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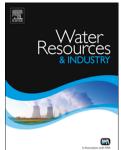
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An Experimental Study of sunflower seed husk and Zeolite as Adsorbents of Ni(II) Ion from Industrial Wastewater

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7

8 Abstract

Due to the structural similarities, sunflower seed husk (SSH), an agricultural, low-cost, and 9 eco-friendly waste, is employed interchangeably with zeolite to extract Ni (II) ions from model 10 and real industrial wastewater in this work. Batch experiment adsorption was carried out to 11 12 investigate the possibility of Ni (II) ion removal by adsorbents. Zeolite powder and SSH were used in three different sizes and without any modifications to optimize the effect of adsorbent 13 size. The maximum adsorption rate of 76% for the bulk size of SSH was obtained at pH 6.5, 14 15 20 g/L of adsoadsorbent, an initial concentration of ions of 20 mg/L, and 2 h of contact time. Thermodynamic results showed that the process is spontaneous, feasible, and exothermic 16 within the set temperature range (10°C-80°C). It can be concluded from the results that SSH 17 can be used as a feasible, eco-friendly, and biodegradable organic material for Ni ion 18 adsorption. 19

20

21 Keywords: Biosorbent, Nickel, Sunflower Seed Husk, Wastewater, Zeolite.

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23 **1. Introduction**

24 Apart from being the most necessity of all living creatures in nature, water is regarded as the most essential source of life. Water contamination and inadequacy are putting a major strain 25 on the environment, and its restricted supply is worsening as natural water sources are depleted. 26 Consequently, economic growth, human sustenance, and environmental development are all 27 28 hampered [1]. Roughly 40% of the population faces water scarcity difficulties as a result of climatic change, increased urbanization, natural resource consumption, and dietary 29 30 requirements [2]. Freshwater utilization for industrial and agricultural needs is increasing, resulting in a rise in water demand. This issue can be addressed by using recovered wastewater, 31 32 which is a relatively new source of water [3–5]. Furthermore, due to fast industrialization and 33 manufacturing expansion, a steady increase in industrial pollution and metal content has 34 occurred in rivers and agricultural regions owing to the inappropriate dumping and disposal of industrialized waste products [6]. Heavy metals, the primary component of the earth's crust, 35 36 are long-lasting environmental pollutants that can merely be transferred into nontoxic forms 37 without considering to biodegrade them purely [7]. Heavy metal pollution in aquatic systems is a worldwide concern because it is a threat to lives of living beings. Heavy metals like 38 chromium, cadmium, Ni (II), lead, zinc, and copper are common metals present in industrial 39 effluents that can be toxic and chronic, even in low concentrations [8]. Ni (II) is one of the 40 41 heavy metals that is used in silver refineries, electroplating, and the battery industry, which can 42 cause health problems like disruption of the lungs, extreme weakness, and shortness of breath. In high concentrations, it can cause different cancers and even death. Dermatitis (Ni itch) is the 43 44 most common side effect of exposure to Ni (II). In some cases, the signs of poisoning by Ni were reported as severe headaches, dizziness, nausea, and vomiting [9]. Heavy metals can be 45 removed from aqueous solutions using a variety of techniques. Ion exchange, electrodialysis, 46 precipitation, flocculation, membrane separation and sorption are common methods for heavy 47

metal uptake from wastewaters [10]. However, each of the methods mentioned above has its 48 49 own pros and cons [11]. Chemical precipitation is commonly employed in Turkey [12] and 50 Thailand [13] to remediate electroplating effluent. In China [14] and Thailand [13], 51 coagulation-flocculation has been used to remove heavy metals from inorganic wastewater. The extraction of non-surface active metal ions from industrial wastewaters utilizing sorptive 52 53 flotation has piqued interest in the US [15] and Greece [16]. Ion exchange has gained attraction 54 in Spain [17] and Italy [18] as one of the key technologies for treating heavy metal-laden wastewaters. 55

Lately, adsorption has gained the attraction of many scientists as one of the alternative 56 treatment strategies for removing heavy metals from wastewater [19]. Adsorption, in its most 57 basic form, is a mass transfer procedure in which a material is transferred from the liquid phase 58 to the solid's surface and gets bonded by physical/chemical interactions [20]. Simple process 59 and design, sludge free environment and being cost effective are the superiorities of adsorption 60 61 technique against the other methods [21]. Recently, studies have been conducted to create novel adsorbents or improve existing adsorbents to find proper alternatives to common natural 62 adsorbents like zeolite [22]. Since the earliest initiatives to purify water in the late nineteenth 63 century, zeolites as potential materials have been particularly appealing due to their low price 64 and high efficiency for heavy metals [23]. Natural zeolites are extensively employed in 65 adsorption, construction, catalysis, soil remediation, agriculture, and energy, with global use 66 of natural zeolites reaching 5.5 Mt in 2010 [24]. 67

