

# **FeIII-substituted brucite: Hydrothermal synthesis from (Mg0.8FeII0.2)-brucite, crystal chemistry and relevance to the alteration of ultramafic rocks**

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# **FeIII-substituted brucite: hydrothermal synthesis from (Mg0.8,FeII** <sup>1</sup> **0.2)-brucite,**

# <sup>2</sup> **crystal chemistry and relevance to the alteration of ultramafic rocks**

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# **Abstract**

12 Ferroan brucite,  $(Mg,Fe)(OH)_2$ , is a common mineral product of serpentinization reactions. The alteration of ferroan brucite under subsurface conditions is expected to form magnetite and 14 hydrogen  $(H_2)$ . Ferroan brucite,  $(Mg_{0.8}Fe_{0.2})(OH)_2$ , with a grain size of  $20 - 100$  nm, was synthesized by precipitation of iron salts in the presence of NaOH under sub-anoxic conditions. Both composition and grain size of the synthetic product are similar to those of ferroan brucite found in serpentinized peridotites collected during the Oman Drilling Project. Synthetic ferroan brucite was then reacted in aqueous solutions at 378 and 403 K during 1 to 36 days either in PTFE-lined reactors or in gold capsules placed in externally heated pressure vessels. In gold capsules, ferroan brucite barely reacted 20 and minor magnetite and  $H_2$  were produced. In PTFE-lined reactors, reaction progress over 75% could be achieved with reaction products composed of magnetite, pyroaurite  $[Mg_6Fe_2(OH)_{16}(CO_3) \cdot 4.5H_2O]$ , and a new phase, identified as ferrian brucite  $[(Mg<sub>0.8</sub>Fe<sup>III</sup><sub>0.2</sub>)O<sub>0.2</sub>(OH)<sub>1.8</sub>]$  based on the Rietveld refinement of its X-ray powder diffraction data,  $F^{\text{III}}/Fe_{\text{tot}}$  colorimetric determination and thermogravimetric analysis. Ferrian brucite is isostructural to ferroan brucite and displays the same iron/magnesium ratio. However, all iron is trivalent. X-ray diffraction and thermogravimetric data support deprotonation as the mechanism responsible for 27 charge compensating Fe<sup>II</sup> oxidation (Fe<sup>2+</sup> + OH<sup>-</sup> => Fe<sup>3+</sup> + O<sup>2-</sup>). The difference in reaction products 28 obtained with the two types of reactors is attributed to the higher permeability to  $H_2$  (and/or  $O_2$ ) of the PTFE-lined reactors compared to gold capsules. Ferroan brucite conversion into ferrian brucite was unexpectedly fast and proceeded in a few days. The thermodynamic stability of ferrian brucite is discussed as a function of oxygen fugacity and pH.

 **Keywords:** ferroan brucite oxidation, ferrian brucite, serpentinization, low-temperature alteration, H<sup>2</sup> production.

### **1 Introduction**

 Seepages of natural H2-containing gas are encountered onshore in association with ultramafic bodies that interact chemically with meteoritic waters under sub-surface conditions (Neal and Stanger 1983; Coveney et al. 1987; Abrajano et al. 1990). Petrographic investigation of Oman ophiolite samples has actually shown that the alteration under subsurface conditions of minerals bearing ferrous iron hosted in partially to fully serpentinized samples can lead to further iron oxidation, probably coupled with H<sup>2</sup> production (Mayhew et al. 2018; Ellison et al. 2021). Among serpentinization mineral products, ferroan brucite appears to be the most reactive in the course of low-temperature alteration processes and has thus been the subject of growing interest as a possible contributor to low 44 temperature  $H_2$  generation which may in turn fuel hydrogenotrophic microbial activity (Malvoisin 2015; Jöns et al. 2017; Miller et al. 2017; Klein et al. 2020; Templeton and Ellison 2020).

 Brucite structure was initially determined by Aminoff (1921) and is composed of layers of edge-sharing octahedra. Subsequent investigations of structural analogues by infrared spectroscopy (Brindley and Kao 1984) and neutron diffraction (Chakoumakos et al. 1997) showed that hydroxyl 49 groups are perpendicular to the layer. Ferroan brucite,  $(Mg_{1-x}Fe^{II}_x)(OH)_2$ , preserved in serpentinized peridotites contains significant divalent iron with *x* generally ranging from 0.15 to 0.4 per formula unit in samples collected at mid-ocean ridges, in ophiolites, and in forearc settings (D'Antonio and Kristensen 2004; Bach et al. 2006; Beard et al. 2009; Klein et al. 2009, 2014; Kodolányi and Pettke 2011; Kodolányi et al. 2012; Frost et al. 2013; Schwarzenbach et al. 2016; Malvoisin et al. 2020). 54 Thermochemical models have shown that equilibrium between the  $Fe(OH)_2$  component of ferroan 55 brucite and magnetite buffers the  $H_2$  activity (e.g., McCollom and Bach 2009) through the equilibrium:

$$
3 \text{ Fe(OH)}_2 = \text{Fe}_3\text{O}_4 + \text{H}_2 + 2 \text{ H}_2\text{O} (1)
$$

58 Reaction (1) can also be used to calculate  $Fe(OH)_2$  activity in brucite at a given  $H_2$  partial pressure assuming a ferroan brucite solid-solution model and knowing the thermodynamic parameters 60 of the Fe(OH)<sub>2</sub> end-member. Thermodynamic models involving Fe-bearing brucite that reasonably  reproduce natural observations and experimental data have been proposed (Bach and Klein 2009; Klein et al. 2009, 2013; McCollom and Bach 2009; Jöns et al. 2017). On simple thermodynamic grounds, it can be predicted that ferroan brucite initially formed by oceanic serpentinization may further produce H<sup>2</sup> when exposed to meteoric water. According to Reaction (1), potential change in 65 H<sub>2</sub> activity will lead to the production of more magnetite (and additional H<sub>2</sub>), thereby consuming the 66 Fe(OH)<sub>2</sub> component of ferroan brucite. Such a change in H<sub>2</sub> activity may occur by dilution due to fluid infiltration, loss to the atmosphere, or consumption through microbial activity (Takai et al. 2004; Petersen et al. 2011; Myagkiy et al. 2020). This simple mechanism of H<sup>2</sup> production through near- surface fluid-rock interactions might be more complicated in natural systems where aqueous fluids 70 contain dissolved species  $(SO<sub>4</sub><sup>2</sup>, Cl<sub>1</sub>, HCO<sub>3</sub>)$  and  $O<sub>2</sub>$ . Oxidation of ferroan brucite may thus yield 71 Fe<sup>II</sup>/Fe<sup>III</sup> layered double hydroxides containing chlorine (iowaite; Klein et al. 2020) or  $CO<sub>2</sub>$ 72 (pyroaurite; Boschi et al. 2017) with or without simultaneous  $H_2$  production.

 In order to gain insight on the behavior of ferroan brucite when exposed to fluids in subsurface conditions relevant to ophiolite settings, ferroan brucite was synthesized and compared (composition, size, morphology) to natural ferroan brucite from the Oman ophiolite. Synthetic ferroan brucite was then reacted in the presence of water at temperatures close to 373 K, considered here as low temperatures. The characterization of the reaction products with X-ray diffraction, scanning electron  $\mu$ <sup>38</sup> microscopy, bulk Fe<sup>III</sup> determination by colorimetry, and thermogravimetric analysis allowed us to 79 propose phase relationships for ferroan brucite in the naturally relevant FeO-MgO-H<sub>2</sub>O+/-O<sub>2</sub> sub-system.

#### **2 Materials and Methods**

# **2.1 FeII -bearing brucite synthesis**

84 Ferroan brucite with  $x \sim 0.2$  was synthesized at ambient conditions based on a method used to synthesize aqueous  $Fe^{II}$  precipitates (Olowe and Génin 1991; Gilbert et al. 2008). Ferroan brucite was 86 precipitated from a stoichiometric solution of dissolved  $Fe^{II}$  and Mg salts, either sulphate 87 ( $MgSO_4$ , 7 $H_2O$  and  $FeSO_4$ , 7 $H_2O$ ) or chloride ( $MgCl_2$ , 6 $H_2O$  and  $FeCl_2$ , 4 $H_2O$ ). Precipitation occurred 88 after pouring the metal salt solution into a NaOH solution under stirring at  $\sim$  400 rpm. The composition of the mixture is characterized by its *R* ratio defined as  $R = \frac{[Fe^{2+}] + [Mg^{2+}]}{[Mg^{2+}]}$ 89 composition of the mixture is characterized by its R ratio defined as  $R = \frac{[Fe^{-}] + [Mg^{-}]}{[NaOH]}$ . Solutions of 90 100 mL with salt concentrations of 0.3 mol.L<sup>-1</sup> were mixed with 100 mL solutions with a NaOH 91 concentration of either 0.75 or 6 mol.L<sup>-1</sup>. This led to 200 mL solutions with  $R = 0.4$  and  $R = 0.05$ , respectively. In order to minimize the oxidation of  $Fe^{II}$ , ultrapure water (resistivity of 18.2 MΩ.cm) 93 was boiled under continuous  $N_2$  bubbling prior to all experiments.

