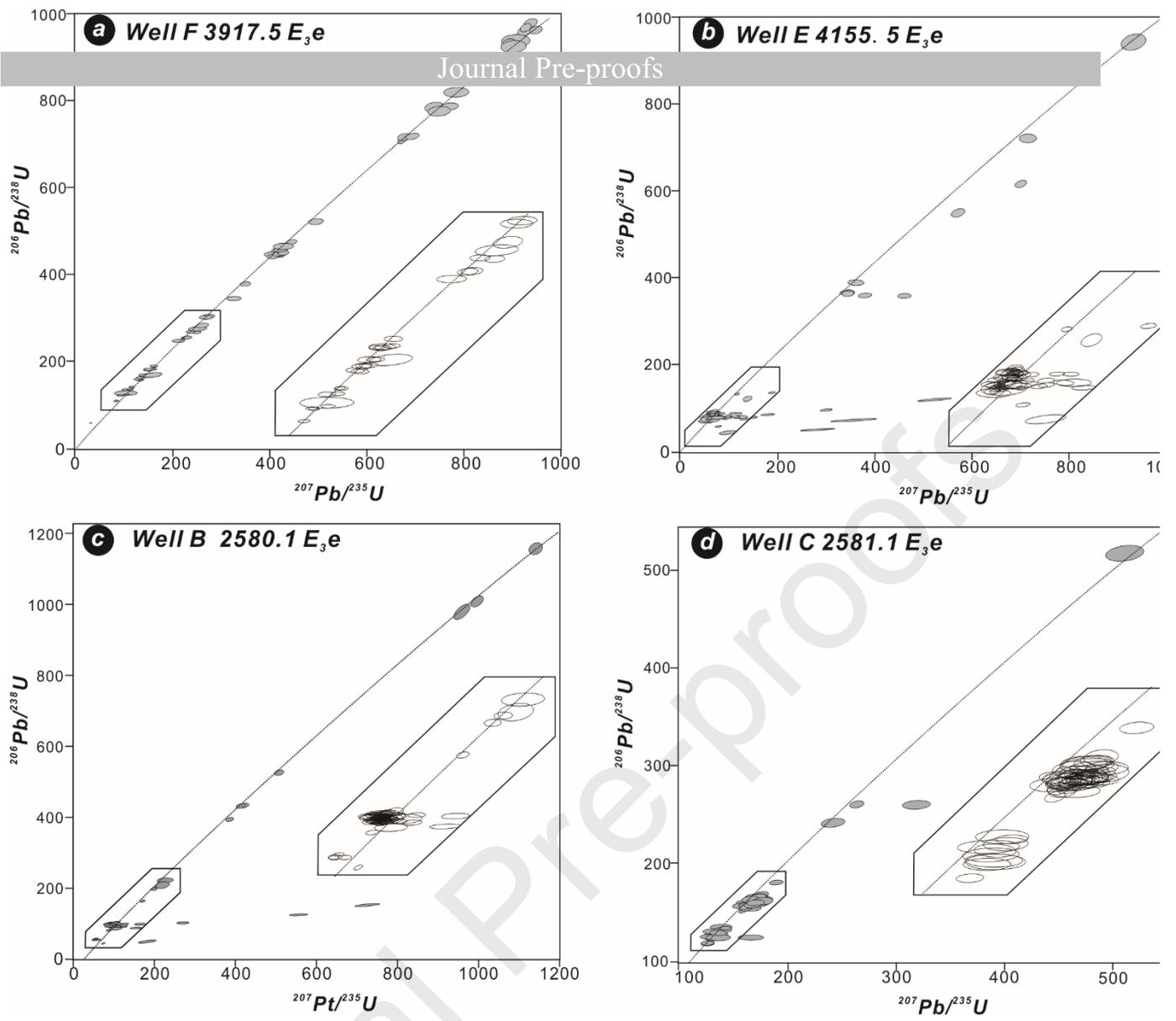


**FIG 9**





**FIG 10**