In accordance to previous studies, numerous agricultural residues have been used to remove heavy metals (e.g. coconut husk, mango husk, corncob and cornstalk, tomato waste and green walnut shell) [25–30]. Sunflower seed (Helianthus annuus) is a kind of oil seed used in oil production industries and bakery crafts [31]. These applications produce a large amount of SSH that have low density and thus need a large space to store. Therefore, the goal of this research

is to develop a cost-effective adsorbent as well as test the effectiveness of modified SSH in 73 removing Ni(II) from synthetic and industrial wastewater. Hence, on a small scale of effluent 74 75 or low metal ion contaminated industrial wastewater, a novel, affordable modified adsorbent 76 made from agricultural waste might be used and practicable for metal ion removal. Aluminum silicate minerals like zeolite are used as commercial absorbers and catalysts. The ability of 77 78 selective ion exchange and its microporous structure make them efficient adsorbents for 79 wastewater treatment [32,33]. The mesoporous structure of zeolite is the same as that of SSH. 80 Hence, we used these two adsorbents to study the potential of SSH absorbability in comparison 81 to zeolite.

82

83 **2. Materials and methods**

84 2.1. Adsorbents

The sunflower seeds were bought from a local market in Shiraz, Iran, and then dehulled. To remove dust and other contaminants, they were washed several times with distilled water. Then, they were dried in an oven at 80°C for 24 h [34]. To optimize the size, three different sizes of SSH were utilized as adsorbents: bulk, crushed, and milled powder (see Figure 1). The zeolite powders were supplied by Afrand Tooska Company (Tehran, Iran).



93 2.2. Batch Studies

Experiments were conducted in a 100 ml beaker containing a Ni(II) ion solution with a
specified concentration. The Ni ion solutions were made from a stock solution of Ni (II) nitrate.
The solutions were stirred on a magnetic stirrer to make sure equilibrium was reached. As a
control sample, sampling was performed from a solution containing Ni ions before adding the
adsorbent. At predetermined periods after adding the adsorbent (i.e., 10, 15, 20, 30, 45, 60, 80,
100, and 120 min), the concentration of Ni(II) ions remaining in the solution was measured.

100 2.3. Experimental apparatuses

Atomic Adsorption Spectroscopy (AAS) was used to measure the Ni ion concentration in the 101 solution. The spectrometer that was used in this study was the Shimadzu A-A 680. The 102 wavelength was 232 nm and the slit width was 0.5 nm. A Fourier transform infrared (FTIR) 103 spectrometer, the Avatar model, made by Thermo Company, was used to determine the 104 functional groups of SSH, before and after adsorption. To study the morphology of adsorbents, 105 a Cambridge S360 scanning electron microscope (SEM) was used. The size of powder particles 106 was determined by a dynamic light scattering (DLS) analyzer, model SZ-100 Horiba, Japan. 107 108 To separate particles suspended in the solution were centrifuged at 10000 rpm for 10 min by a centrifuge machine, model PC-15000M. The pH values of the solutions were measured by a 109 Metrohm pH meter. 110

111 **2.4. Ion Adsorption Measurements**

A batch mode was used in all adsorption experiments on a magnetic stirrer with a rate of 90 rpm. The adsorption phenomenon was studied by adding adsorbents to 100 ml of Ni(II) ion solution with the required initial concentrations at room temperature. The percentage of adsorbed ions from solution was calculated using equation 1 [35]:

% of metal ion removed =
$$\frac{(C_0 - C_e) \times 100}{C_0}$$
 Eq. 1
116 The following equation was used to determine the adsorbent adsorption capacity [11,36]:

$$q = \frac{(c_0 - c_e)v}{m}$$
 Eq. 2

117

where c_0 and c_e are the concentrations of Ni(II) ions in the solution at the initial and equilibrium state, respectively, v is the adsorbent mass, and m stands for the adsorbent mass.

120

121 **2.5. Adsorption Isotherm**

The goal of the adsorption isotherm is to fit experimental data to the common isotherm models, such as Langmuir and Freundlich, which represent the relationship between the adsorbed ion per unit of adsorbent and the concentration of an ion in the liquid phase at equilibrium time, and are crucial in optimizing adsorbent usage. Equation 3 [37] gives the expression for the applied non-linear Langmuir model.

$$q_e = q_m \frac{k_L c_e}{1 + k_L c_e}$$
 Eq. 3

where C_e is the equilibrium ion concentration remained in the solution (mg/L), K_L is the Langmuir adsorption constant related to the capacity of adsorbent and adsorption energy, and q_m stands for the maximum adsorption capacity (mg/g).