 The precipitate was separated from the solution by ultra-centrifugation in an airtight bottle. The bottle was then opened in a glove box under an Ar atmosphere with a continuous measurement 96 of  $O_2$  level indicating concentration  $\langle 10 \text{ ppm} \rangle$ . The glove box was systematically used in the subsequent steps requiring an inert atmosphere. The precipitate was recovered and rinsed using two 98 different procedures: 1) vacuum enhanced filtration to collect the solid on a 0.8  $\mu$ m nitrocellulose 99 filter (AAWP filter), followed by washing three to four times with a total of  $\sim$  50 mL degassed ultrapure water without resuspending the solid fraction; and 2) repeated cycles of centrifugation, 101 supernatant removal, resuspension of the powder paste under manual stirring with  $\sim 150$  mL of degassed ultrapure water. Two to four cycles were needed to reach the point where the pH did not longer decrease (10.3 – 10.7 range). This second method was mainly used in the present study due to its convenience.

# 105 **2.2 Ferroan brucite reactivity experiments**

 A total of twenty experiments was carried out by reacting Fe-bearing brucite with an aqueous solution in two types of reactors (Table 1). Eighteen experiments were performed with synthetic ferroan brucite loaded with an aqueous solution (Table 1) into 45 mL PTFE-lined vessels (Parr  $4744^{\text{TM}}$ ). Five of these experiments (Runs #01 to #05, Table 1) were performed directly with the 110 ferroan brucite  $(-1)$  g) recovered after the first centrifugation stage (see the above-described procedure 2). In this case, the starting material was thus neither rinsed nor dried and was reacted 112 under pressure and temperature with the solution  $(25 \text{ g})$  from which this ferroan brucite precipitated (pH > 13). In all other experiments, the initial ferroan brucite used was rinsed according to one of the above-described protocols. The initial pH of the solution was measured for Runs #10, #19 and #20 and found to be close to 10 (i.e., close to the pH range measured for the last rinsing cycle, *see* previous section). The reactors were loaded and sealed in the glove box and Ar atmosphere. They were then placed in an oven regulated within 1 K. Reactivity of ferroan brucite was investigated at two temperatures: 378 and 403 K and at the water vapor pressure (0.12 and 0.27 MPa, respectively). Each experiment was stopped at a specific time ranging from 1 to 36 days (Table 1). Reactors were then opened in the glove box where the solid product was recovered. The final pH of the solution measured 121 for eleven runs (Runs  $#8-16, #19, and #20$ ) is  $9.4 +/- 0.5$ .

 Two additional experiments (#17 and #18 in Table 1) were performed by loading in the glove 123 box about 30 mg of ferroan brucite with 100  $\mu$ L of degassed ultrapure water in 2 – 3 cm long gold tubes (4.4 mm outer diameter and 4.0 mm inner diameter) welded shut at one end. The open end of the capsule was then squeezed and the capsule transferred outside the glove box for immediate welding. The Au capsule was then placed in a horizontal cold seal pressure vessel for reaction at 378 K under a water pressure of 20 MPa. The temperature was measured with a Ni-NiCr thermocouple and regulated within 1 K. At the end of the experiment, the vessel was cooled down under a compressed air stream (see Brunet and Chopin 1995 for experimental details).

### **2.3 Gas chromatography**

 H<sup>2</sup> gas contained in the sealed gold capsules (experiments # 17 and # 18) was recovered using the method described in Malvoisin et al. (2013). The recovered gas diluted in Ar was injected with a 250 µL gas-tight syringe in a Clarus 500 gas chromatograph (Perkin Elmer<sup>TM</sup>) equipped with a 134 polymer filled column (Restek ShinCarbon<sup>TM</sup>) and a thermal conductivity detector (TCD). Argon was 135 used as carrier gas. Each gas sample was analyzed at least three times consecutively.  $H_2$  detection 136 limit with the gas chromatograph setup was estimated to  $10 - 100$  ppm. A H<sub>2</sub> blank experiment was performed in a sealed gold capsule with 100 µL of degassed ultrapure water. After fifteen days at 378

 K and 20 MPa, no hydrogen was detected in the blank experiment. After gas chromatography analysis, the capsules were opened in the glove box where the solid was dried for several days in the Ar atmosphere before characterization.

# **2.4 X-ray diffraction (XRD) and Rietveld analysis**

 Run products were front-loaded as randomly oriented mounts in the glove box using an air- tight holder and analyzed by X-ray diffraction (XRD) with a Bruker D8 diffractometer. XRD patterns 144 were collected from 15 to 80° (2 $\theta$ ) using Cu*K*  $\alpha$  radiation and counting times of 3 s per 0.04° step. After identification of the different mineral phases, XRD patterns were analyzed using the Rietveld technique with the BGMN software (Doebelin and Kleeberg 2015). A non-exhaustive list of independently refined parameters includes: i) the proportions of the different phases present in the 148 samples: ferroan brucite  $[containing Fe<sup>II</sup>]$ , pyroaurite  $[a]$  Fe-containing layered double hydroxide (LDH) structure], magnetite, and ferrian brucite [containing  $Fe^{III}$ ]; ii) the unit-cell parameters of these phases; iii) the Mg:Fe ratios in ferroan and ferrian brucites if present at > 10 and >25 wt.%, respectively; iv) z-coordinate of the O atom 2d position in ferroan and ferrian brucites (space group  $P\overline{3}m1$ ) if present at >50 wt%; v) preferred orientation of the different phases using spherical harmonic functions if the phase content was sufficient (Doebelin and Kleeberg 2015); vi) size of the coherent scattering domains and strain in the different phases. In particular, the partial occupancy of the mixed (Fe,Mg) site refined in ferroan brucite was constrained both from the variation of the in-plane *a* unit-156 cell parameter between values reported for  $Mg(OH)_2$  (brucite – ICDD #44-1482) and Fe(OH)<sub>2</sub> (amakinite – ICSD #107289) end-members and from the influence of site mixed occupancy on the intensity distribution between *hkl* reflections. To our knowledge, no systematic study is available to confirm the validity of Vegard's law between these two end-members. The remarkably linear relationship existing between the in-plane dimension of brucite-like structures and the ionic radius of 161 the octahedral cation ( $R^2 = 0.996$  – Fig. S1) strongly supports the validity of the approach, however. Unit-cell *c* parameter was not included in the approach owing to the more erratic variation of this dimension with the ionic radius of the octahedral cation (Fig. S1). Intensity distribution between  reflections was used as an additional constraint to refine the partial occupancy of the mixed (Fe,Mg) site when proportion of ferroan brucite exceeded 10 wt.%. As no structure model was available for ferrian brucite, unit-cell parameters and Fe contents were refined independently when proportion of ferrian brucite exceeded 25 wt.% and charge compensation was hypothesized to originate either from the presence of octahedral vacancies or from the partial deprotonation of the layered structure as proposed by Genin et al. (2006a) for the octahedral layer of fully oxidized green rust. In the latter case, the partial occupancy of the mixed (Fe,Mg) site was refined using a split site and constraining a complete (Fe+Mg) site occupancy. In the former case, the Fe content was kept constant and similar to that in ferroan brucite (0.17 Fe per octahedral site) and only Mg site occupancy was refined to avoid refinement of cross-correlated parameters related to electron density at the octahedral cation position (overall site occupancy and Mg:Fe ratio).

#### **2.5 SEM imaging**

 Powders of the starting material and of the run products were mounted on double-sided carbon tape in the glove box under Ar atmosphere. They were then coated under vacuum with a 1 nm thick gold layer and characterized with a field emission gun scanning electron microscope (FEG-SEM; Zeiss Ultra 55) operated at 5 to 10 kV accelerating voltage.

# **2.6 Thermogravimetric analysis**

 Thermogravimetric analyses (TGA) were performed using a Mettler-Toledo TGA-DSC3+ instrument. Samples were loaded into 100 μL aluminum crucibles inside the glove box. The crucibles were mechanically sealed in the glove box using a manual press (Mettler-Toledo) and then brought to the instrument. The lid was pierced using a small needle just prior to the measurements to minimize atmosphere exposure. A thermal treatment consisting of a 5 min isotherm at 298.15 K and a 186 subsequent ramp from 298.15 to 873.15 K at 10 K/min was programmed, under a 50 mL/min N<sub>2</sub> flow. The gas produced by the sample during the TGA measurement was analyzed using an IS50 Fourier Transform Infrared (FTIR) spectrometer from Thermo Scientific. The gas was transferred from the outlet of the TGA instrument to the spectrometer using a heated transfer line (573 K). 40 scans were 190 acquired and averaged every 51 s. Absorbance spectra were measured from 4500 to 500 cm<sup>-1</sup>, with a 191  $4 \text{ cm}^{-1}$  resolution.