**FIG 11**

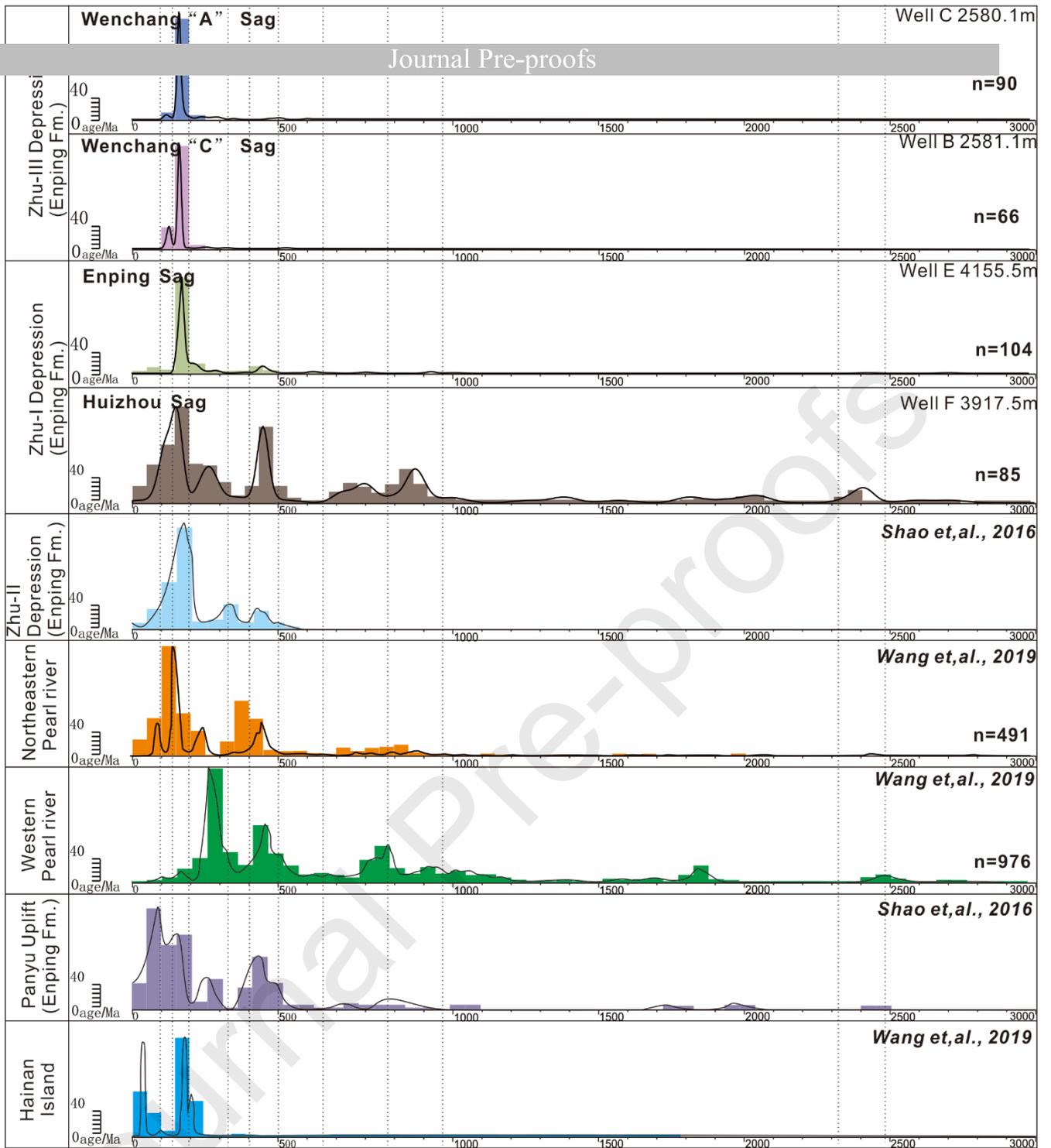