130 The favorability of the adsorption process (R_L) was obtained from the parameters of Langmuir131 isotherm model. It can be calculate from equation 4 [38].

$$R_{L} = \frac{1}{(1+K_{L}C_{0})}$$
Eq. 4

- 132 The value of R_L specifies the state of the adsorption process, with $R_L>1$ indicating an
- unfavorable adsorption process, R_L between 0 and 1 indicating a favorable adsorption process,
- 134 $R_L=1$ showing linear adsorption, and $R_L=0$ representing irreversible circumstances.
- Equation 5 [39] also gives the Freundlich isotherm model.

$$q_e = k_f c_e^{\frac{1}{n}}$$
 Eq. 5

The *n* value in this equation indicates that the adsorption process is favorable, and K_f represents the adsorbate's adsorption capacity and intensity.

138 2.6. Adsorption Kinetics

139 The time-dependent experimental adsorption data are used for kinetic modeling [40]. To 140 estimate the removal kinetics of Ni (II) ion from an aqueous solution pseudo-first-order and 141 pseudo-second-order models were used. The pseudo-first-order model is given by equation 6.

$$\log \frac{(q_e - q)}{q_e} = -\frac{K_1}{2.303}t$$
 Eq. 6

where K₁ is the pseudo-first-order rate constant (min⁻¹), q_e is the adsorption capacity at
equilibrium state (mg/g), and q_t denotes the amount of metal adsorbed at specific times (mg/g).
Pseudo-second-order model was fitted according to equation 7:

$$\frac{t}{q} = \frac{1}{K_2 {q_e}^2} + \frac{1}{q_e}$$
 Eq. 7

145 The values of q_e , K_1 and K_2 were determined from the slopes and intercepts of the plot of $\frac{t}{q}$ 146 against t [41], and K_2 is the pseudo-second-order constant rate (min⁻¹).

147

148 2.7. Thermodynamic Studies

149 The effect of temperature on the sorption of Ni(II) ion onto the adsorbent was carried out at 150 different temperatures. Also, thermodynamic parameters including Gibbs free energy (ΔG , 151 J/mol), enthalpy (ΔH , J/mol), and entropy (ΔS , J/mol) were calculated using the following 152 equation.

$$\Delta G = \Delta G^{\circ} + RT ln K_L$$
 Eq. 8

where K_L is the Langmuir constant, R is the universal gas constant (8.314 J/molK).

154 The values of ΔH and ΔS are defined using the Vant Hoff plot from equation 9.

$$LnK_L = -\frac{\Delta H}{RT} + \frac{\Delta S}{R}$$
 Eq. 9

155 Δ H and Δ S values were determined from the slope and intercept, respectively, based on the 156 plot of LnK_L against 1/T [42,43].

157 **2.8. Pre-equilibrium pH Measurements**

To determine the pre-equilibrium pH of SSH, 1g of biosorbent was added to 100 ml of distilled
water. The samples were agitated for 48h and the pH of the solution was measured using a pH
meter.

161 **2.9. Point of Zero Charge**

A 50 ml solution of 1 M KNO₃ was prepared in multiple containers to determine the point of zero charges of the adsorbent. By adding 0.1 M of HCl or 0.1 M of NaOH solution to the KNO₃ solution, the pH was changed from 2 to 12. After recording the initial pH of the solution (pH_i), 1 g of adsorbent was added to the solution and agitated at room temperature for 48 h on a stirrer. The adsorbent solutions were centrifuged at 10000 rpm for 10 min, and the ultimate pH of the solution (pH_f) was measured. The intercept of the pH (pH_i-pH_f) versus pH_i plot was used to determine the point of no charge [36,44,45]. 169

170 **3. Results and Discussions**

171 **3.1. Morphology Studies**

- 172 Figures 2 depicts the external and internal surfaces of bulk SSH at various magnifications
- 173 determined from DLS measurements.

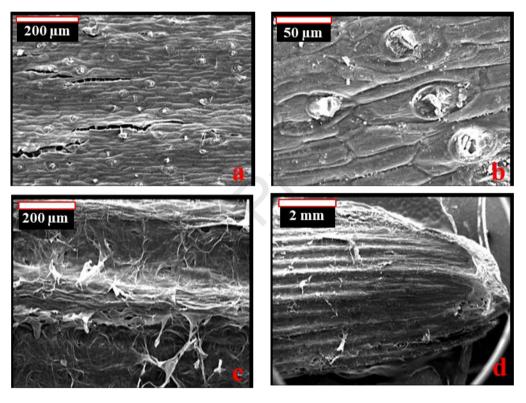




Fig. 2 Photomicrographs of the external (a and b) and internal (c and d) surfaces of SSH with different magnifications

177 The morphology of bulk external surface is smooth and nonporous but the interface of bulk

- size is rough and few small cavities are visible. The inner surface was examined with higher
- 179 magnification and it was shown in Figure 3.