# 192 **2.7 Raman microspectroscopy**

 Value of *x* in the ferroan brucite was determined by Raman spectroscopy with a confocal Horiba LabRAM Soleil equipped with a 532 nm laser at ISTerre. The confocal aperture was set at 200 µm and the gratings at 600 groves/mm. Five duplicate spectra were acquired over the 3200-3800 196 cm<sup>-1</sup> range with a x100 objective. After subtracting the baseline, spectra were fitted with Lorentzian 197 functions to determine the position of the  $v_1$  O-H stretching band of ferroan brucite. This position was then used to calculate *x* using the linear relationship from Templeton and Ellison (2020).

# 199 **2.8 Ferric and ferrous iron quantification in the solid products**

200 For Runs #19 and 20, ferric and ferrous iron contents of the starting ferroan brucite and of its 201 hydrothermal reaction products were determined by colorimetric assay with a  $\sim$  3% precision. 202 Sample preparation for Fe quantification was performed in a glove box under an Ar atmosphere 203 containing 3 ppmv  $O_2$ . A mass of 103 mg of sample powder was dissolved into 4 mL of 3M HCl 204 according to the protocol proposed in Pan et al. (2020). The resulting solution was first diluted to 50 205 mL with ultrapure water (18.2 MΩ) and then diluted again 10 times in ultrapure water. A 1 mL aliquot 206 of this last solution was mixed with 1 mL of a pH-buffered solution ( $pH = 3.5$ ); then, 1 mL of ultrapure 207 degassed water and 1 mL of  $10^{-2}$  M O-phenanthroline were successively added for  $[Fe^{2+}]$ 208 quantification by spectrophotometric method (Herrera et al. 2007). Stability of aqueous  $Fe^{2+}$  in acidified solution (pH ~1) has been tested on 0.1 M  $\text{Fe}^{\text{II}}\text{Cl}_2$  solutions prepared outside the glove box, 210 with degassed water. No significant aqueous  $Fe^{2+}$  oxidation is expected in the time lapse (< 2 h) 211 between dissolution and iron complexation in a glove box with 3 ppmv  $O_2$ . The procedure described 212 above was repeated with 1 mL of hydroxylamine chloride instead of 1 mL of ultrapure degassed water 213 to obtain  $[Fe]_{total}$ ;  $[Fe^{3+}]$  was deduced from the difference between  $[Fe]_{total}$  and  $[Fe^{2+}]$ .

## **2.9 Comparison to a natural ferroan brucite from the Oman ophiolite**

 A ferroan brucite bearing sample was collected in the Wadi Tayin massif of the Samail Ophiolite during the Oman Drilling Project (sample BA4A-81-1-1-17; Kelemen et al. 2020). Sample mineralogical composition and microstructure are described in detail in Malvoisin et al. (2020, 2021). The sample consists of an extensively serpentinized dunite (serpentinization progress > 80%) containing olivine relicts surrounded by serpentine and ferroan brucite. Magnetite is rare. Malvoisin 220 et al. (2021) have shown that serpentine occurs as  $\sim 1$  µm wide lizardite columns perpendicular to the olivine surface. These columns are embedded in an aggregate of randomly oriented ferroan brucite grains (< 100 nm across). An *x* value of 0.2762 (95% confidence bounds of 0.2760 and 0.2765) was inferred by Malvoisin et al. (2020) for ferroan brucite composition based on the microprobe analyses of mixtures of lizardite columns and ferroan brucite grains.

#### **3 Results**

# **3.1 Characterization of synthetic ferroan brucite**

 The synthesis protocol led to ferroan brucite production as a single crystalline phase as shown by powder XRD (Fig. 1). The same results were obtained whether chloride of sulfate iron salt was used, and whether the solid products were recovered by vacuum enhanced filtration or centrifugation. 231 Two peaks were identified in the  $3200-3800$  cm<sup>-1</sup> range with Raman spectroscopy on sample FeBR\_R0.4\_Cl\_11 (also used as starting material for Run #20; Fig. S2A): the broad peak at  $\sim$  3586 cm<sup>-1</sup> was attributed to ferroan brucite oxidation in air during measurement, whereas the sharp 234 peak at  $\sim$  3641 cm<sup>-1</sup> was attributed to the  $v_1$  O-H stretching band of ferroan brucite. Using the 235 relationship of Templeton and Ellison (2020), the position of this  $v_1$  O-H stretching band indicates a *x* value of 0.17  $\pm$  0.05. Based on Vegard's law, refined unit-cell parameters confirmed the  $x \sim 0.2$  composition (Tables S1, S2) that allows also reproducing the experimental distribution of intensities between the different *hkl* reflections. The FWHM of ferroan brucite diffraction peaks are similar for all synthetic samples and indicative of a 20 - 40 nm crystal size within the **ab** plane (Table 1). The 240 crystal size inferred from XRD data is close to the size of synthetic ferroan brucite platelets (50 - 100 241 nm across with homogeneous size distribution) observed with SEM (Fig. 2A and 2B). In this ferroan 242 brucite, calculated (Mg,Fe)-O bond lengths ( $\sim$  2.13 Å – Table S2) are consistent with the prevalence 243 of divalent cations in the structure. Bond valence calculated with the Valence program (Brown and 244 Altermatt 1985; Brown 2009) and bond-valence parameters from Gagné and Hawthorne (2015) 245 indicate that  $Fe^{II}$  atoms would receive 0.348 v.u. from each of its 6 surrounding O atoms. This ensures 246 an almost ideal charge compensation (2.088 v.u.), whereas  $Mg<sup>II</sup>$  atoms would receive 0.308 v.u. from 247 each of the 6 surrounding O atoms. By contrast, bond valence calculated for  $Fe^{III}$  cations and a similar 248 Fe-O bond length indicates that these cations would receive only 0.364 v.u. from surrounding O 249 atoms, thus resulting in their strong undersaturation (2.184 v.u.). These charge compensation 250 calculations support the prevalence of  $Fe^{II}$  over  $Fe^{III}$  in ferroan brucite.

251 Bulk Fe<sup>III</sup> content has been determined experimentally for the two synthetic ferroan brucite 252 used as initial material in Runs #20 and #19 (Fig. S3). In sample #20, which was prepared using the same protocol as all other syntheses,  $Fe^{III}/Fe_{tot}$  amounts to 0.08(1). Sample #19 was aged in the glove 254 box until the product was covered with a thin pale reddish layer indicative of oxidation. In this extreme case,  $Fe^{III}/Fe_{tot}$  reaches 0.17(1) (Fig. S3). In both cases, these experimentally determined 256 proportions of  $Fe^{II}$  and  $Fe^{III}$  further support the prevalence of  $Fe^{II}$  over  $Fe^{III}$  in ferroan brucite.

# 257 **3.2 Identification and quantification of the products of ferroan brucite reaction in aqueous**  258 **media at T**  $\leq 403$  **K**

259 At 378 and 403 K, in PTFE-lined reactors, ferroan brucite was found to react significantly. 260 Indeed, after one week of experiment,  $20 - 30$  wt.% of ferroan brucite have reacted at both 261 temperatures (Table 1). For a duration of about a month, up to  $80 - 90$  wt.% of ferroan brucite has 262 reacted at the two temperatures (Table 1). The two experiments performed in gold capsules yielded 263 strikingly different results, ferroan brucite having barely reacted even after 26 d at 378 K (Table 1). 264 In this case, only two reaction products were identified, magnetite  $[3.2(2) - 3.9(3)$  wt.%] and  pyroaurite [0.4(3) – 5.4(19) wt.%], a ferromagnesian LDH with interlayer water and carbonate anions 266 (Allmann 1968), nominally Fe<sub>2</sub>Mg<sub>6</sub>(OH)<sub>16</sub>(CO<sub>3</sub>) $\cdot$ 4.5H<sub>2</sub>O.

 The ferric iron content of the reaction products from PTFE-lined reactors has been experimentally determined for Experiments #19 and #20 which were specifically designed to quantify the oxidation of iron in the course of the ferroan brucite reaction. The starting material of Run #19 270 was purposely oxidized leading to a  $Fe^{III}/Fe_{tot}$  ratio of 0.17(1) (Fig. S3). This ratio increased to 0.92(1) after hydrothermal treatment for 32 days at 378 K (Run #19). Like for all other experiments, the 272 starting material of Run #20 [Fe<sup>III</sup>/Fe<sub>tot</sub> ratio of 0.08(1)] was prepared to avoid as much as possible 273 oxygen contamination. After hydrothermal treatment for 32 days at 378 K (Run #20) a  $Fe^{III}/Fe_{tot}$  ratio of 0.87(5) was measured in the reaction product (Fig. S3). Both experiments indicate that Fe is mainly 275 present as  $Fe^{III}$  in reaction products of ferroan brucite.