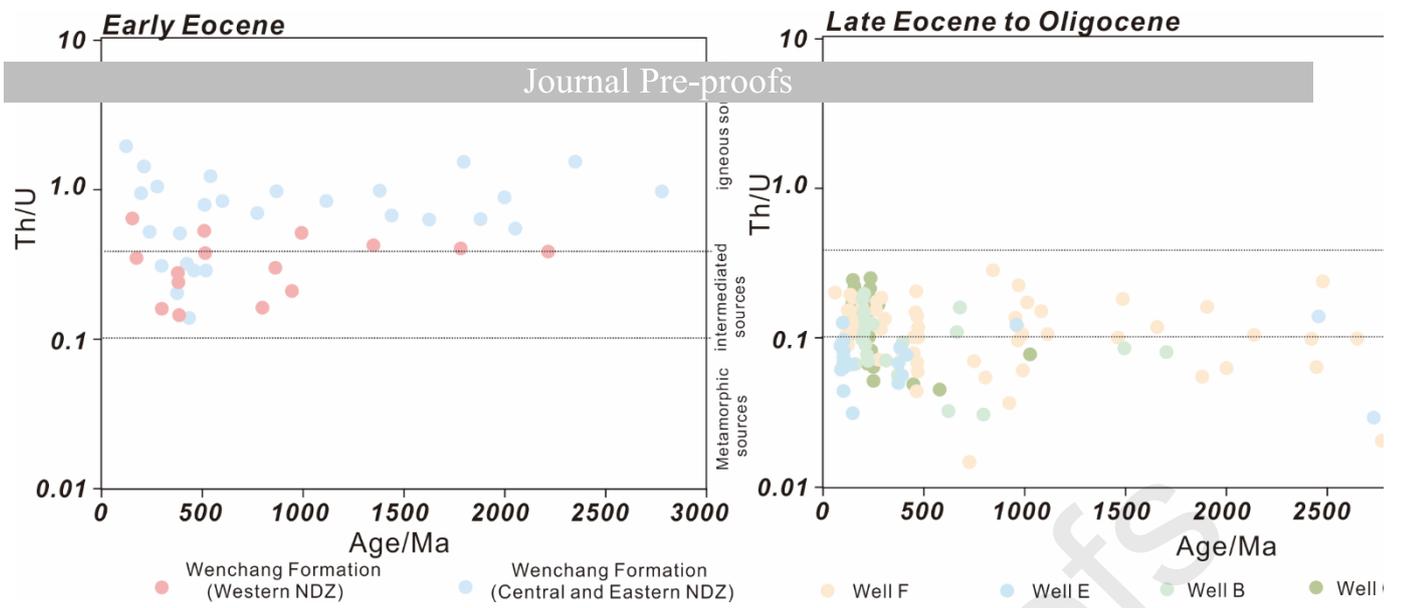
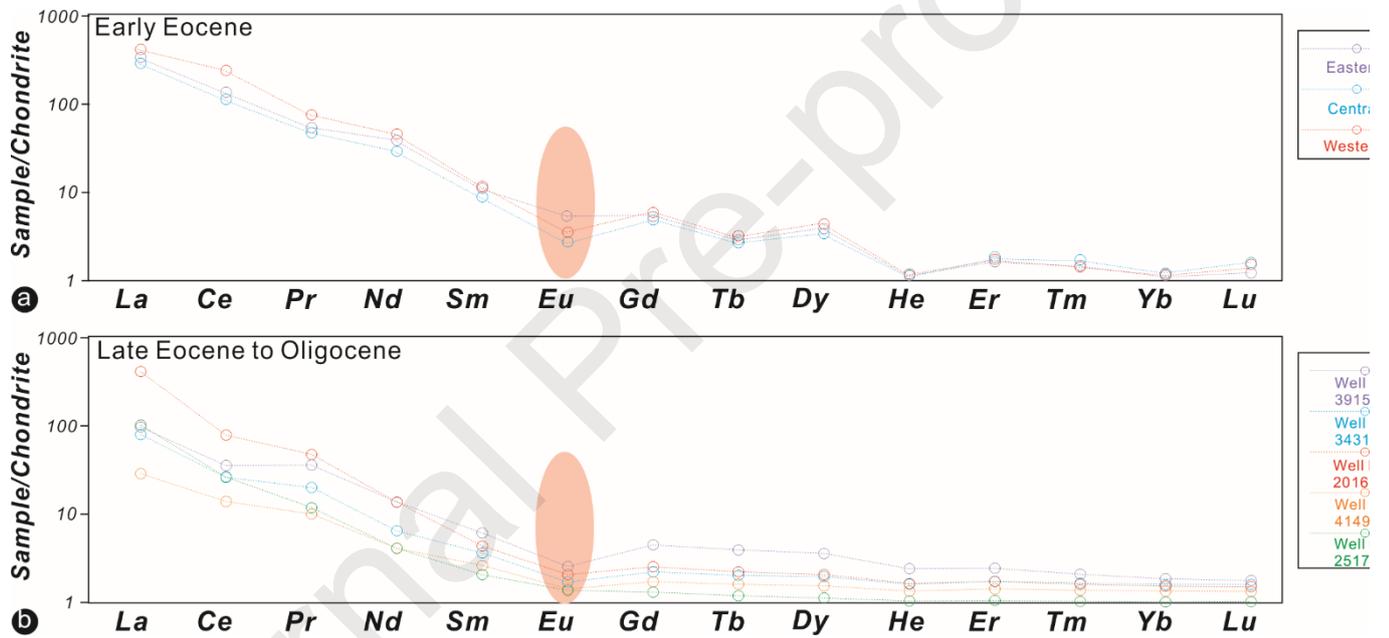