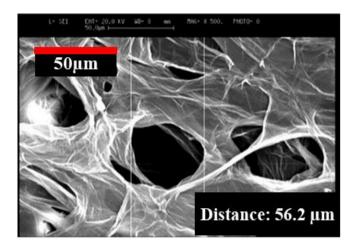
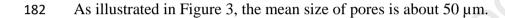


Fig. 3. SEM image of a pore in the inner surface of SSH



Many pores were found in the cross-section of SSH, indicating that the adsorbent had a porous structure. The smallest pore measured roughly 0.86 m in diameter. The Microstructure Image Processing software (MIP) was employed and the porosity of the SSH bulk was estimated as 70 %. A DLS analysis was also performed on SSH powder particles to determine the size distribution of the powders. The powdered SSH particles have an average size of roughly 9 nm.

188 **3.2. FTIR Spectroscopy**

180

181

Before and after the adsorption process, the functional group composition of the SSH was
 analyzed using Fourier transform infrared (FTIR) spectrometry. The FTIR spectra of the
 adsorbent were recorded using an infrared spectrophotometer FT/IR-5300 in the 400–4000 cm⁻¹
 ¹ range (JASCO Corp., Tokyo, Japan).

Before adsorption, the bands at 3424.61 and 2922.26 cm⁻¹ correspond to the alcohol group's O-H stretching and the alkane's C-H stretching, respectively. The values of these peaks remained unchanged after adsorption, but the intensity of the peaks changed. The peaks at 1729.5, 1030.2, and 1244.9 cm-1, as shown in Figure 4, correspond to the C=O stretching α , β unsaturated ester, S=O stretching sulfoxide, and C-N stretching amine, respectively. Following adsorption, these bands changed to 1733.74 cm⁻¹, 1028.96 cm⁻¹, and 1242.85 cm⁻¹, indicating

a significant decrease in the intensity of these peaks. After adsorption, the peak at 827.53 cm⁻¹
 which belonged to the minerals, slipped away.

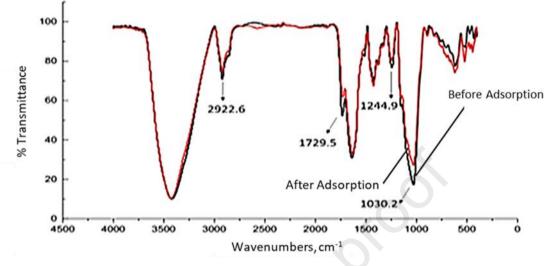




Fig. 4. Differences between peaks of FTIR spectra before and after Nickle sorption onto SSH

3.3. Effects of adsorbent type on the Ni ion adsorption efficiency

To find out the capacity of adsorbents (SSH and Zeolite) for Ni (II) removal from solution, in the first step, 3ml solution containing Ni (II) ion (pH=6.5, Co=20 mg/L, T=24 C°) were taken to specify the total dissolved solution (TDS value) of water after adding the adsorbent to the solution and calculate the percentage of Ni (II) ion removal by different adsorbents. The TDS value for distilled water was determined as 12.38 ppm, and for the solutions containing different sizes of SSH (i.e., powdered, crushed, and bulk) and zeolite were measured as 111.10, 137.50, 71.12, and 118.25 ppm, respectively.

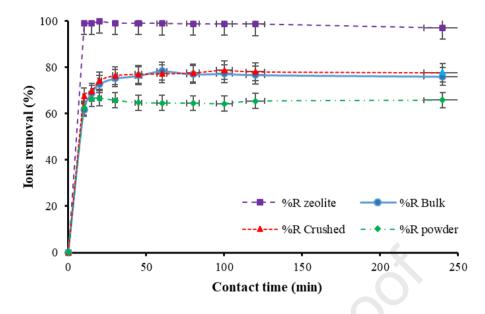
SSH removed approximately 76 % of Ni (II) ions in bulk and crushed forms. Powdered SSH and zeolite, on the other hand, could remove approximately 62 % and 92 % of the Ni (II) ions from the solution, respectively. The TDS value is one of the factors used to assess water purification and quality [46]. The diagram shows that the amount of TDS in the crushed and powdered sizes of SSH, as well as the zeolite powder, was very high. Some other studies have generally claimed that powder samples have better sorption capacities when used to remove some kinds

of ions from aqueous solutions due to their larger surface areas [47]. However, in the present study, bulk samples were found to be better absorbents than powder samples in Ni (II) ion removal from aqueous solutions with no significant TDS increase. As a result, bulk size SSH was used as an adsorbent in our experiments. The percentage of Ni (II) ion removal by SSH and zeolite differed by almost 16%. So, the ability of SSH to absorb Ni (II) ions is comparable to that of an adsorbent such as zeolite.