 Refinement of unit-cell parameters of ferroan brucite remaining in reaction products indicates 277 that its Fe content  $(x)$  after reaction is similar to that of the starting material  $(0.2)$ . Magnetite was 278 found in almost all run products  $(0.9 - 4.1 \text{ wt.})$ , even in experiments having lasted less than a week (Table 1). Pyroaurite was identified by XRD in all experiments but in proportions close to the 280 detection limit ( $\sim 0.2 - 0.3$  wt.%) for Runs #04, #05 and #18 (Table 1). In all other runs, quantitative 281 phase analysis yielded pyroaurite proportions of  $\sim$  5 to  $\sim$  30 wt.% depending on run duration and water-to-rock ratio. Another layered phase was present whose peak positions are similar to those of the initial ferroan brucite, although slightly shifted towards higher angles (Fig. 3B). This phase was assumed to be isostructural to ferroan brucite but with shorter unit-cell parameters, most likely as a 285 consequence of  $Fe^{II}$  oxidation shown by the initial quick formation of pyroaurite, and will hereafter be referred to as ferrian brucite. Progressive replacement of ferroan brucite by ferrian brucite is illustrated on Fig. 3A where the time evolution of the XRD pattern of the run product is displayed. Accordingly, a satisfactory fit to the data was obtained assuming a contribution from this ferrian brucite structure (Fig. S4). SEM images (Fig. 2C) showed that ferrian brucite displayed the same habitus as starting ferroan brucite (Fig. 2A and 2B) with platelets of larger size however (~ 400 nm).

# 291 **3.3 Crystal chemistry of ferrian brucite**

292 For Run #03, in which ferrian brucite accounts for  $\sim$  75% of the reaction products, its unit-293 cell parameters and atomic positions were refined to further constrain its crystal chemistry, and more 294 especially its Fe/Mg ratio and Fe valence. Refined unit-cell parameters  $(a = 3.1255(5)$  Å,  $c =$ 295 4.6774(13) Å; space group  $\overline{P3}m1$  – Tables S1, S3) suggest the presence of ~ 15% Fe<sup>III</sup> in the ferrian 296 structure using brucite and fully oxidized green rust ( $Fe^{III}$ <sub>6</sub>O<sub>12</sub>H<sub>8</sub>CO<sub>3</sub>) as end members for Vegard's 297 law ( $a = 3.1442 \text{ Å} - \text{ICDD}$  #44-1482 – and  $a = 3.01 \text{ Å} - \text{Génin}$  et al. 2006a – respectively). Validity 298 of Vegard's law between these two end-members is supported by the extension of the linear regression 299 between the in-plane *a* dimension of brucite-like structures and the ionic radius of the octahedral 300 cations to include Fe<sup>III</sup> ( $R^2 = 0.994 - Fig. S5$ ). Validity of Vegard's law for the in-plane *a* parameter 301 of mixed (Fe<sup>III</sup>,Mg<sup>II</sup>) octahedral layers is further supported by the consistency between calculated and experimentally measured *a* unit-cell parameters of  $(Fe^{III}, Mg^{II})$ -LDHs of similar layer composition. 303 The *a* parameter calculated by Elmoubarki et al. (2017) for a LDH [Fe<sup>III</sup><sub>0.27</sub>Mg<sup>II</sup><sub>0.73</sub>(OH)<sub>2</sub> – 3.108 Å] 304 is indeed equivalent to their experimentally determined value of 3.11 Å, and similar to the 3.109 Å *a* 305 unit-cell parameter of pyroaurite ( $Fe^{III}_{0.25}Mg^{II}_{0.75}(OH)_{2}$  – ICDD #1-70-2150). In addition, the Fe 306 content refined independently for ferrian brucite from intensity distribution of its *hkl* reflections is  $307 \sim 0.17$ , a content similar to that of the initial brucite suggesting that all / most of ferroan brucite initial  $F e^{II}$  was oxidized to Fe<sup>III</sup>. The complete oxidation of Fe in ferrian brucite is supported further by the consistency of  $Fe^{III}/Fe_{tot}$  ratios determined experimentally and calculated from quantitative phase 310 analysis for Runs #19 and #20 (Fig. S3 and Table S4, respectively). In addition, evolution of layer O 311 atomic coordinate (Table S3) and of in-plane unit-cell parameters in ferrian brucite compared to 312 ferroan brucite led to a significant shortening of the (Mg,Fe)-O bond length from  $\sim$  2.13 Å in the 313 initial ferroan brucite to  $\sim$  2.08 Å in ferrian brucite. The resulting increase in the Fe-O bond valence 314 calculated for Fe<sup>III</sup>-O in ferrian brucite (0.418 v.u.) compared to Fe<sup>II</sup>-O in ferroan brucite (0.348 v.u.) 315 is consistent with the sole presence of  $Fe^{III}$  in ferrian brucite ( $Fe^{III}$  receives 2.508 v.u. from the 6

316 surrounding O atoms), especially as Mg remains the dominant cation  $(\sim 80\%)$  in ferrian brucite, thus preventing shortening further the average (Mg,Fe)-O bond length.

In this model, compensation of the increased positive charge induced by  $Fe^{II}$  oxidation was assumed to be achieved by partial deprotonation of the structure, as proposed by Genin et al. (2006a) 320 for oxidized green rust, leading to a  $(Fe^{III}vMg_{1-v})(OH_{(1-v/2)})$  structural formula. Another alternative for charge compensation is the creation of Mg octahedral vacancies. This alternative structure model 322 was assessed for ferrian brucite by refining the partial occupancy of a mixed  $[Fe_{0.17}Mg_{w}]$  octahedral 323 site for Run #03. The refined  $[Fe_{0.17}Mg_{0.80(2)}]$  average cationic composition of this site is ~ 1.0 and supports the absence of octahedral vacancies. This alternative model was thus rejected and it was concluded that deprotonation charge-compensates  $Fe^{II}$  oxidation in the initial ferroan brucite.

#### **3.4 Thermogravimetric analysis of ferroan brucite and ferrian brucite rich samples**

 Evolution of sample mass as a function of temperature measured by TGA and its derivative are displayed in Fig. 4 for ferroan brucite (synthesized from chloride salts) and for Runs #09 and #15 which both contained over 30 wt.% ferrian brucite (Table 1). Ferroan brucite exhibits two mass loss events. The first one occurred below 461 K (Fig. 4A) which is interpreted as departure of physisorbed water (6.2 wt.%), whereas a second mass loss of much higher amplitude occurred between 500 and 700 K and is interpreted as dehydroxylation of ferroan brucite (Reaction 2):

333 
$$
(Mg, Fe)(OH)_2 = (Mg, Fe)O + H_2O \t(2)
$$

 This temperature range of dehydroxylation is consistent with thermogravimetric data on 335 synthetic brucite,  $Mg(OH)_2$ , which was found to dehydroxylate in the 550 – 700 K range (Turner et al. 1963; Klein et al. 2020).

 In comparison, TGA analysis of reaction products shows a more limited mass loss (2.9 wt.%) due to physisorbed water that may be related to the larger grain size (smaller surface area). An 339 additional mass loss (2.3 wt.%) is observed from  $461 - 505$  K (Fig. 4B and 4C). It is most likely 340 related to the dehydration of pyroaurite interlayers that contain  $H_2O$  in addition to  $CO_3^{2}$  anions.  Indeed, based on 4.5 H2O per formula unit, pyroaurite structural water represents 2.9 wt.% of the total TGA weight loss (Run #15, calculated with 24.3 wt.% pyroaurite as given by Rietveld refinement). In the reaction products, the main mass loss event was found to shift towards higher temperature when the ferrian brucite content in the sample increased, from 660 K for the ferroan brucite starting material up to 692 K for Run #15 (Fig. 4D). This event is expected to include the dehydroxylation of both ferrian brucite / pyroaurite and of residual ferroan brucite. Dehydroxylation of pyroaurite and ferrian brucite are expected to occur in the same temperature range since they have identical 348 octahedral layer composition. Coupled infrared spectroscopy indicated that  $CO<sub>2</sub>$  from pyroaurite was also mostly released over this temperature range. The increase in the temperature of the main mass loss event with respect to single-phase ferroan brucite could be related either to a grain size effect 351 with ferrian brucite and pyroaurite having larger grain size than starting  $(Mg_{0.8}Fe_{0.2})(OH)_2$  and/or to the valence modification in the octahedral layer due to the presence of trivalent Fe.