FIG 12



**FIG 13**



**FIG 14**

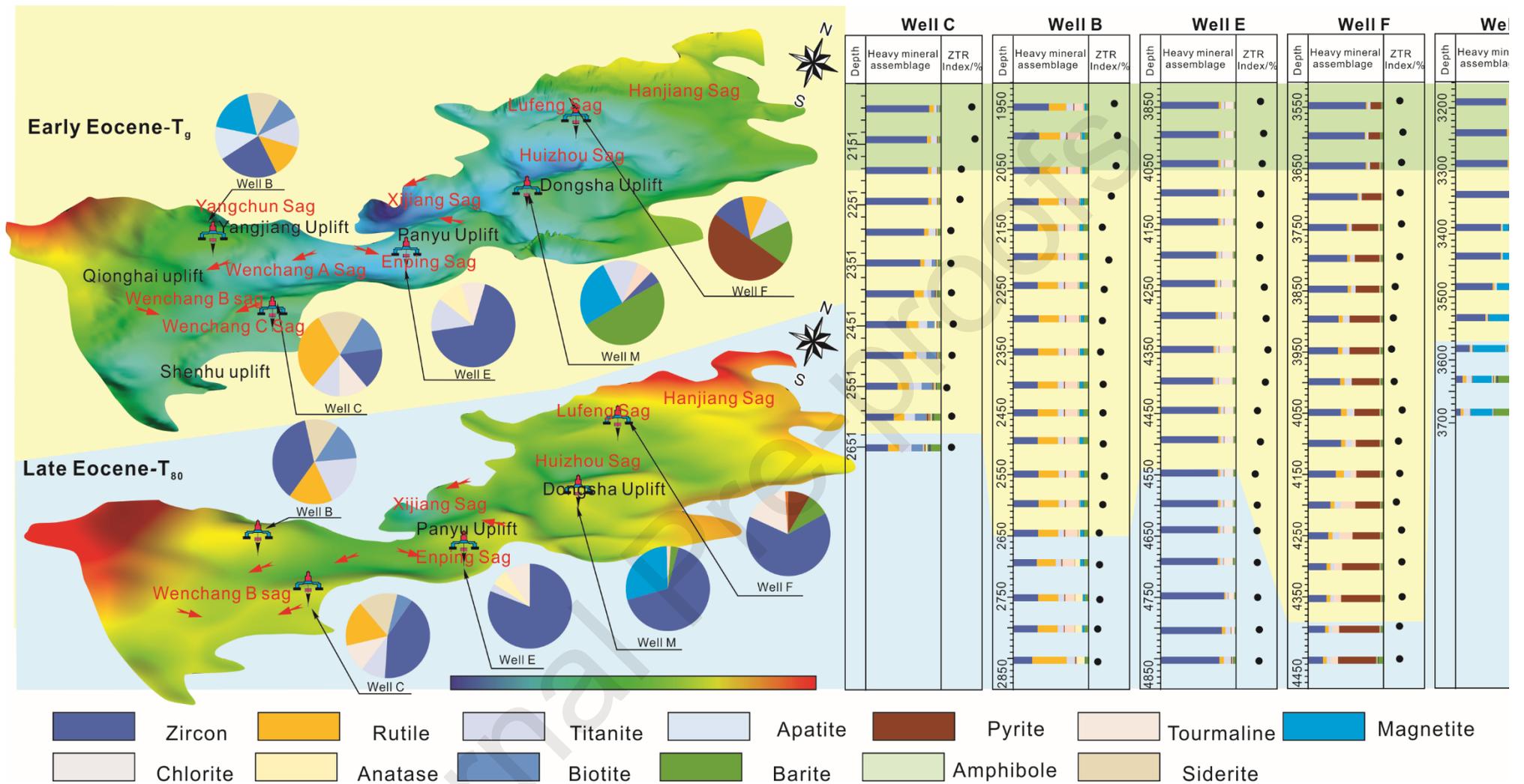
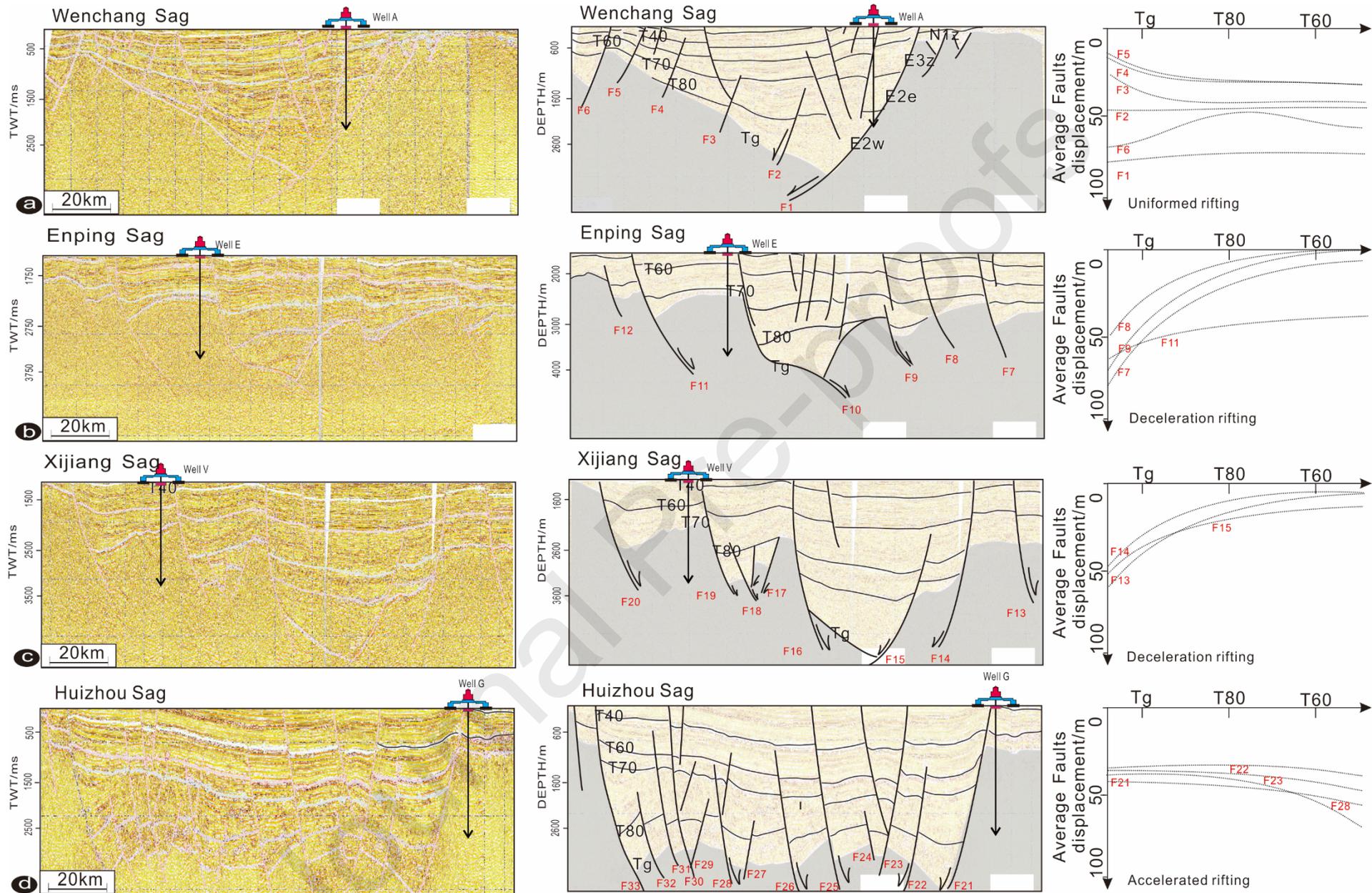


FIG 15



**FIG 16**

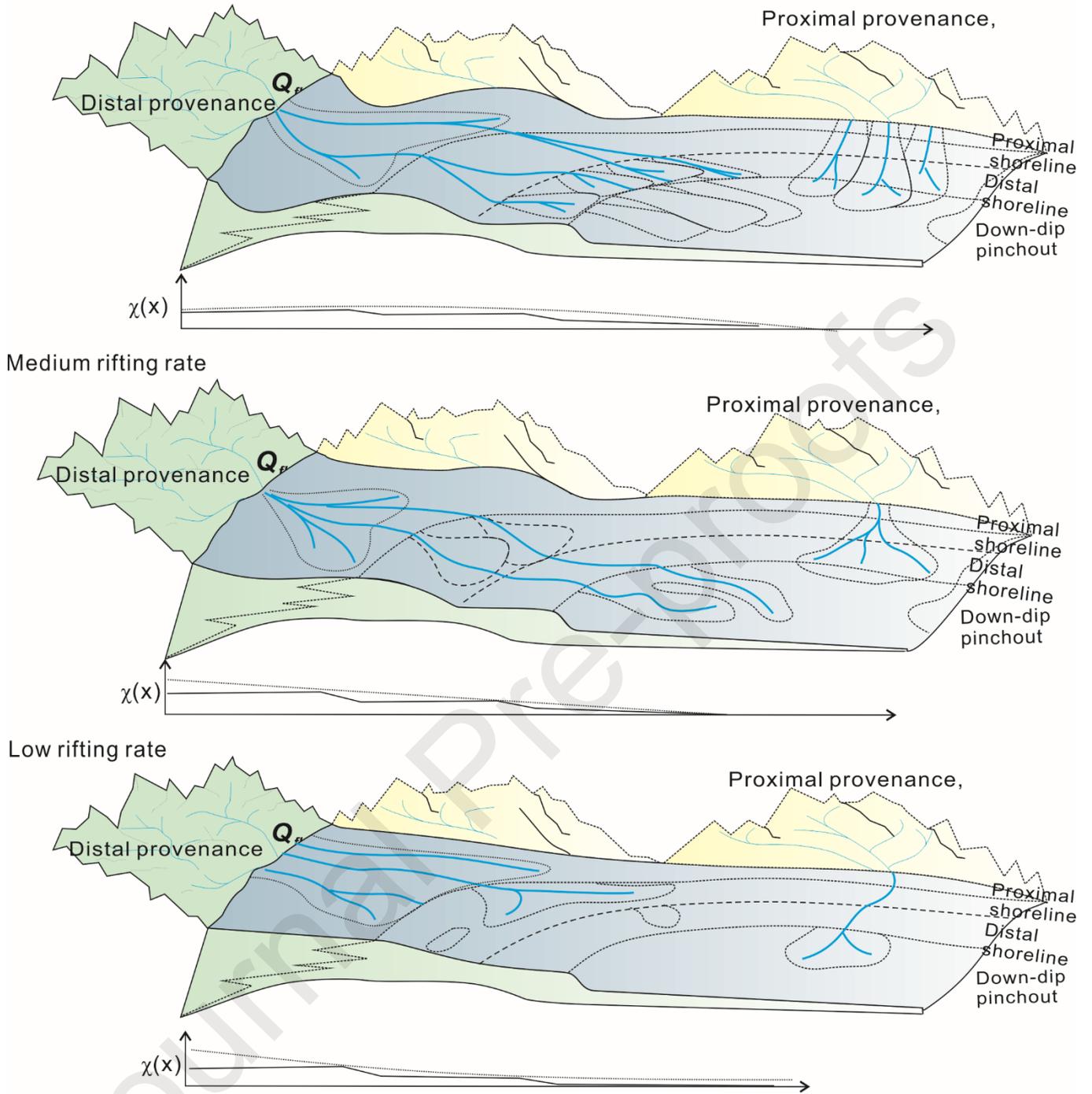