222 **3.4. Effect of Contact Time**

The rate of ion removal is one of the most important factors to predicting the required time for water treatment. Thus, to estimate the needed time for Ni (II) ion removal by SSH and zeolite, 2g of SSH in three different forms and zeolite powder were added to 100 ml solution with the initial concentration of Ni (II) ion (20 mg/L), in separate containers (initial pH= 6.5, T=25 C°). The rate of Ni (II) ion adsorption in the presence of zeolite and SSH with different sizes is shown in Figure 5.

229 The rapid ion removal rate by adsorbents in the first 15 min is seen in contact time plots, and the required time to attain equilibrium was roughly 120 min, and the rate of adsorption 230 remained constant after equilibrium. During the sorption process, the sorbent surface has 231 numerous binding sites. Therefore, there is no competition amongst ions for sites at first, but 232 as time passes, available sites are filled by other ions, and there are insufficient sites for ion 233 234 adsorption. The repulsive forces between the adsorbed ions on the sorbent surface and the 235 remaining ions in the solution, on the other hand, make the adsorption process more difficult than it was in the beginning. As a result, after attaining equilibrium, the rate of adsorption 236 decreased with time. 237





239

Fig. 5. Rate of Ni (II) ion sorption by zeolite and different sizes of SSH

240 **3.5. Effect of pH on the Sorption Process**

Metal ion adsorption depends strongly on pH values. Ironically, the pH of the system regulates the adsorption capacity by influencing the surface characteristics of the adsorbent and the ionic forms of Ni (II) in the solution [48,49]. To investigate the effect of pH on Ni (II) ion removal by SSH, four different pH values in the range of 1.5 to 9.4 were examined. The batch studies were carried out under the aforementioned conditions (adsorbent dosage= 2 g, Ni (II) ion concentration=20 mg/L, and T=25 °C). The results are presented in Figure 6 before and after adding the adsorbent.

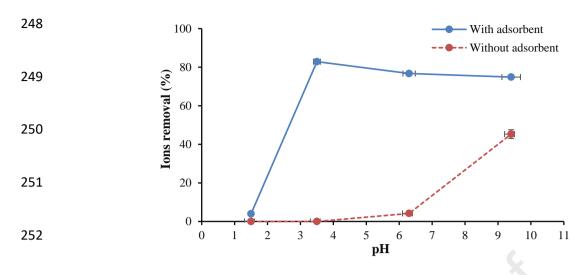


Fig. 6. Percentage of Ni (II) ion removal at different pH conditions in the presence (solid line) and absence
(dashed line) of the adsorbent

As the results show, the maximum adsorption occurred at pH 3.5 and decreased gradually by 255 increasing the pH to 9.4. This reduction was due to the precipitation of Ni (II) ions because of 256 257 the formation of Ni (II) hydroxide complexes [50]. To substantiate this conclusion, the initial concentration of the batch was set to 20 mg/L and then the pH range was changed from 1.5 to 258 9.4 without sorbent. Then, at specified pH values, the amounts of Ni (II) ions remained in the 259 solution were determined. After increasing pH to 9.5, the amount of initial Ni (II) concentration 260 reduced, indicating that complexation and precipitation occur at higher pH values. The amount 261 262 of adsorption was negligible at pH 1.5. This can be described in terms of PZC, which is the electrical potential at an adsorbent's surface and was determined to be 1.8 in our case, as shown 263 264 in Figure 7.

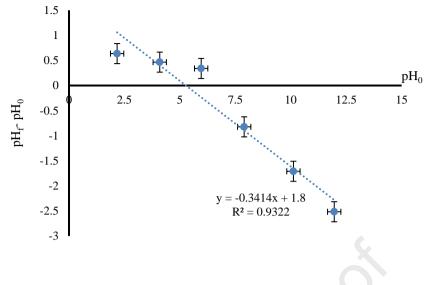


Fig. 7. PZC for the SSH solution

The surface of the adsorbent is negatively charged at any pH higher than 1.8, hence the ratio 267 of Ni (II) ions adsorption increases dramatically when the pH is changed from 3.5 to 6.5. 268 Conversely, the ions should compete with H+ ions for active site adhesion below the PZC due 269 to repulsive forces on the sorbent surface. As a result, at low pH values, the adsorption 270 percentage is negligible [51]. For additional testing, the optimum pH for Ni (II) ion removal 271 by SSH was determined to be 6.5. Argun observed that the highest rate of adsorption of Ni (II) 272 ion by zeolite occurred at pH 7 [52]. For low and high values of pH, the process of adsorption 273 was the same as for SSH. 274