#### **3.5 Natural ferroan brucite from Oman**

 Powder diffraction patterns and Raman spectroscopy of natural serpentinite sample show the presence of ferroan brucite and serpentine (Fig. 1B and S2B – Wadi Tayin massif, Samail ophiolite). Ferrian brucite was not detected. The comparison between the powder diffraction patterns of the synthetic product and that of ferroan brucite from the natural serpentinite sample shows that the lattice parameters are the same and that diffraction peak widths are similar, indicative of crystallite sizes in 359 the order of 30 to 100 nm in the **ab** plane. Raman spectroscopy in the  $3200-3800$  cm<sup>-1</sup> range on the natural sample reveals peaks similar to those observed for synthetic ferroan brucite but slightly shifted 361 at ~ 3594 cm<sup>-1</sup> for the broad peak and at ~ 3632 cm<sup>-1</sup> for the sharp peak ( $v_1$  O-H stretching band; Fig. 362 S2B). Using the relationship of Templeton and Ellison (2020), the position of this  $v_1$  O-H stretching 363 band indicates a x value of  $0.287 \pm 0.03$ . This latter value is consistent with results from electron 364 microprobe analysis on the same sample yielding  $x = 0.276$  (Malvoisin et al. 2020). SEM characterization of both sample types confirmed the grain size derived from XRD data analysis.

#### **4 Discussion**

# **4.1 Magnetite and H<sup>2</sup> formation**

 When reacted in gold capsules that are known to be impermeable to H<sup>2</sup> below 623 K (Chou 1986), synthetic ferroan brucite only barely reacted and the identified run products were magnetite  $(3.2(2) - 3.9(3)$  wt.% – Table 1), pyroaurite, and H<sub>2</sub>. The amount of H<sub>2</sub> gas produced during Runs #17 372 and #18 ranged from  $2.87 \pm 0.46$  to  $8.49 \pm 1.5$  nanomoles leading to [H<sub>2</sub>,aq] comprised between 28.7  $\pm$  4.6 and 84.9  $\pm$  15 µmol/L at 20 MPa and 378 K. This amount of H<sub>2</sub> recovered is three orders of magnitude lower than expected if all the magnetite in the run products would have formed from ferroan brucite oxidation according to the following equation:

376 
$$
[Fe^{2+}]^{brucite} + H_2O = Fe^{3+} + OH^- + \frac{1}{2}H_2
$$
 (3)

Based on the magnetite content of Runs  $#19$  and  $#20$ , for which the Fe<sup>III</sup> content of the starting ferroan-brucite material was analyzed, it can thus be concluded that magnetite mainly derived from 379 trivalent iron present in the starting material  $\sim 10\%$  of Fe<sub>tot</sub>).

# **4.2 Ferroan brucite oxidation to ferrian brucite and pyroaurite**

The reaction of ferroan brucite in PTFE reactors mostly involved  $Fe^{II}$  oxidation to  $Fe^{III}$  and the formation of ferrian brucite. As for the above experiments in sealed gold capsules (Runs #17 and 383 #18),  $\sim$  3 - 4 wt.% of magnetite has formed, most likely from Fe<sup>III</sup> present in the starting material (and  $\Omega_2$  contamination). This Fe<sup>III</sup> did not form hematite that could have been produced if more oxidizing conditions had prevailed in the experimental setup. Similarly, lepidocrocite or goethite that are easily formed in air from Fe(OH)<sup>2</sup> (Olowe and Génin 1991; Gilbert et al. 2008) were not detected.

 The formation of ferrian brucite in PTFE reactor and its absence in experiments performed in gold capsules at the same temperature, duration and absence of stirring, can be interpreted as reflecting different RedOx conditions in the two setups. Whereas gold capsules are not permeable to  $\text{H}_2$  at the temperatures of the present experiments (378 – 403 K), PTFE reactors with a PTFE seal are known to be more permeable to gases, and even to store gases in the PTFE macro-porosity (Vacher 392 et al. 2019). In PTFE reactors where significant outward  $H_2$  diffusion and/or inward  $O_2$  diffusion cannot be avoided, RedOx conditions occurred to be favorable to the oxidation of  $Fe<sup>H</sup>$  contained in ferroan brucite layer to form ferrian brucite.

 At 378 K, the ferroan brucite transformation to ferrian brucite seemed to follow zero-order kinetics irrespective of the reaction medium, i.e., ultrapure degassed water or ferroan brucite synthesis solution (Fig. 5). Magnetite and pyroaurite formed before ferrian brucite in the early stage of the experiments in both aqueous media. Departure from zero-order kinetics of the ferroan-to-ferrian brucite transformation in the first 3 days of experiments may thus be interpreted as the result of rapid pyroaurite (and possibly magnetite) formation. This early transformation of ferroan brucite can be considered as fast since it proceeded at the day scale at temperatures relevant to subsurface conditions.

 The amount of pyroaurite product appears to be proportional to the water-to-rock ratio 403 indicating that the main source of  $CO<sub>2</sub>$  is likely the  $CO<sub>2</sub>$  dissolved in the added solution (Table 1). Indeed, CO<sup>2</sup> is highly soluble at elevated pH in NaOH solutions (Yoo et al. 2013 and references 405 therein). This strong partitioning of  $CO<sub>2</sub>$  into pyroaurite confirms the potential of this mineral as efficient CO<sup>2</sup> sink in rocks or mine tailing containing Fe-brucite (e.g., Assima et al. 2014; Boschi et al. 2017; Turvey et al. 2018). The low concentration (~ 2 wt.%) or even the absence of pyroaurite in 408 experiments performed in sealed gold-capsule where the highest  $H_2$  pressure has been attained might result from a combination of low water-to-rock ratio and of reducing conditions that hindered or 410 prevented the oxidation of  $Fe^{II}$  to  $Fe^{III}$  in ferroan brucite and the associated formation of pyroaurite 411 (Fe<sup>III</sup>,Mg)(OH)<sub>2</sub> octahedral layer.

#### **4.3 Transformation mechanisms of ferroan brucite into ferrian brucite**

 The similarity between initial ferroan brucite and ferrian brucite product in terms of constitutive crystallite sizes, suggests that changes affecting the octahedral layer remained limited to  $F^{\text{H}}$  oxidation and to the induced partial deprotonation to compensate for the increased cationic charge. This similarity and similar Fe/Mg ratios determined in ferroan and ferrian brucites both indicate an isomorphic oxidation process. Rietveld refinement of ferrian brucite indicated little or no

octahedral vacancies, thus supporting deprotonation of the hydroxyl groups (Fe<sup>2+</sup>+ OH<sup>-</sup> = Fe<sup>3+</sup> + O<sup>2-</sup> 418 419 ) as the mechanism balancing the charge resulting from  $Fe^{II}$  oxidation in brucite octahedral layers.

420 Based on the phase proportions and their estimated standard deviations (esd) derived from 421 Rietveld refinement and considering the following nominal compositions,  $(Mg_{0.81}Fe^{II}_{0.19})(OH)_2$ , 422 (Mg<sub>0.83</sub>Fe<sup>III</sup><sub>0.17</sub>)O<sub>0.17</sub>(OH)<sub>1.83</sub> and Mg<sub>6</sub>Fe<sup>III</sup><sub>2</sub>(CO<sub>3</sub>)(OH)<sub>16</sub>.4.5H<sub>2</sub>O for ferroan brucite, ferrian brucite 423 and pyroaurite, respectively, a theoretical total mass loss  $(H_2O \text{ and } CO_2)$  of 28.9(8) wt.% was 424 calculated for Run #15. This prediction agrees well with the experimental total mass loss of Run #15 425 which amounts to 27.2(2) wt.% after subtraction of the contribution of physisorbed water. For 426 comparison, the alternative model which considers a ferrian brucite composition with octahedral 427 vacancies,  $(Mg_{0.76}\square_{0.08}Fe^{III}{}_{0.16})(OH)_2$ , would lead to a total mass loss of 30.6(8) wt.%. TGA data thus 428 support further the deprotonation model to charge balance the presence of  $Fe^{III}$  in the octahedral sheets 429 of ferrian brucite consistent with the Rietveld refinement of XRD data. The equation to describe the 430 oxidation of ferroan brucite is thus most likely:

431 
$$
(Mg_{0.8}, Fe^{II}_{0.2})(OH)_2 \Rightarrow (Mg_{0.8}, Fe^{III}_{0.2})O_{0.2}(OH)_{1.8} + 0.1 H_2
$$
 (4)

432 In the same chemical system, fougerite which belongs to the green rust mineral group also 433 possesses a structure based on brucite-like octahedral sheets with interlayer water molecules and 434 anion(s). The structural formula of fougerite is  $[Fe^{II}]_{1}$ -z $Fe^{III}]_{z}Mg_{y}(OH)_{2+2y}]^{+z}[z/nA^{-n}.mH_{2}O]^{-z}$  where *A* 435 is the interlayer anion (OH<sup>-</sup>, Cl<sup>-</sup>, CO<sub>3</sub><sup>2-</sup>, SO<sub>4</sub><sup>2</sup><sup>-</sup>) and *n* its valency (Trolard et al. 2007). The charge 436 excess of the octahedral sheet is compensated for by the presence of interlayer anions. Génin et al. 437 (2006b) consistently showed that the oxidation of synthetic  $(CO<sub>3</sub><sup>2</sup>)$  green rust can be achieved 438 following the general substitution scheme  $Fe^{II}_{6(1-z)}Fe^{III}_{6z}O_{12}H_{2(7-3z)}CO_3$  which involves charge 439 compensation by progressive deprotonation.