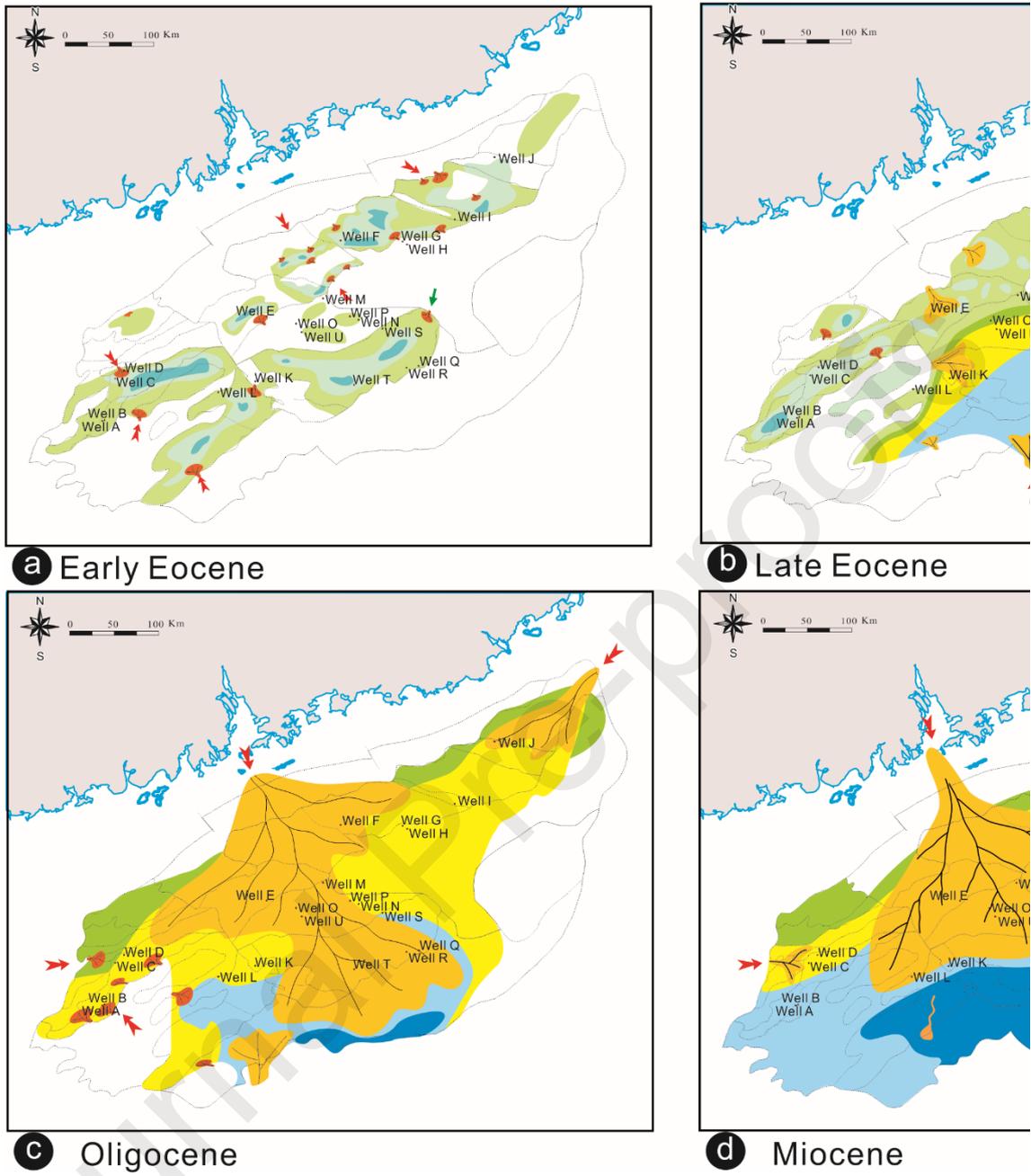
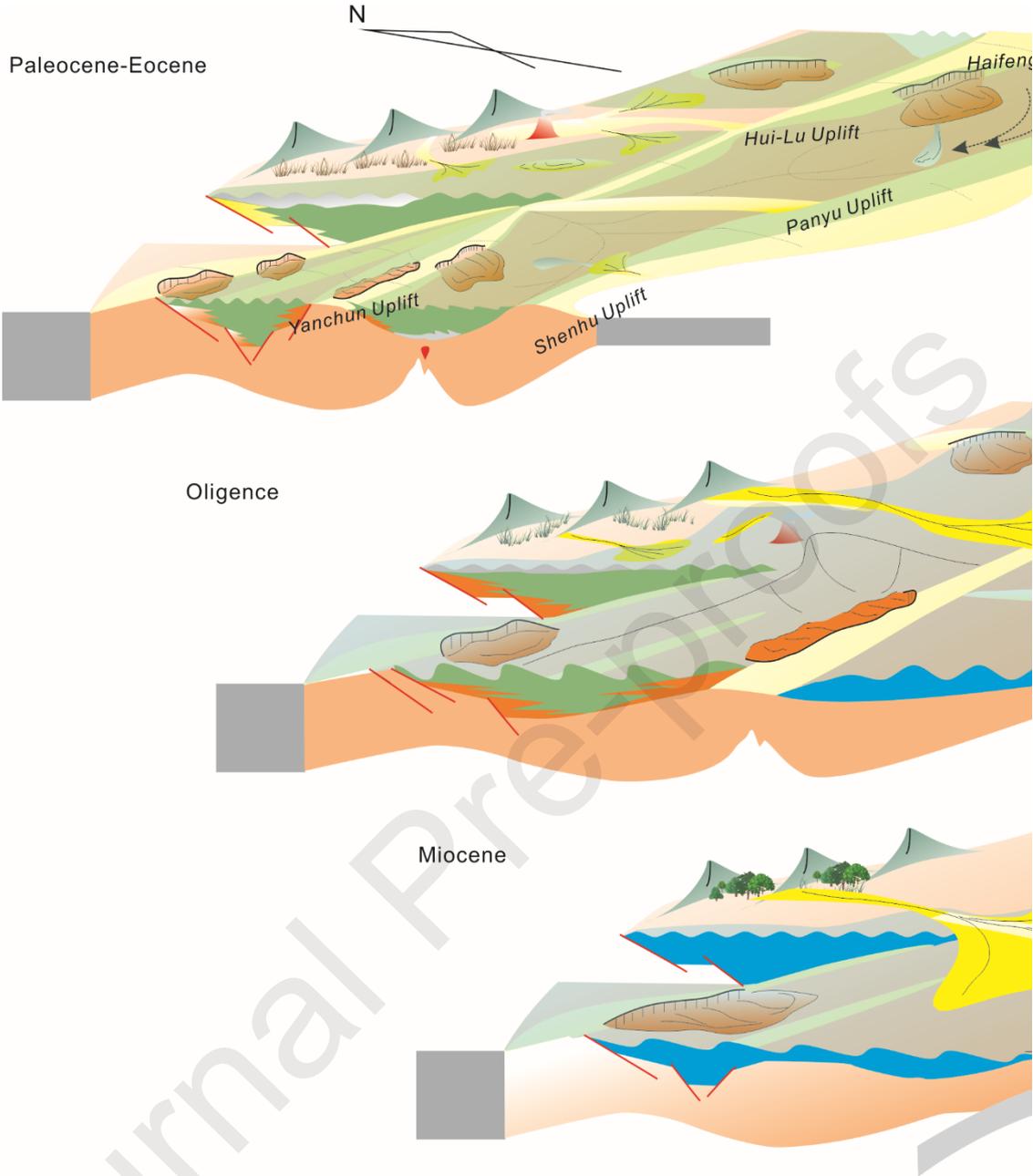


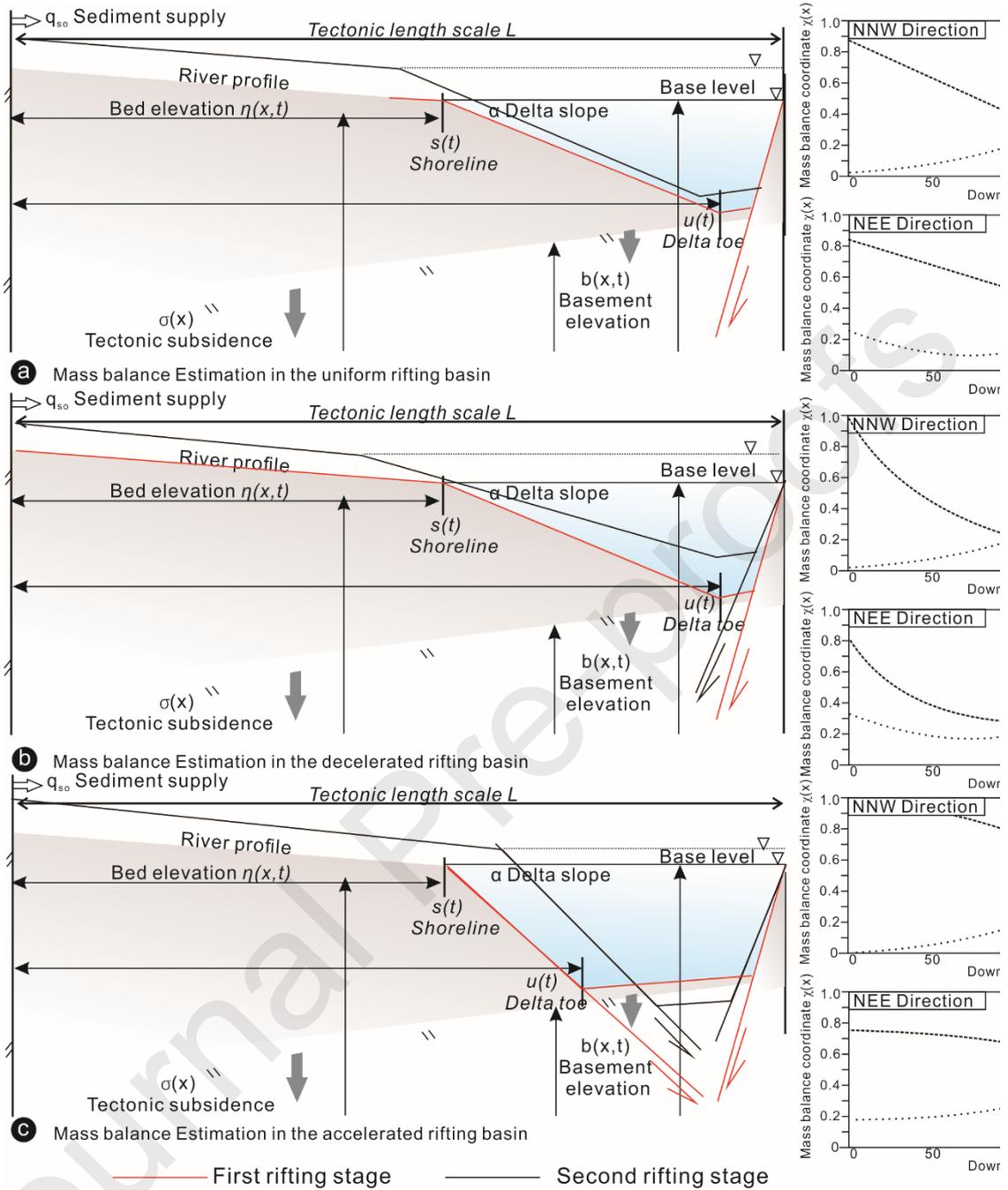
FIG 17



**FIG 18**



**FIG 19**

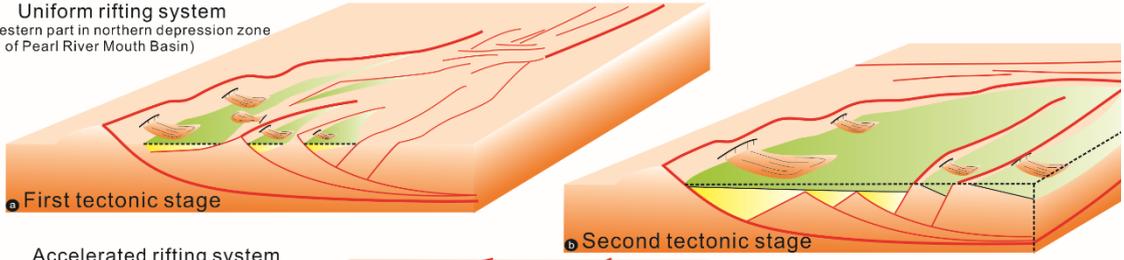


**FIG 20**

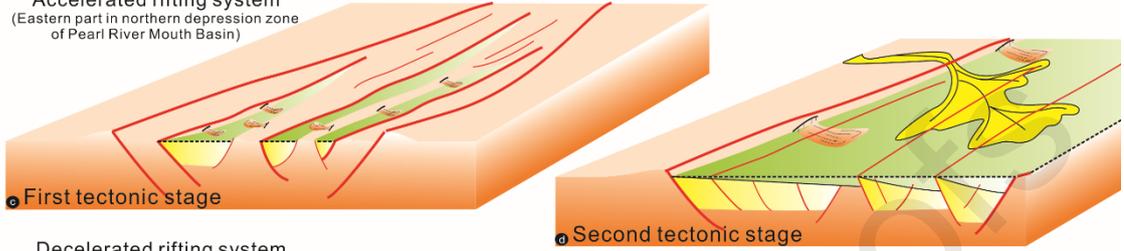
1

2

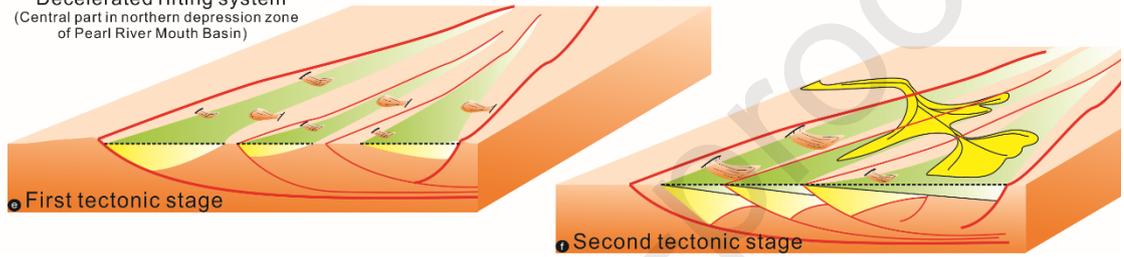
**Uniform rifting system**  
(Western part in northern depression zone  
of Pearl River Mouth Basin)



**Accelerated rifting system**  
(Eastern part in northern depression zone  
of Pearl River Mouth Basin)



**Decelerated rifting system**  
(Central part in northern depression zone  
of Pearl River Mouth Basin)



3

4

5 **Highlight**

6 1. Episodically rifting processes in PRMB include uniform rifting, decelerated rifting,  
7 and accelerated rifting according to their rifting rates.

8 2. There was a change of provenance in the North PRMB from a proximal to a distal  
9 area during the Eocene -Oligocene.

10 3. Sediment supply was the dominant factor in the decelerated rifting basin, whereas  
11 the relative height was the dominant factor in the accelerated rifting basin.

12

13

14

15

16

17

18