275 **3.6. Effect of Temperature on the Sorption Process**

265

266

276 2g of adsorbent were introduced to 100 ml of solution with an initial concentration of 20 mg/L 277 at pH 6.5 to investigate the influence of temperature on Ni (II) ion sorption by SSH. The 278 sorption effectiveness of Ni (II) ions increased by 67.5% when the temperature was reduced 279 from 80 to 10 °C. With increasing temperature from 10 to 80 °C, the adsorbent capacity reduced 280 from 0.877 to 0.183 mg/g. The increased adsorption of Ni (II) ions by SSH can be attributed to 281 the lower energy of Ni (II) cations, resulting in more interaction between metal ions and active 282 sites on the adsorbent surface [53]. The effect of temperature on the adsorption of Ni (II) ions

is shown in Figure 8. Similarly, Hannachi et al. investigated zeolite, and their findings revealed

that the sorption of Ni (II) ions by zeolite increased with increasing temperature [54].

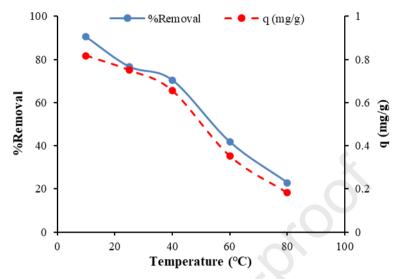




Fig. 8. Effect of temperature on adsorption process of Ni (II) ions

3.7. Effect of Adsorbent Dosage and Initial Ni (II) Ion Concentration on the Sorption Process

Figure 9 (a and b) shows the capacity and efficiency of Ni (II) ion adsorption by SSH as functions of the adsorbent, respectively. The effect of adsorbent dosage on the uptake of Ni (II) ion at pH 6.5, 20 mg/L initial ion concentration, and at ambient temperature was examined. The amount of sorbent varied between 1 and 4 g in a 100 ml solution.

As can be deduced from Figure 9 b, the increase in adsorbent dosage from 10 to 40 g/L causes an increase in the adsorption of Ni (II) ions from 67% to 88%. This substantial increase is because of the increased surface area of the adsorbent and more accessible active sites for the adsorption of Ni (II) ions. To compare the dose of the adsorbent parameter by zeolite, Cocaoba et al. conducted a similar study. They reported the same trend for Ni (II) ion sorption by zeolite. They showed that the efficiency of Ni (II) ion sorption by zeolite increased to 81.6% by increasing the amount of sorbent from 0.2 to 2 g [55].

300 The Ni (II) ion adsorption capacity and efficiency of SSH in Ni (II) removal from the solution are respectively presented against time in Figures 9 (c and d). The initial concentration was 301 changed from 10 to 35 mg/L. As shown in Figure 9c, by increasing the initial Ni (II) ion 302 concentration from 10 to 35 mg/L, the residual Ni (II) ion concentration of the solution 303 increased. Hence, the efficiency of Ni (II) ion sorption decreased. However, the capacity of the 304 adsorbent increased from 0.36 to 1.31 mg/g by increasing the initial concentration of Ni (II) 305 306 ions. This can be due to increasing the driving force of Ni (II) ions in high concentration solutions [30]. The Ni (II) ion uptake increased rapidly with time up to 35 min and then 307 308 increased slowly. According to the results, the adsorption equilibrium time was 120 min. Cocaoba et al. studied the effect of Ni (II) initial concentration on zeolite as a biosorbent. In 309 their study, the initial concentration changed from 1 to 100 mg/L. The results showed that Ni 310 (II) ion sorption rate was rapid for the first 10 min and thereafter it increased slowly to reach 311 an equilibrium time of 80 min [55]. 312