440

#### 441 **5 Implications**

# 442 **5.1 Ferrian brucite stability in the FeO-MgO-H2O+/-O<sup>2</sup> system**

443 The oxidation of Fe(OH)<sub>2</sub> in air (high oxygen fugacity;  $fO_2$ ) produces goethite, lepidocrocite, 444 or hematite ( $\alpha$ -FeOOH,  $\gamma$ -FeOOH, and  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub>, respectively; Gilbert et al. 2008). The experiments 445 in gold capsules performed at 378 K confirmed that under low  $fO_2$  conditions,  $H_2$  is produced during 446 ferroan brucite oxidation. Under these conditions, the only oxidized reaction product was magnetite, 447 suggesting that reaction (1) led to  $H_2$  production, even though the presence of trivalent iron in the 448 starting material also significantly contributed to magnetite formation (Ellison et al. 2021; Mayhew 449 et al. 2013; Miller et al. 2017). In the PTFE reactors, ferrian brucite was formed and the *f*O<sub>2</sub> was thus 450 intermediate between that of sealed gold capsules and air (intermediate  $fO_2$ ). It cannot be concluded 451 at this stage whether ferrian brucite was a stable or a metastable phase. It can however be deduced 452 from its coexistence with magnetite observed in PTFE experiments that its stability/metastability field 453 should fall in a  $fO_2$  range comprised between the stability fields of ferroan brucite and of hematite. 454 To confirm this statement, the thermodynamic properties of ferrian brucite,  $(Mg_{1-x}, Fe^{III}_x)O_x(OH)_{2-x}$ , 455 were computed from a linear combination of the thermodynamic properties of goethite and brucite 456 with the slop16.dat database (Fig. 6). Obviously, such an approximation is fraught with uncertainty. 457 The effect of changing the Gibbs energy of formation ( $\Delta G^{\circ}$ ) of ferrian brucite in the calculation by 458  $\pm$  10 kJ/mol was thus considered. Within that range of  $\Delta G^{\circ}$ <sub>f</sub>, the topology remains unchanged and 459 ferrian brucite is always found to occur at *fO<sup>2</sup>* comprised between those of ferroan brucite and 460 hematite stability fields (Fig. 6). However, the uncertainty on the thermodynamic parameters does 461 not allow to determine if  $O_2$  or  $H_2$  is the dominant gas species in the stability field of ferrian brucite 462 (Fig. 6). It is thus still unclear whether ferrian brucite formed in PTFE-lined reactors at the expense 463 of ferroan brucite by consuming  $O_2$  or by producing H<sub>2</sub>, according to one of the following reactions:

464 
$$
(Mg_{0.8},Fe^{II}_{0.2})(OH)_2 + 0.05 O_2 = (Mg_{0.8},Fe^{III}_{0.2})O_{0.2}(OH)_{1.8} + 0.1 H_2O
$$
 (5)

465 or

$$
466 \qquad (Mg_{0.8},Fe^{II}_{0.2})(OH)_2 = (Mg_{0.8},Fe^{III}_{0.2})O_{0.2}(OH)_{1.8} + 0.1 H_2 \qquad (6)
$$

467 One should note that Tosca et al. (2008) observed  $H_2$  production during Fe(OH)<sub>2</sub> conversion into 468 green rust-CO<sub>3</sub>, which, as shown above, shares crystallographic properties with ferrian brucite. 469 Additional experiments in the FeO-MgO-H<sub>2</sub>O+/-O<sub>2</sub> system are still needed to constrain the exact 470 range of  $fQ_2$ -T conditions under which ferrian brucite may be expected to occur in nature.

## 471 **5.2 Ferroan brucite oxidation kinetics**

472 Mineral replacement reactions generally proceed through dissolution and precipitation which are 473 mineral-surface dependent leading to non-constant replacement rates (Putnis 2002; Malvoisin et al. 474 2012). The conversion from ferroan to ferrian brucite appeared here to follow zero-order kinetics, 475 indicating that reaction rate is not controlled by this common dissolution-precipitation process. The 476 fact that ferrian brucite is likely stable at relatively low  $H_2$  partial pressure (Fig. 6) implies that 477 Reaction (6) cannot reach large extent in closed system. H<sub>2</sub> partial pressure should indeed remain low 478 to maintain the system in the stability field of ferrian brucite. Large reaction extents as those observed 479 here (e.g.,  $> 75\%$ ) would thus require extraction of at least part of the H<sub>2</sub> produced according to 480 Reaction (6). As a result, ferroan to ferrian brucite conversion was likely controlled by the rate of  $H_2$ 481 permeation through the PTFE reactor. This latter rate is expected to be constant (and the reaction 482 kinetics of zero order) if  $H_2$  permeates into an infinite gas reservoir, which is a reasonable 483 approximation for the room in which the experiments were conducted. A symmetrical scenario 484 involving atmospheric  $O_2$  permeation into the reactor would yield similar results and cannot be ruled 485 out at this stage to account for ferrian brucite formation.

 This being said, ferroan brucite oxidation into ferrian brucite and/or pyroaurite revealed to be remarkably fast even at temperatures as low as 378 K. Indeed, about half of the starting ferroan brucite converted into ferrian brucite after 15 days and more than 90% reacted after 36 days (Table 1). Ferrian brucite and pyroaurite (like other LDH containing different anions) are based on the same structural arrangement composed of brucite-like octahedral layers. They actually differ only in the way 491 octahedral Fe<sup>III</sup> is charge balanced: incorporation of an interlayer anion  $(CO<sub>3</sub><sup>2</sup>, Cl<sub>1</sub>, SO<sub>4</sub><sup>2</sup>)$  group or partial deprotonation of the brucite-like layer, respectively. The fact that these two charge-balance  mechanisms do not involve recrystallization of the octahedral layer might explain why they are effective at a temperature as low as 378 K and on a day – week timescale (Fig. 5).

495 Although ferrian brucite may well no be a stable phase in the FeO-MgO-H<sub>2</sub>O+/-O<sub>2</sub> system, the relatively fast transformation of ferroan into ferrian brucite makes the latter a likely metastable state in the ferroan brucite reaction process into Fe(III)-bearing oxides/hydroxides according to Ostwald's rule of stages. It must be noted that deprotonation coupled to iron oxidation in brucite layers is also relevant to clay minerals such as smectite (Drits and Manceau 2000; Manceau et al. 2000). Interestingly, this process was found to occur in soils at a relative short timescale of several months.

# **5.3 Why ferrian brucite has never been reported in ophiolites?**

 The reddish color and chemical analyses of brucite in some natural samples indicate ferroan brucite oxidation (Beard and Hopkinson 2000; Beard and Frost 2016; Ellison et al. 2021). However, the presence of ferrian brucite was not confirmed by mineralogical analysis and ferric (oxyhydr)oxides could lead to the same characteristics. The ubiquitous presence of anions in natural fluids (e.g., seawater, meteoric waters) likely favors the formation of green rust group minerals over that of ferrian brucite. In addition to pyroaurite discussed above, iowaite  $(Mg_6Fe^{III}_2Cl_2(OH)_{16.}4H_2O;$  Kohls and Rodda 1967) is another LDH reported in serpentinized peridotites (Heling and Schwarz 1992; Gibson et al. 1996; Bach et al. 2004; D'Antonio and Kristensen 2004; Sharp and Barnes 2004; Moll et al. 2007; Bonifacie et al. 2008; Kodolányi and Pettke 2011; Kodolányi et al. 2012; Albers et al. 2020). It occurs in samples collected at mid-ocean ridges, on passive margins and in ophiolites where it is generally associated at the submicrometer scale with ferroan brucite (Klein et al. 2020). Heling and Schwarz (1992) proposed that iowaite forms from brucite with iron oxidation charge-515 balanced by interlayer Cl<sup>-</sup>. This reaction is thought to occur under the oxidizing conditions associated to weathering at low temperature (Bach et al. 2004). However, methane was reported in seamounts where iowaite was found (Heling and Schwarz 1992), suggesting that iowaite formation, similarly to ferrian brucite formation in the experiments reported here, does not necessarily involve oxidizing  conditions. Similarly, Génin et al. (2006b) and Ruby et al. (2010) determined Eh-pH diagrams in 520 which naturally occurring green rust group minerals (mixed valence  $Fe^{II}$ ,  $Fe^{III}$  LDHs) are stable in the same field as molecular hydrogen.

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## **CRediT authorship contribution statement**

 **William Carlin:** Methodology, Investigation, Data Curation, Writing – Original Draft, Visualization. **Benjamin Malvoisin:** Conceptualization, Formal analysis, Writing – Original Draft, Writing – Review & Editing, Supervision, Visualization. **Bruno Lanson:** Methodology, Software, Investigation, Writing – Review & Editing, Visualization. **Fabrice Brunet:** Conceptualization, Formal analysis, Writing – Original Draft, Writing – Review & Editing, Supervision. **Nathaniel Findling:** Methodology, Software. **Martine Lanson:** Methodology, Investigation. **Valérie Magnin:** Investigation. **Tiphaine Fargetton:** Review and Supervision. **Laurent Jeannin:** Review and Supervision. **Olivier Lhote:** Project administration.

## **Declaration of Competing Interest**

 The authors declare no known competing financial interests or personal relationships that could have appeared to influence the work reported in this article.

## **Data availability**

The data presented in this study are available on request from the corresponding author.

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**Figure captions**

**Fig. 1.** X-ray diffraction patterns of ferroan brucite (CuK $\alpha$  radiation). (A) Synthetic product obtained by precipitation of chloride salts. (B) Natural sample from the Oman ophiolite (B). The main Bragg's reflexions of ferroan brucite are marked with vertical dashed lines. S: serpentine minerals.

 **Fig. 2.** Back-scattered electron micrographs of the starting material and reaction products. A and B: 772 Starting material where ferroan brucite occurs as  $\sim$  50 to 100 nm wide platelets. C: Reaction 773 product from PTFE reactor (Run  $# 15$ ) showing  $\sim 400$  nm wide platelets composed of the aggregation of smaller crystallites. (D) Nanometric euhedral magnetite precipitating at the surface of platelets (Run #15). mag: magnetite.

 **Fig. 3.** X-ray diffraction patterns (Cu*Kα*) of ferroan brucite reaction products (PTFE reactors) displayed from bottom to top with increasing run duration. A: Full XRD patterns with labeled phases; 778 B: Enlargement of  $[36 - 40^\circ]$  2-theta region to emphasize the shift of the (101) reflexion of ferroan brucite as the result of iron oxidation. Bragg's reflexions of ferroan and ferrian brucites are marked with vertical dashed lines and vertical long-dashed lines, respectively. Phase names as in Table 1. From bottom to top, XRD patterns correspond to ferroan brucite starting material followed by the powder XRD of Runs #06 to #10 (Table 1).

 **Fig. 4.** Thermogravimetric analysis of the ferroan brucite starting material and of two ferrian brucite rich samples. (A) Synthetic ferroan brucite weight loss during thermogravimetric analysis (solid line). From ambient to 461 K, physisorbed water is mainly released. (B) Ferrian brucite rich sample (Run #15) weight loss during thermogravimetric analysis (dotted-dashed line). Weight loss between 461 and 505 K could be attributed to pyroaurite structural (interlayer) water loss. (C) Comparison of TGA data for starting material (solid line) and reaction products from Runs #09 (dashed line) and #15 (dotted-dashed line). (D) Weight loss first derivative (smoothed with sliding mean method) for

 starting material (solid line) and reaction products from Runs #09 (dashed line) and #15 (dotted- dashed line). Heating rate: 10 K/min. For C and D, light grey zones indicate the temperature ranges 792 where evolved  $CO_2$  has been detected. TGA data up to 1273 K have been collected on Run #15 and no significant mass loss was observed above 873 K.

 **Fig. 5.** Time evolution of phase proportions at 378 K as determined using quantitative phase analysis on the reaction products. Black lines: Runs #06 to #10 (ferroan brucite synthesized from Cl-solutions and reacted with ultrapure degassed water); Grey lines: Runs #01 to #03 (ferroan brucite synthesized 797 with  $SO_4$ -solution and reacted in the synthesis solution). Abbreviations: Fe<sup>II</sup>-brc: ferroan brucite; pyr: 798 - pyroaurite; mag: magnetite;  $Fe^{III}$ -brc: ferrian brucite.

**Fig. 6.** Eh-pH Pourbaix diagram of iron phases in a Mg-bearing aqueous system ( $a_{Mg^{2+}} = 10^{-3}$  mol/L) 800 at 378 K. The stability fields of ferroan and ferrian brucite are displayed for  $x = 0.2$  by considering ideal solid solutions. Computations were performed with the slop16.dat database [\(https://gitlab.com/ENKI-portal/geopig/-/blob/master/slop/slop16.dat\)](https://gitlab.com/ENKI-portal/geopig/-/blob/master/slop/slop16.dat) and the properties for Fe(OH)<sup>2</sup> given in Klein et al. (2013). Diagrams were computed by excluding ferrian brucite (solid line), using a solid solution computed from goethite and brucite thermodynamic properties (dotted line), and for Gibbs energy of formation 10 kJ/mol below (dashed line) and above (dashed-dotted line) this latter solid solution.

# **Highlights**

- Reaction of synthetic ferroan brucite, a serpentinization product, at temperatures below 403 K
- Ferrian brucite is formed from ferroan brucite oxidation under intermediate oxygen fugacity
- Ferrian brucite is isostructural to ferroan brucite and has the same Fe/Mg ratio
- Deprotonation of ferrian brucite layer is responsible for charge compensating  $Fe^{II}$ oxidation
- In the presence of common anions  $(Cl^-, CO_3^2)$ , LDHs are formed from ferroan brucite oxidation



Table 1. List of all experiments sorted by starting material and experimental setup. Mass proportions, xFe and grain sizes are inferred from Rietveld refinement. Numbers in parentheses are standard deviations associated with the refinement. W/R: water to rock ratio ; Ferroan brc: brucite containing Fe(II) ; Pyr: pyroaurite ; Mag: magnetite ; Ferrian brc: brucite containing Fe(III) ; xFe = Fetot/Fetot+Mg SO<sup>4</sup> : sulfate salts used for ferroan brucite synthesis ; Cl : chloride salts used for ferroan brucite synthesis ; R : see text ; \* : starting material "FeBR\_R0.4\_Cl\_5": salt type = Cl, ferroan brc with x = 23.1(6) and  $CSD (110) = 14(1)$  nm





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# 15 **Details for Rietveld refinements on ferroan and ferrian brucite**

17 **Fig. S1.** Evolution of in-plane *a* and out-of-plane *c* unit-cell parameters in brucite-like structures as a 18 function of the ionic radius of octahedral cation. Ionic radii from Shannon (1976). Unit-cell 19 parameters from ICDD database: portlandite-Ca(OH)<sub>2</sub> #44-1481; Cd(OH)<sub>2</sub> #31-228; pyrochroite-20 Mn(OH)<sub>2</sub> #1-73-1133;  $\beta$ -Co(OH)<sub>2</sub> #30-443; brucite-Mg(OH)<sub>2</sub> #44-1482; theophrastite-Ni(OH)<sub>2</sub> #14-21 117; amakinite-Fe $(OH)_2$  from Wyckoff (1963).



 **Fig. S2.** Raman spectra of (A) synthetic and (B) natural ferroan brucites. The spectra were fitted with Lorentzian functions (dashed lines), and their sum is displayed with the solid red curve. The peak at 26 3641 cm<sup>-1</sup> in A and at 3632 cm<sup>-1</sup> in B was attributed to the  $v_1$  OH-stretching band of ferroan brucite. Its position is used to determine the Fe content of ferroan brucite (*x***)** using the calibration of 28 Templeton and Ellison (2020). The broad peak at  $\sim 3590 \text{ cm}^{-1}$  was attributed to ferroan brucite oxidation in air during measurement. **A**. Synthetic ferroan brucite (sample FeBR\_R0.4\_Cl\_11) for 30 which  $x = 0.17 \pm 0.05$  (from Raman spectroscopy). **B**. Oman sample BA4A-81-1-1-17 for which  $x =$ 31  $0.287 \pm 0.03$ . The peak at 3686 cm<sup>-1</sup> with a shoulder at 3700 cm<sup>-1</sup> (Auzende et al., 2004) corresponds to lizardite that is intermixed with ferroan brucite at the submicrometer scale.

# **Implications of the FeIII and FeII** 34 **determination performed on Runs #19 and #20**

35 Both starting material and reaction products of Runs #19 and #20 have been analyzed for their 36 Fe<sup>III</sup> and Fe<sup>II</sup> contents (Fig. S3). The starting material of Run #19 has been aged in the glove box until a thin reddish film was visible. The  $Fe^{III}$  content of this starting material can thus be considered as an 38 upper bound. For comparison, the starting material of Run #20 has been prepared with the same care 39 with respect to  $O_2$  contamination as all the other starting materials used in this study. Despite this 40 care,  $\sim$  8 wt. % of Fe<sup>III</sup> is present in the starting material.

Assuming that all  $Fe^{III}$  present in the starting material would readily produce magnetite, an expected wt.% of magnetite for Runs #19 and #20, of 6.4 and 2.9 is calculated which compares relatively well with the magnetite content derived from Rietveld analysis of the XRPD data of 5.9 and 4.2 wt.%, respectively.

45 The expected  $Fe^{III}/Fe_{tot}$  ratio in Runs #19 and #20 can be calculated from the Rietveld analysis 46 of the XRPD data (Table S4) which provides both phase compositions and proportions. Pyroaurite 47 composition was assumed to be ideal (Mg:Fe ratio of 3:1) because the refined value of its in-plane 48 unit-cell parameter *a* scatters very little [3.1112(13)-3.1170(70) for all samples with > 10% pyroaurite 49 – data not shown] close to the ideal  $3.109 \text{ Å}$  value.

For the run product of Run #19,  $Fe^{III}/Fe_{tot} = 0.82(9)$  to be compared with the measured value 51 of 0.92(6) (Fig. S3). For Run #20,  $Fe^{III}/Fe_{tot} = 0.79(6)$  to be compared with the measured value of 52 0.87(5) (Fig. S3). The Fe<sup>III</sup> and Fe<sup>II</sup> contents of Runs #19 and #20 are therefore in good agreement 53 with the phase composition/structural model that has been used for Rietveld refinement.



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- materials (left) and reaction products (right) for Runs #19 and #20 (top and bottom, respectively).



 **Fig. S4.** Rietveld refinement of X-ray diffraction data from Run #03 reaction products. Zoomed frames show the contribution of each phase. *Int. Exp.*: Measured intensity; *Int. Calc.*: Calculated intensity; *Diff.*: Difference between measured and calculated intensities; *Bkg*: Background



62 **Fig. S5.** Extension of the regression between in-plane *a* unit-cell parameters of brucite-like structures 63 and the ionic radius of divalent octahedral cation to include  $Fe^{III}$ . Values for divalent cations as in Fig. S1; unit-cell parameters for fully oxidized green rust  $(Fe^{III}6O_{12}H_8CO_3)$  from Génin et al. (2006).

65 **Table S1.** Crystal parameters refined for ferroan and ferrian brucite and Rietveld refinement details.

Phase / Sample	a	C	V	Z	$R_{p}$	$R_{WD}$	$R_{exp}$	GoF
	(Å)	(Å)	(Å <sup>3</sup> )		(%)	(%)	$(\%)$	
Ferroan brucite (s.g. #164 $P\overline{3}m1$ )								
FeBR RO.4 S 2	3.1699(4)	4.744(1)	41.29	1	12.2	16.1	18.2	0.88
FeBR RO.4 Cl 2	3.1651(6)	4.751(2)	41.22	1	15.9	21.0	17.9	1.18
Ferrian brucite (s.g. #164 $P\overline{3}m1$ )								
#03 / FeBR R0.4 S M105-2 31d	3.1255(5)	4.6774(13)	39.57	1	10.3	13.5	16.6	0.82
#10 / FeBR R0.4 Cl 36d	3.1259(5)	4.6759(18)	39.57	1	11.8	15.2	15.6	0.97
Notes: <i>a</i> and <i>c</i> : Unit-cell parameters; <i>V</i> : Cell volume; <i>Z</i> : Formula units per cell; <i>Rp</i> : Unweighted profile R-factor; <i>Rwp</i> :								
Weighted profile R-factor; Rexp: Expected R-factor; GoF: Goodness of fit.								

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Phase / Sample	Site - Position	X	у	z	B <sub>iso</sub> $(\AA^2)$	Occ.	(Mg1,Fe1)-O1 (Å)
Ferroan brucite / FeBR R0.4 S 2	$Mg1 - 1a$	$\mathbf 0$	$\Omega$	$\Omega$	0.48	0.774(4)	
	$FeH1 - 1a$	$\mathbf 0$	$\mathbf 0$	0	0.48	0.226(4)	2.121(8)
	$01 - 2d$	1/3	2/3	0.226(3)	0.82		
Ferroan brucite / FeBR R0.4 Cl 2	$Mg1 - 1a$	0	0	0	0.48	0.816(5)	
	$FeH1 - 1a$	0	$\mathbf 0$	$\mathbf 0$	0.48	0.184(5)	2.139(8)
	$01 - 2d$	1/3	2/3	0.234(3)	0.82		
Ferrian brucite	$Mg1 - 1a$	0	0	$\mathbf{0}$	0.48	0.842(20)	
#03 / FeBR R0.4 S M105-2 31d	$Fe^{III}1 - 1a$	$\mathbf 0$	$\mathbf 0$	$\mathbf 0$	0.48	0.152(20)	2.087(8)
	$01 - 2d$	1/3	2/3	0.224(3)	0.82	1	
Ferrian brucite	$Mg1 - 1a$	0	$\mathbf 0$	0	0.48	0.807(36)	
#10 / FeBR R0.4 Cl 36d	$Fe^{III}1 - 1a$	$\mathbf{0}$	$\mathbf 0$	$\mathbf 0$	0.48	0.193(36)	2.080(10)
	$01 - 2d$	1/3	2/3	0.221(4)	0.82		

68 **Table S2.** Fractional atomic coordinates, isotropic displacement parameters and selected interatomic bond distances (Å) for ferroan and ferrian brucite.

		Fit quality estimates					
Run number / Sample name	a param. (Å)	c param. (Å)	z (fraction of c param.)	<b>CSD 110</b> (nm)	Rwp	Rexp	GoF
#01 / FeBR_R0.4_S_M105_8d					16.6	17.9	0.93
#02 / FeBR_R0.4_S_M105_15d	3.1276(8)	4.6703(24)	0.222	44(10)	19.4	19.0	1.02
#03 / FeBR_R0.4_S_M105_31d	3.1255(5)	4.6774(13)	0.224(3)	51(5)	13.5	16.6	0.82
#04 / FeBR_R0.05_S_M105_7d	3.1383(39)	4.7157(31)	0.222	14(2)	14.7	18.4	0.8
#05 / FeBR_R0.05 S_M105_31d	3.1354(9)	4.6891(32)	0.222	48(12)	21.3	20.2	1.06
#06 / FeBR_R0.4_Cl_1d					18.3	17.6	1.03
#07 / FeBR_R0.4_Cl_3d					16.3	18.0	0.91
#08 / FeBR_R0.4_Cl_7d	3.1298(19)	4.6674(41)	0.222	16(2)	15.6	17.0	0.92
#09 / FeBR_R0.4_Cl_15d	3.1244(56)	4.6723(20)	0.222	40(5)	15.1	18.2	0.83
#10 / FeBR_R0.4_Cl_36d	3.1259(5)	4.6759(18)	0.221(4)	58(11)	15.2	15.6	0.97
#11 / FeBR_R0.05_Cl_1d					17.8	19.9	0.89
#12 / FeBR_R0.05_Cl_3d					18.2	19.7	0.92
#13 / FeBR_R0.05_Cl_7d	3.1167(24)	4.6712(41)	0.222		16.1	18.9	0.85
#14 / FeBR_R0.05_Cl_15d	3.1282(12)	4.6789(37)	0.222	23(3)	15.5	17.8	0.87
#15 / FeBR_R0.05_Cl_31d	3.1294(5)	4.6817(12)	0.220(3)	105(24)	17.0	18.9	0.90
#16 / FeBR_R0.05_Cl_w-r25_3d					15.4	18.1	0.85
#17 / FeBR_R0.4_Cl_caps1_105deg_15d					18.2	18.5	0.98
#18 / FeBR_R0.4_Cl_caps2_105deg_26d					15.3	17.4	0.88
#19 / FeBR_R0.4_Cl_10_32d	3.1273(6)	4.6859(21)	0.218(4)	53(10)	29.6	28.7	1.03
#20 / FeBR R0.4 Cl 11 32d	3.1246(7)	4.6733(21)	0.226(4)	38(4)	29.8	28.2	1.05

70 **Table S3.** Results of the Rietveld refinements performed on reaction products from all experiments.

*Note: a* and *c*: ferrian brucite unit-cell parameters (space group  $\overline{P3}m1$ ); *z*: z-coordinate of the O atom 2d position (space group  $\overline{P3m1}$ ); CSD: size of the coherent scattering domains along 110; *Rwp*: Weighted profile R-factor; *Rexp*: Expected R-factor ; *GoF*: Goodness of fit.

72 **Table S4.** Fe<sup>III</sup>/Fe<sub>tot</sub> ratio calculated from phase composition and relative proportions derived from

73 the quantitative phase analysis of reaction products from Runs #19  $\&$  #20.



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