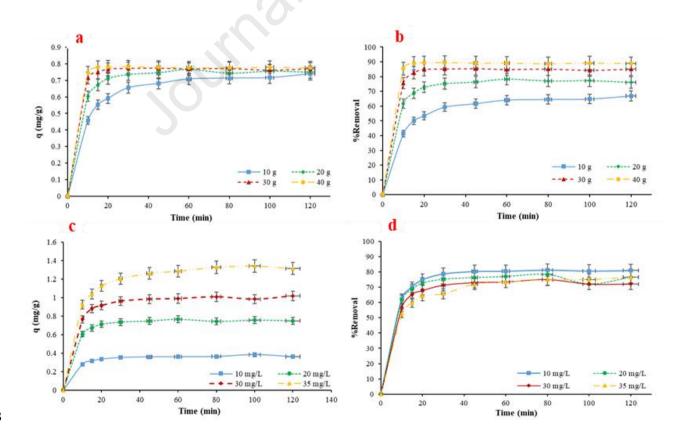
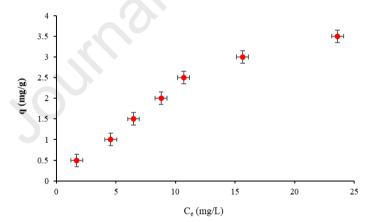


Fig. 9. Effect of sorbent dosage and initial concentration of Ni (II) on the adsorption capacity of SSH
(respectively shown in figures a and c), and on the percentage of Ni (II) removal by SSH (respectively shown in figures b and d)

317 **3.8. Adsorption Isotherm**

The adsorption isotherm's purpose is to fit adsorption experimental data using prevalent isotherm models that represent the relationship between the adsorbed ion per unit of adsorbent and the concentration of an ion in the liquid phase at equilibrium time.

As demonstrated in Figure 10, the amount of Ni (II) absorbed by the adsorbent increased sharply after the equilibrium starting concentration was increased, and subsequently the trend went toward a plateau. It could be owing to the energy of ion adsorption at varying concentrations. In low concentrations of Ni (II), ion adsorption on active sites requires more energy to bind these sites, while in high concentrations, the opposite is true [56].



326 327

Fig. 10. Changes in the Ni (II) ion removal against different equilibrium concentrations

Langmuir and Freundlich isotherm models were utilized to determine the interaction between SSH and Ni (II) ions. The results are depicted in Figure 11. Within the SSH, the Langmuir isotherm model predicts monolayer adsorption of Ni ions on a homogeneous surface. Adsorption of adsorbate on an adsorbent occurs on a heterogeneous surface by multilayer sorption in the Freundlich model, and the adsorption capacity can be improved by increasing the adsorbent dosage. Eq. 5 gives a non-linear Freundlich isotherm model. The *n* value in this

equation denotes the favorability of the adsorption process, while K_f represents the adsorption capacity and intensity of the adsorbate. The experimental isotherm data were fitted to the Langmuir and Freundlich models to distinguish between heterogeneous and homogeneous adsorption of the Ni (II) ion on SSH. The parameters of these models are tabulated in Table 1.

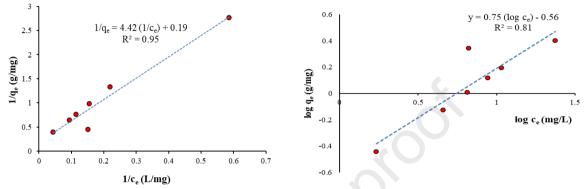


Fig. 11. Models for Ni ion removal by SSH: Langmuir (left) and Freundlich (right) adsorption isotherms



Table 1. Parameters of the Langmuir and Freundlich models

Freundlich model			Langmuir model			
\mathbb{R}^2	Ν	K _f (mg/g)	R ²	K _L (L/mg)	q _m (mg/g)	Adsorbed ion
0.81	1.34	0.28	0.95	0.04	5.29	Ni (II)

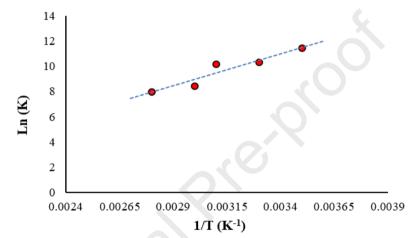
340

The Langmuir model could better predict the sorption process of Ni (II) ions on SSH. The *n* values in equation 5 were found to be more than 1 despite the fact that the adsorption process did not match the Freundlich model properly. It indicates that Ni (II) ion sorption on SSH was favorable [57,58].

From Table 1 the equilibrium adsorption capacity of SSH was found to be 5.29 mg/g under the optimized situations. It may be concluded that the SSH can be applied to remove Ni (II) ions from aqueous solution. Hence, the isotherm of Ni (II) sorption on zeolite was investigated and the results showed that sorption of Ni (II) on SSH by zeolite was fitted to the Langmuir model and the sorption was also monolayer [59,60].

350 **3.9. Thermodynamic Parameters**

The effect of temperature on Ni (II) ion sorption onto SSH was investigated at five different temperatures: 283, 298, 313, and 353 K, based on the change in ion adsorption capacity when the temperature was varied. Equation 9 was used to calculate thermodynamic characteristics such as Gibbs free energy (G, kJ/mol) and standard Gibbs free energy (G°, kJ/mol), enthalpy (H, kJ/mol), and entropy (S, kJ/molK), as tabulated in Table 2. The values of H and S were calculated using the Vant Hoff plot (see Figure 12) [61–63].



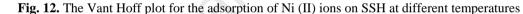


		Table 2. The	ermodyna	mic parameters	
$\Delta G0$	(kJ/mol)	$\Delta G(kJ/mol)$	T (K)	$\Delta S^{0}(kJ/molK)$	$\Delta H^{0}(kJ/mol)$
-	26.97	-9.54	283.15		
-	25.52	-7.15	298.15		
-	26.44	-7.13	313.15	-0.052	-42.07
-	23.29	-2.72	333.15		
	23.41	-1.59	353.15		

360

357 358

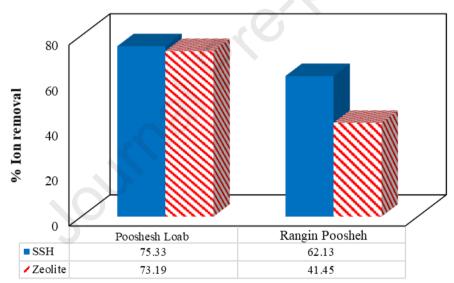
359

The spontaneous nature of Ni (II) ion sorption on SSH is indicated by the negative values of G at all temperatures. With increasing temperature, the negative values indicate stronger adsorptive forces between Ni (II) ions and SSH. The sorption process had an enthalpy value of 42.07 (kJ/mol), indicating that Ni (II) ion adsorption on SSH is exothermic. Negative S values indicate that the randomness of the solid/solution interface is decreasing [64]. Argun et al. investigated the effects of temperature and thermodynamic behavior on Ni ion adsorption by

367 zeolite. They discovered that the adsorption process was spontaneous and that both the enthalpy368 and the entropy were negative [52].

369 3.10. Comparison the Performance of Ni (II) Ion Sorption from an Industrial Effluent by 370 SSH and a Selected Zeolite

To study the industrial application of adsorbates, effluents from two different companies (Pooshesh Loab and Rangin Poosheh, Shiraz, Iran) were collected. Ni (II) ion concentrations in Pooshesh Loab and Rangin Pooshesh were 115.5 and 59.83, respectively. Due to the high concentration of Ni (II) in the effluents, 5g of adsorbent was used in each experiment, and the results are shown in Figure 13.



376
 377
 378
 Fig. 13. Comparison of the Ni (II) ion removal percentage from industrial wastewater samples by SSH and Zeolite

The results show that the percentage of Ni (II) ion sorption by SSH in solutions with higher concentrations of Ni (II) ions was greater than their adsorption by zeolite. The reason for this is the selective properties of zeolite. Since industrial effluents contain other heavy metal ions apart from Ni ions, the active sites on the surface of zeolite were saturated, and the Ni (II) ion sorption was less probable [32]. Therefore, it can be deduced that Ni (II) ion removal from industrial effluents is more efficient by SSH than zeolite.

386 4. Conclusions

387 In this study, SSH was used to adsorb Ni ion at different contact times in three different sizes: bulk (20 mm), crushed (7 mm), and milled powder (10 nm). SEM was used to examine the 388 surface and morphology of different shapes, and DLS was used to determine particle sizes. The 389 concentration of Ni (II) ions was also measured using atomic absorption spectroscopy (AAS) 390 before and after the adsorption process. FTIR tests were used to determine the active groups 391 on the adsorbent's surface before and after Ni (II) adsorption. The SEM micrographs show the 392 393 bulk SSH surface's rough, tubular, and porous structure, which is suitable for use as an absorbent. The maximum absorbing rate for bulk SSH was 76%, while zeolite absorption was 394 395 86%. The effects of pH, adsorbent dose, initial Ni (II) ion concentration, temperature, and 396 contact time were investigated. The optimum adsorption of Ni (II) ions was observed at pH 6.5, 20 g/L adsorbents, an initial ion concentration of 20 mg/L, and a contact time of 2 h. In 397 addition, the Langmuir isotherm model fit the experimental metal absorption values well. The 398 thermodynamic parameters analysis revealed that the process was spontaneous, feasible, and 399 exothermic within the specified temperature range (10-80 °C). Eventually, waste bulk SSH 400 can be used as a biodegradable organic material to absorb the Ni ion from industrial wastewater. 401 402

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Declaration of interests

 \boxtimes The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

□The authors declare the following financial interests/personal relationships which may be considered as potential competing interests: