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1	Fluid-rock reaction path modeling of uranium mobility in granite-
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3	Armorican Domain
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7 Abstract

8 The mobilization of uranium in granite-related systems presents a complex interplay of 9 chemical and hydrodynamic factors. This is particularly obvious within syn-orogenic 10 detachment zones where *per descensum* surface-derived fluids interact with *per ascensum* 11 deeply sourced hydrothermal fluids. In this study, we employ a thermo-hydro-chemical (TH-12 C) modeling approach to explore the multifaceted processes that govern uranium transport and deposition in such environments. Our findings indicate that uranium mobility is not solely 13 14 determined by the oxidizing nature of the percolating surface-derived fluids. Actually, the 15 oxidation-reduction potential of these fluids varies as they flow in the crust, ultimately 16 adjusting towards more neutral or mildly reducing conditions conducive to uranium dissolution 17 and precipitation. Even in the presence of magnetite, which enhances the reductive potential of 18 the fluids, uranium continues to dissolve, albeit in much smaller quantities, with U(IV) being 19 the predominant species in the aqueous phase. The study highlights the crucial roles of 20 temperature, pH, and fluid/rock interaction ratios in influencing uranium leaching efficacy. 21 High fluid/rock ratios enhance uranium extraction from source rocks. A fluid/rock ratio around 22 1 is optimal, maximizing the dissolution of uranium-bearing minerals in the source rock and 23 promoting the precipitation of uranium minerals in different locations along the fluid pathway 24 due to changes in fluid chemistry. The TH-C modeling has the potential to be applied to a 25 variety of other uranium deposits, developed below 300°C.

- 26 Key-words: Uranium Mobilization; Fluid/Rock Interaction; Redox Potential; Thermo-Hydro-
- 27 Chemical Modeling (TH-C); Syn-kinematic Granite; Detachment Zones.
- 28

29 **1. Introduction**

30 Uranium mineralization associated with granites emerges as an important category among the 31 various types of uranium deposits, demonstrating widespread occurrences worldwide (Cuney, 32 2009, 2010; Romer and Cuney, 2018). These deposits account for 29% of the total identified 33 uranium resources in China (Woods et al., 2019). The Variscan belt hosts numerous uranium deposits that are both spatially and temporally associated with granites (Cuney et al., 1990; 34 35 Marignac and Cuney, 1999; Kříbek et al., 2009; René and Dolníček, 2017; Romer and Cuney, 2018; Mikulski et al., 2020), especially with peraluminous syn-kinematic granites (Poty et al., 36 37 1986; Cathelineau et al., 1990; Cuney et al., 1990; Tartèse et al., 2013; Ballouard et al., 2017).

38 The interplay between hydrothermal fluids circulations and the activity of shear zones, particularly in the context of syn-kinematic granite emplacement helps understanding the 39 40 genesis of uranium deposits. Advances in this area are propelled by geological characterization, 41 which allows building conceptual models (e.g., Ballouard et al., 2017; Qiu et al., 2018). 42 Besides, numerical studies have been developed to reconstruct the physical conditions under 43 which hydrothermal circulations in permeable zones have enabled the development of 44 comprehensive thermo-hydrodynamic models (e.g., Eldursi et al., 2009; Souche et al., 2014; Labrousse et al., 2016; Bock et al., 2024). Despite these advances, current fully-coupled 45 46 numerical studies (i.e., Thermo-Hydro-Mechanical-Chemical, THMC) have not yet reached 47 the level of sophistication required to encompass the bulk complexities, among which are 48 chemical aspects associated with hydrothermal circulation especially linked to granite 49 emplacement.

50 At high temperatures, from 300°C to magmatic conditions (~650°C), the chemical processes 51 involved in uranium mobilization and trapping are underexplored (Cuney and Kyser, 2009). 52 This is primarily due to the limitations of current thermodynamic databases, which only cover 53 uranium species up to a maximum temperature of 300°C (Pearson and Berner, 1991). Below 54 300°C, the understanding of uranium geochemistry is sufficient to model the mechanisms of 55 uranium dissolution and precipitation (Romberger 1984; Timofeev et al., 2018). The oxidation 56 state of uranium is a critical factor in determining its geochemical behavior. Under reducing 57 conditions, tetravalent uranium (U(IV)) commonly forms poorly soluble phases, thereby 58 limiting its mobility in aqueous fluids, whereas hexavalent uranium (U(VI)) is significantly 59 more soluble, enhancing its transport (Langmuir, 1997; Grenthe et al., 1992; Finch and Ewing, 60 1992; Curtis et al., 2006; Cuney and Kyser, 2009; Spycher et al., 2011). This underscores the 61 importance of redox conditions and ligand complexation in controlling uranium behavior in 62 geological environments (Langmuir, 1978; Abdelouas, 2006). However, it is also recognized 63 that uranium can sometimes remain mobile under reducing conditions, particularly when 64 complexed with ligands such as chloride. Recent experimental investigations by Timofeev et 65 al. (2018) have identified a novel uranium chloride species, UCl₄°, that demonstrates greater thermodynamic stability under reducing conditions compared to oxidizing conditions. 66 67 Furthermore, the mobility of uranium is influenced by the solubility of its complexes, with 68 predictions of uranium migration being inherently complex due to the interplay between 69 temperature gradients, pH variations and changes in oxidation states (Carnahan, 1986).

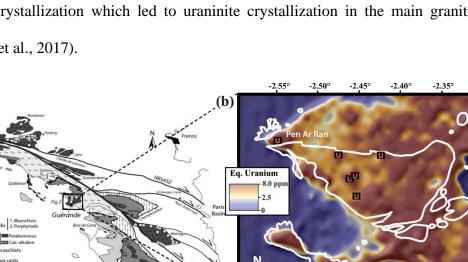
Addressing the metallogenic triptych of source, transport and deposition necessitates tracking fluid-rock interactions across various temperature fields and fluid/rock ratios. This complexity has not been thoroughly characterized for uranium, particularly regarding chemical conditions such as redox potential, pH and speciation (White, 1968). To bridge this gap, we have developed a TH-C modeling approach, complementary to methods such as thermo-hydro-

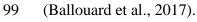
75 chemical coupling (THCC) employed by Carnahan (1986). The TH-C approach investigates 76 uranium mobility in relation to fluid flow associated with granitic intrusions in tectonically 77 active settings dominated by detachment faulting. This local uranium mobility can lead to 78 uranium mineralization, as seen in the Variscan South Armorican uranium system (Ballouard 79 et al., 2017), which serves as an application of our modeling. The aim of this study is to enhance 80 our understanding of uranium speciation, redox conditions and of the interactions between 81 uranium-bearing fluids and host rocks, especially in cases where fluids encounter relatively 82 high temperature conditions (around 300°C).

83 2. The Variscan South Armorican Domain as a case study

Uranium deposits associated with peraluminous granites are found worldwide, for instance and among numerous others, in the Erzgebirge-Krušné Hory region spanning Germany and the Czech Republic (Zhang et al., 2017) and in the Motianling uranium district of South China (Qiu et al., 2018). The South Armorican Massif uranium deposits investigated in this study (Fig. 1) exemplify a general case study of granite-related uranium deposits (e.g., Cuney, 1978; Tartèse et al., 2013; Ballouard et al., 2017).

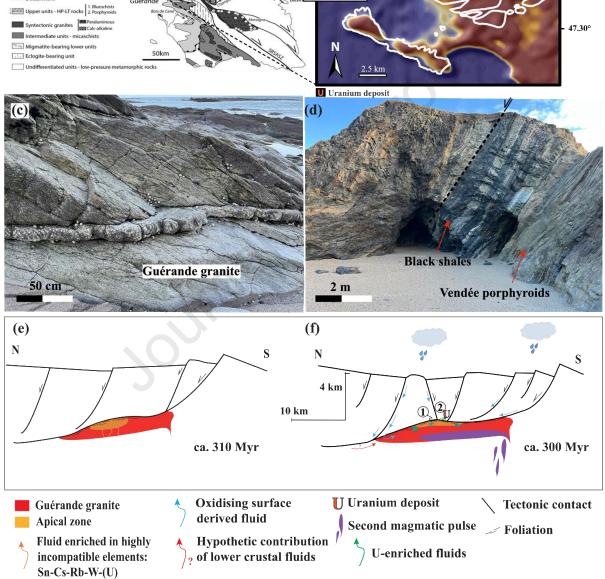
90 In the southern region of the Armorican Massif (Fig. 1a), the Guérande leucogranite was 91 emplaced around 300 Ma along a late-orogenic detachment fault (Ballouard et al., 2015). It 92 hosts a cluster of uranium deposits (Fig. 1b). The uranium mineralization has been dated 93 between 300 and 275Ma (Ballouard et al., 2017). It coincides with late intrusion of 94 microgranite dykes around 300 Ma and on-going hydrothermal pulses. Some uranium deposits 95 occur at the faulted contact between black shales and metavolcanics, commonly known as 96 porphyroids (see Fig. 1c and 1d), which are situated over the apical zone of the intrusion (see 97 Fig. 1e and f). Primary enrichment in uranium in this apical zone is basically a consequence of 98 fractional crystallization which led to uraninite crystallization in the main granitic pluton





(a)

Maior thr





101 Figure 1: (a): Simplified geological map of the South American Domain; the insert corresponds to the Variscan 102 Guérande pluton (Ballouard et al., 2017)). (b): Airborne radiometric map showing the distribution of uranium 103 deposits in the Guérande area. The white line corresponds to the cartographic contour of the Guérande pluton 104 (Ballouard et al., 2017). (c) and (d) are field views, localized in (f), showing respectively the deformed U-rich

-2.30°

47.40°

47.35°

apical zone of the leucogranite pluton intersected by a quartz vein (1), and the alternating layers of porphyroids
(metavolcanics) and black shales crosscut by a normal fault (2); The Pen Ar Ran uraninite deposit occurs along
this fault and was mined about 50 m below the sand beach. (e) and (f) are synthetic cross-sections illustrating the
Guérande metallogenic model (Ballouard et al., 2017).

Data from airborne radiometric surveys combined with stable isotopes and fluid inclusions analyses point to the significant leaching of uranium. This leaching was linked to the alteration of uraninite-bearing apical rocks by oxidizing surface-derived fluids (Ballouard et al., 2017). Both the enhanced thermal conditions related to magmatic intrusions, especially during the second magmatic pulse at ca. 300 Ma and the brittle deformation in the hanging wall of the detachment greatly contributed to trigger and maintain fluid circulation and thus mobilization and deposition of uranium.

116 3. Modeling background

Among the various methodologies available for modeling the formation of uranium deposits (e.g., IAEA, 2020; Qu et al., 2021; Shen, 2021), process-based modeling stands out due to its comprehensive approach (Komninou and Sverjensky, 1996). This technique simulates the fundamental geological processes responsible for ore deposits through THMC (Thermo-Hydro-Mechanical-Chemical) modeling, integrating fluid flow, heat transfer, mechanical dynamics and chemical reactions (e.g., Oliver et al., 2006; Harcouët-Menou et al., 2009; Eldursi et al., 2018).

Expanding on the foundation of process-based modeling, reactive transport modeling serves as a critical tool. It couples fluid flow, heat transfer and multicomponent reactive transport equations, demonstrating its robustness in controlled environments such as in situ uranium leaching, as evidenced in studies by Collet et al. (2022), Qiu et al. (2023) and Zhang et al. (2023). The applicability of this method extends to other deposit types, including unconformity-related deposits (e.g., Wang and Chi, 2023). Despite its proven utility, deploying

130 process-based modeling in large-scale reservoirs spanning tens of kilometers, particularly those 131 subject to multiple driving forces like buoyancy and topography, with high temperatures 132 associated with magma emplacement, poses significant challenges. Solving the thermo-133 hydrodynamic model in these large dynamic systems leads to considerable computation times 134 and difficulties in achieving model convergence. Additionally, integrating reaction rates 135 between fluids and minerals is challenging due to the lack of data for high-temperature 136 conditions and the complexity of solving numerous reactions simultaneously with temperature 137 and fluid pressure calculations.

138 Significant progress has been made in large-scale Darcyan hydrothermal system modeling, 139 particularly in coupling heat, multiphase fluid and salinities (Weis et al., 2014). Building on 140 this progress, we have adopted here a commonly used procedure that decouples heat and fluid 141 transport from chemical species reactions. This approach referred to here as TH-C (Thermo-142 Hydrodynamic-Chemical modeling), allows tackling each component with great focus and 143 specificity, enhancing the accuracy and efficiency of modeling. By solving both thermal and 144 fluid flow processes simultaneously, we can model the influence of heat on fluid flows, 145 including convective heat transport. The way temperature gradients affect fluid circulation can 146 also be targeted. This simultaneous modeling is critical as heat and fluid dynamics are deeply 147 interrelated, and any change in one has a direct impact on the other. For instance, fluid 148 circulation can transport heat through the system, whereas changes in temperature can alter 149 fluid properties such as density and viscosity, which in turn affect flow rates and directions.

150 Chemical reactions, on the other hand, are resolved separately from the thermal and 151 hydrodynamic processes. This decoupling enables more focused and detailed treatment of 152 chemical interactions, such as mineral dissolution, precipitation and complexation reactions, 153 without the additional computational complexity associated with continuously updating 154 thermal and fluid variables.

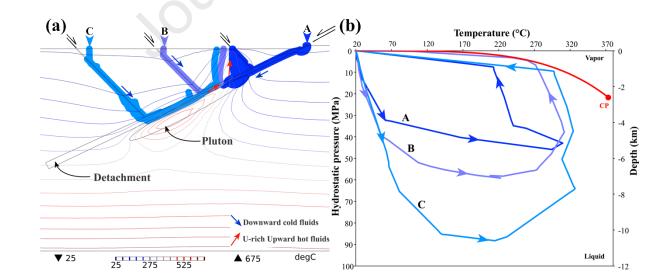
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155 4. Strategy and model set-up

156 **4.1 Numerical approach**

157 Bock et al. (2024) solved the equations of heat and fluid transports in uranium-bearing systems associated with detachment and syn-kinematic granites, with an application to the Guérande 158 159 uranium mineralized system. During periods of plutonic activity, significant downward 160 meteoric fluid flow occurs (Fig. 2a), eventually reaching the apical zone of the granitic pluton. 161 This hydrothermal activity is driven by magmatic emplacement, which increases the buoyancy of the overall system, reinforcing the pre-existing convective flow typically driven by pressure 162 163 gradients due to surface topography, large permeability contrasts, or both. The influx of thermal 164 energy from the magmatic intrusion promotes the downward movement of surface-derived fluids, which then penetrate deep into the system, eventually reaching the apical zone of the 165 166 pluton. As these fluids are heated, their density decreases, triggering their upwelling which 167 completes the convective cycle. The pressure-temperature (PT) trajectories of the fluid particles indicate that they remain in the liquid state (Fig. 2b). In the present study, the PT 168 169 trajectories in space are utilized in an iterative chemical modeling process (Fig. 3). The 170 PHREEQC software (Parkhurst and Appelo 1999) is employed to simulate the interaction of 171 meteoric fluids with rocks at several PT points in three successively infiltrated reservoirs 172 (points 1 to 9; Figs. 3 and 4). This choice of three reservoirs is based on the case of the South American Domain (Fig. 1). Firstly, the fluids flow through the crust (Reservoir 1, points 1 to 173 174 4), where it interacts with crustal rocks before reaching the apical zone of the leucogranitic 175 pluton (Reservoir 2, points 5 to 7), the main source of uranium. Then, the fluid leaves the apical 176 domain and enters the black shale reservoir (Reservoir 3, point 8). Return in the crustal first 177 reservoir corresponds to point 9.

178 PHREEQC is primarily designed for equilibrium chemistry modeling of aqueous solutions as 179 they interact with minerals, gases, solid solutions, exchangers and sorption surfaces. It also has 180 the capability to model kinetic reactions. However, the efficiency of these kinetic models 181 depends on the quality and availability of kinetic data. Given the notable deficiency in kinetic data for uranium species at high temperatures, we have opted for a forward modeling approach 182 183 based on equilibrium calculations, similar to the approach used by Post et al. (2017). This 184 approach leverages well-established and widely available thermodynamic data, such as 185 solubility constants and Gibbs free energy, applicable to a broad spectrum of minerals and 186 environmental conditions. Notably, our approach incorporates both reduced and oxidized 187 uranium species, providing a comprehensive analysis of uranium mobility under various redox 188 conditions. In our methodology, the output from a calculation at one point provides the basis 189 for the subsequent calculation at the next point. For instance, the fluid composition calculated 190 after the reaction at point 1 is used as the invading fluid for point 2. This procedure continues 191 across the nine modeled batch reactions, with evolving temperatures from 25°C to 300°C (for 192 points 1 to 7) and then from 300°C to 200°C (for points 7 to 9), as shown in Figure 3.



193

Figure 2: (a) Model of surface-derived fluids infiltration into a detachment zone associated with a syn-kinematic
leucogranite pluton (particle tracing from Thermo-hydrodynamic models of Bock et al., 2024). The colored lines

196 correspond to isotherms. (b) Pressure-temperature diagram where the flow of fluid particles along paths A, B and

197 C are reported (adapted from Bock et al.,2024). CP = Critical Point for pure water (374°C, 22 MPa).

198

199 **4.2 Experimentation and Sensitivity Studies on Uranium Mobility**

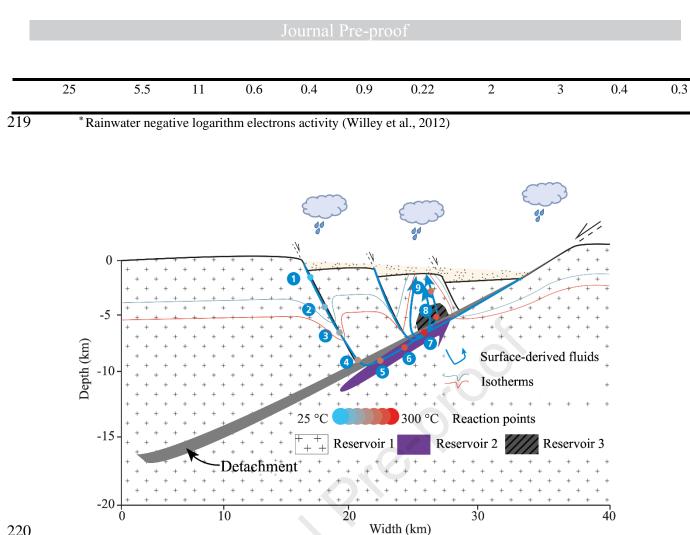
- 200 The numerical analyses conducted in this study are categorized into three groups:
- The first group of experiments, referred to as the base model, involves batch reaction
 computations for the nine designated points (Fig. 3). This setup features a fluid/rock
 ratio (F/R) of 0.01, with 1 kg of water interacting with 99 kg of rocks.
- 204 2. The second experiments undertake a sensitivity analysis to explore the effect of varying
 205 fluid/rock ratios on uranium mobility, with F/R of 0.01 (the base model), 0.1, 0.3, 0.5,
 206 0.7, 0.9, 1, 3 and 100.
- 3. The third experiments focus on a sensitivity analysis concerning the redox conditions of
 surface-derived fluids. This is conducted for the base model by adding magnetite at two
 concentrations in Reservoir 1 (0.5 wt.% and 1.6 wt.%; Fig. 4).
- 210

211 **4.3 Initial conditions**

The initial composition of the meteoric fluid is based on data from Freeze and Cherry (1979). We used the average composition of seven different rain and snow sites across the United States, Australia and Northern Europe, following the approach used by Lee et al. (2003). We set a temperature of 25°C and a typical electron activity (pe) of 11 (Willey et al., 2012) as an input for point 1 (Fig. 3).

217Table 1: Rainwater composition and parameters used at the first batch reaction point, with the composition218in mg/L and the temperature in degrees Celsius. (Freeze and Cherry, 1979)

Temperature	pН	pe*	Na	K	Ca	Mg	HCO3	SO4	Cl	NO3



220

221 Figure 3 : Model of meteoric fluid percolation through different geological reservoirs associated with a detachment 222 zone (inspired from the hydro-thermodynamic models of Bock et al., 2024). The location of the 9 reaction points 223 is deduced from particle tracing in Bock et al. (2024) (see also Fig. 2) and is indicated along the flow path of 224 surface-derived fluids (numbered blue circles).

225 Our approach considers the progression of the surface-derived fluids through three geological 226 reservoirs (Fig. 3 and 4). Reservoir 1 is defined using the average composition of the upper 227 continental crust (Taylor and McLennan, 1985), with a uranium concentration of 2.8 ppm. In 228 the upper crust, uranium typically occurs as a trace element, often found in minerals like zircon 229 and apatite. However, since these minerals do not have uranium in their chemical formulas, it 230 is difficult to accurately represent uranium in the mineral assemblage for this reservoir. 231 Although we could use a uranium mineral like uraninite to model its presence, this would not 232 accurately reflect how uranium is naturally distributed in the upper crust. For this reason, we 233 have avoided including uranium in the first reservoir composition. Reservoir 2 features a

234 classical leucogranite mineral composition (Harris and Inger, 1992) close to the differentiated 235 facies of the Guérande granite (Ballouard et al., 2015, Fig. 4). In Ballouard et al. (2017), the 236 initial uranium content in the granites is reported as 20 ppm, based on drill core samples from 237 Ouddou (1984). Of this, it is estimated that 50% of the uranium is hosted by uranium oxides. Given that uranium in trace amounts (for the remaining 50%) cannot be accurately modeled 238 239 due to technical reasons (as previously discussed), we chose to represent only the uranium 240 hosted by uranium oxides. This choice is supported by Ballouard et al. (2017), which argue that uraninite crystallizes in differentiated melts when the uranium content reaches around 10 241 242 ppm. Based on this information, we selected a uranium concentration of 12.5 mg/kg (corresponding to 0.0014 wt.% of uraninite, Fig. 4) that aligns with the conditions under which 243 244 uraninite is expected to form. Reservoir 3 is close to Reservoir 1 but it contains pyrite to reflect 245 the reducing property of the black shales where U deposits formed (Fig. 1d and f).

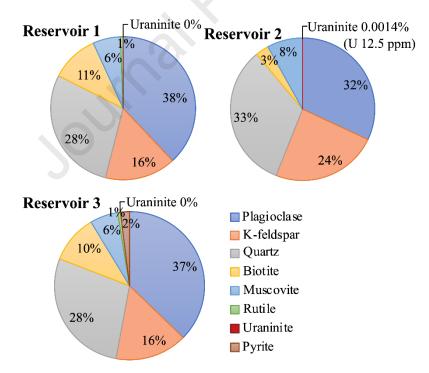


Figure 4: Mineralogical composition in wt.% of the three reservoirs infiltrated by surface-derived fluids. Details and references of the three reservoir compositions are presented in section 4.4.

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247 **4.4 Benchmarking**

248 In the preliminary phase of our research, we have conducted a benchmark study using 249 PHREEQC to replicate the uranium speciation model at ambient conditions of 25°C (Fig. 3), 250 as proposed by Tripathi (1979). This benchmarking served as a foundational step in selecting 251 the most appropriate thermodynamic database from those available within PHREEQC. The 252 Lawrence Livermore National Laboratory (LLNL) database emerged as the preferred choice due to its robustness, relevance to our study and comprehensive temperature applicability, 253 supporting simulations up to 300°C. Additionally, it includes an extensive catalog of 2590 254 255 species ensuring broad coverage of potential reaction pathways. Crucially, the LLNL database demonstrated high fidelity in mirroring the speciation trends outlined in the model of Tripathi 256 257 (1979), as shown in Figures 5a and 5b, affirming its utility for our geochemical modeling. This 258 aligns with the compilation of Cuney and Kyser (2009). In Figure 5c, we present the proportions of Ca-U complexes (CaUO₂(CO₃)_{3²⁻ and Ca₂UO₂(CO₃)₃(aq)) within uranium(VI),} 259 260 which were not identified at the time of the Tripathi calculations.

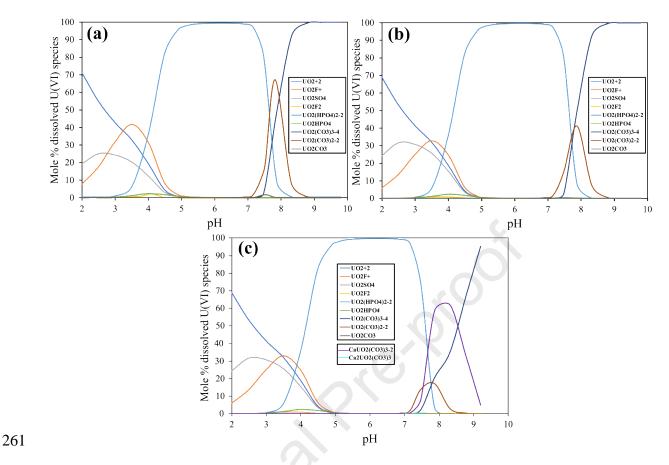


Figure 5: (a) Molar percentage of dissolved uranium (VI) species as a function of pH at 25°C redrawn from Tripathi (1979). Conditions are: $\Sigma U(VI) = 10^{-8}$ M, $\Sigma F = 0.3$ ppm, $\Sigma CI = 10$ ppm, $\Sigma SO4 = 100$ ppm, $\Sigma PO4 = 0.1$ ppm, $\Sigma SiO_2 = 30$ ppm and $P_{CO2} = 10^{-2.5}$ atm. (b) Our replication of Tripathi (1979) model using the Lawrence Livermore National Laboratory (LLNL) database. (c) Same as (b), but adjusted with Ca = 0.9 ppm to include the percentages of Ca-U complexes that were unknown during the original Tripathi (1979) study.

267 **5. Results**

268 5.1 The base model (Fluid/Rock ratio = 0.01)

269 5.1.1 Mineral reactions and evolution of pe and pH

The infiltration of fluid through Reservoir 1 is accompanied by an increase in temperature from 25°C to 150°C (points 1 to 4; Fig. 6), a gradual increase in pe and a decrease in pH. From points 1 to 4, there is no U in the solution. The concentrations of Si, Al and K increase, and those of Ca and Mg decrease.

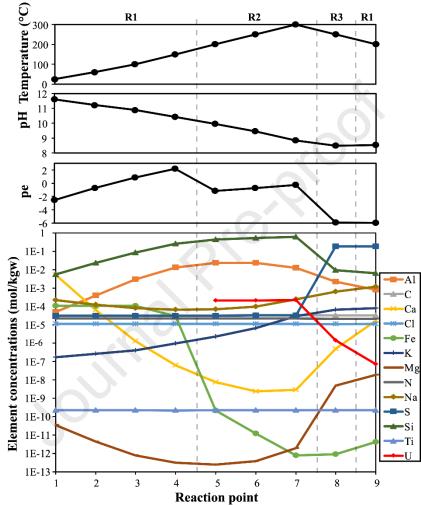


Figure 6: Temperature, pH, pe and concentrations of a variety of elements in the fluid phase for the base model along the flow path represented by the 9 reactions points. The three reservoirs are labeled R1, R2 and R3.

In Reservoir 2, temperature increases from 200°C to 300°C (points 5 to 7) and pH continues to
decrease. Concurrently, there is a marked pe drop before a re-increase toward point 7.
Dissolution of uraninite is evidenced by the appearance of U in solution (red line in Figure 6).
A significant drop in Fe concentration at point 5 then a decrease toward point 7 is observed
(Fig. 6).

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Upon entering Reservoir 3, the temperature decreases after its peak in Reservoir 2, accompanied by continued pH acidification and a drop in pe. The significant decrease in U concentration indicates precipitation of uraninite. There is also a decrease in the concentrations of Si and Al, and a strong increase in S, Ca and Mg. As the fluid returns to Reservoir 1 at 200°C (point 9), both pe and pH do not vary. The U concentration in the solution drops further, whereas there is a significant increase in the concentrations of Ca, Mg and Fe.

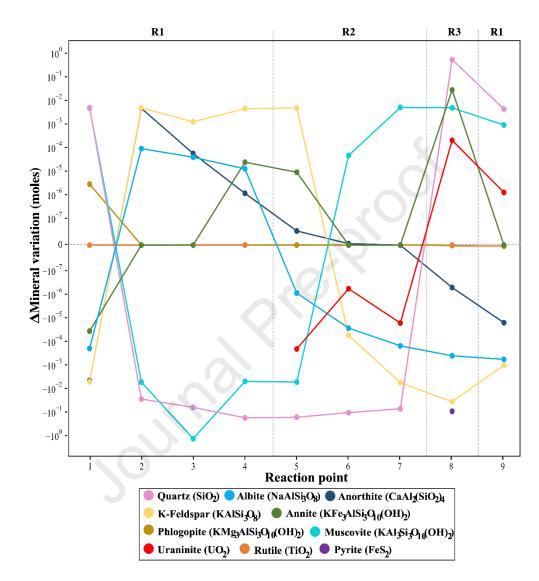
287 Figure 7 exhibits the variations of mineral content at the equilibrium across the three reservoirs. A negative delta value means that the mineral undergoes dissolution, and a positive delta value 288 289 means that the mineral undergoes precipitation. These processes of dissolution and 290 precipitation align with the elemental changes in the solution (Fig. 6), providing insight into 291 the fluctuations in pH $(-\log[H^+])$ and pe $(-\log[e^-])$ across the three reservoirs. For instance, the 292 concentration of Fe in Reservoir 1 remains relatively stable (Fig. 6), as annite dissolution at 293 point 1 (Fig. 7) is followed by stabilization. Upon entering Reservoir 2, a marked drop in Fe concentration (Fig. 6) is observed, consistently with the precipitation of annite (Fig. 7). In 294 295 Reservoir 3, Fe levels increase slightly at points 8 and 9 (Fig. 6), which can be attributed to 296 pyrite dissolution (Fig. 7). This evolution of Fe throughout the system is a key factor in the 297 variations in pe. The rise in pe from -2.5 to 2.2 in Reservoir 1 is primarily driven by the 298 oxidation of ferrous iron (Fe^{2+}) released during the initial dissolution of annite at point 1 (Fig. 299 7):

$$KFe_{3}AlSi_{3}O_{10}(OH)_{2} + 10H^{+} \rightarrow K^{+} + Al^{3+} + 3Fe^{2+} + 3SiO_{2} + 6H_{2}O$$
(1)

$$Fe^{2+} \rightarrow Fe^{3+} + e^{-} \tag{2}$$

300 Although annite undergoes precipitation in subsequent points of Reservoir 1, the moles of Fe^{2+} 301 released from its initial dissolution exceed the amount removed through precipitation. This

302 surplus of Fe^{2+} in the aqueous phase sustains oxidation reactions, consuming electrons and 303 driving the increase in pe (Reaction 2).



304

Figure 7: Variation in mineral concentrations (in moles) within the rock across the nine reaction points, plotted
on a symmetric logarithmic scale. Rutile is absent in Reservoir 2, and pyrite is present only in Reservoir 3 (see
Fig. 4 for details).

- 308 The sudden drop in pe from 2.2 to -1.1, at the transition to Reservoir 2 (Fig. 6), is primarily
- 309 driven by the dissolution and oxidation of uraninite:

$$UO_2 + 4H^+ \to U^{4+} + 2H_2O$$
 (3)

310 Under oxidizing conditions, U^{4+} is readily oxidized to U(VI) in the form of UO₂²⁺:

$$U^{4+} + 2H_2O \to UO_2^{2+} + 4H^+ + 2e^-$$
(4)

Following this sharp drop in pe, a slight increase from -1.1 to -0.27 (Fig. 6) occurs due to the
ongoing consumption of electrons remaining in the system (Reaction 2).

In Reservoir 3 (point 8), the fluid exhibits a drop in pe to -5.9 (Fig. 6). This significant shift in
the redox potential is directly associated with the introduction and dissolution of pyrite (Fig.
7):

$$FeS_2 + H_2O \rightarrow 0.25H^+ + 0.25SO_4^{2-} + Fe^{2+} + 1.75HS^-$$
(5)

316 During this process, both ferrous iron (Fe²⁺) and hydrosulfide ions (HS⁻) are released, both of 317 which can participate in redox reactions. One key reaction is the oxidation of hydrosulfide 318 (HS⁻) to sulfate (SO_{4²⁻}), which releases electrons. This increase in electron activity lowers the 319 pe of the system:

$$HS^- + 4H_2O \rightarrow SO_{4^{2-}} + 9H^+ + 8e^-$$
 (6)

At Point 9 (Reservoir 1), the pe remains relatively constant with only a minor increase from -5.92 to -5.97 as the system is already under strongly reducing conditions due to previous processes, such as pyrite dissolution. The electron consumption from uraninite precipitation is balanced by the limited availability of oxidizing agents, resulting in the pe stabilizing rather than increasing.

In terms of pH, the fluid shows a steady decrease from 11.6 at point 1 to 8.4 at point 8, followed by a slight rise to 8.5 at point 9 (Fig. 6). The gradual decline in pH from point 1 to point 8 can be primarily attributed to proton-releasing precipitation reactions, which outweigh protonconsuming dissolution reactions. The precipitation of silicate minerals (Fig. 7), such as annite 329 (Reaction 1), albite (Reaction 7), K-feldspar (Reaction 8), anorthite (Reaction 9), and 330 muscovite (Reaction 10), releases protons (H⁺), contributing to an increase in hydrogen ion 331 concentration, thereby lowering the pH:

$$Al^{3+} + Na^{+} + 2H_2O + 3SiO_2 \rightarrow NaAlSi_3O_8 + 4H^+$$
 (7)

$$K^+ + Al^{3+} + 3SiO_2 + 2H_2O \rightarrow KAlSi_3O_8 + 4H^+$$
 (8)

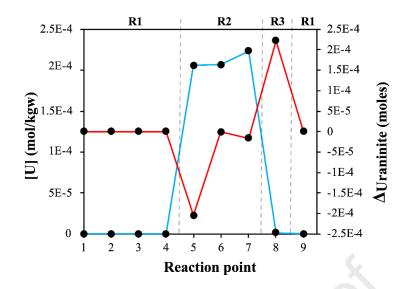
$$Ca^{2+} + 2Al^{3+} + 2SiO_2 + 4H_2O \rightarrow CaAl_2Si_2O_8 + 8H^+$$
(9)

$$K^{+} + 3Al_{3}^{+} + 3SiO_{2} + 6H_{2}O \rightarrow KAl_{3}Si_{3}O_{10}(OH)_{2} + 10H^{+}$$
(10)

In contrast, the subtle rise in pH is primarily due to the dissolution of silicate minerals (Fig. 7).
The dissolution of these minerals consumes hydrogen ions, thereby reducing the acidity of the
fluid and causing a slight increase in pH at point 9 (Fig. 6).

335 5.1.2 Uranium solubility and speciation

In Figure 8, we observe an inverse relationship between the U concentration in the solution and the changes in the amount of uraninite in the rock ($\Delta_{\text{Uraninite}}$). When U concentration in solution increases, the amount of uraninite decreases due to dissolution, and when U concentration decreases, it increases due to precipitation.



340

Figure 8: The variations of uraninite moles (in red) and uranium concentration in the solution (in blue) across thethree reservoirs.

The distribution of the uranium species in solution is depicted in Figure 9. In Reservoir 2, U(VI) species predominate, featuring a variety of forms such as $UO_2(OH)^{3-}$ and $(UO_2)_3(OH)^{5+}$, reflecting stability influenced by pH fluctuations. Conversely, in Reservoir 3, where uranium concentration is significantly reduced due to uraninite precipitation under reductive conditions, U(IV) species become predominant. Specifically, U(OH)₂ is the stable form observed consistently across all five batch reaction stages, despite substantial variations in pH and pe.

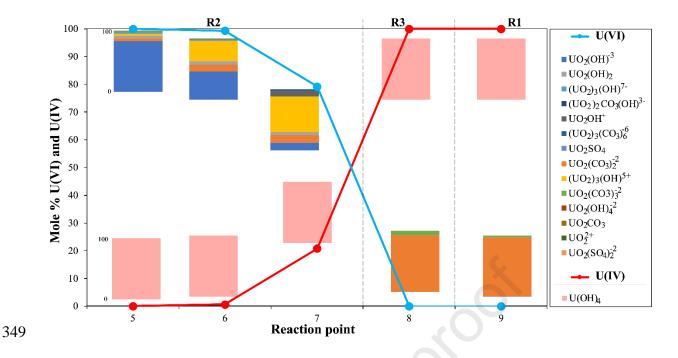


Figure 9: Relative proportions of U(VI) and U(IV) in the fluid phase for Reservoirs 2 and 3 for the base model.
The dissolved species for U(VI) and their relative abundance are indicated as colored bands in the rectangles close
to the blue line. The U(IV) species is U(OH)₄ for all points.

353 5.2 Dependency of uranium mobility on Fluid/Rock (F/R) ratio

The influence of the fluid/rock ratio on chemical parameters along the fluid path is shown in Figure 10. Initially, pH decreases consistently along the flow path for all F/R ratios, with the exception of a stabilization between points 8 and 9. This pH decline is particularly pronounced at lower F/R ratios (F/R = 0.01, 1 and 3; Fig. 10a). In Reservoir 1, the pe increases similarly across all F/R ratios (Fig. 10b). However, in Reservoir 2, the pe profile diverges, F/R ratios of 0.01 and 1 exhibit a significant drop followed by a subsequent increase, whereas F/R ratios of 3 and 100 display a continuous rise without a preceding decrease.

In the high fluid/rock ratio scenario (F/R = 100), the fluid geochemical evolution reveals distinct trends in both pH and pe compared to the base model. The pH decreases gradually from 11.6 at point 1 to 10.7 at point 8, followed by a slight increase to 10.8 at point 9. This more moderate pH decline can be attributed to a closer balance between proton-releasing and proton-

365 consuming reactions compared to the base model. In parallel, the pe rises from -2.5 at point 1 366 to a peak of 1.6 at point 6, then drops sharply to -8.2 at point 8, and remains low through point 367 9 (Fig. 10a and 10b). These notable deviations from the base model can be attributed to the 368 high fluid volume compared to that of the rock, which facilitates extensive annite dissolution 369 (Reaction 1), enabling the continuous increase in pe at the transition of Reservoir 1 to Reservoir 370 2. Additionally, the extensive pyrite dissolution (Reaction 5) in Reservoir 3 intensifies the 371 reducing conditions, causing the pe to decline significantly to -8.2 at point 8.

372 In the scenarios with F/R ratios of 1 and 3, the pH behavior closely mirrors that observed in 373 the base model. However, the pe profiles exhibit significant variations due to the different fluid-374 to-rock proportions.

For F/R = 1, the pe trend is similar to the base model but displays higher values between points 5 and 7 (Fig. 10b), indicating a relatively more oxidizing environment during this interval. The increased fluid volume relative to rock promotes enhanced oxidation reactions, such as the oxidation of ferrous iron and uranium species. Notably, uraninite dissolution reaches its peak at this fluid/rock ratio (Fig. 10b and 10d). The higher pe values suggest that the system has a greater capacity to consume electrons through these oxidation processes, resulting in more oxidizing conditions compared to the base model.

For F/R = 3, the pe pattern is similar to that of F/R = 100, with an initial increase followed by a decrease (Fig. 10b). However, the pe values remain higher from points 3 to 9 compared to the F/R = 100 scenario. This suggests that at F/R = 3, the system maintains more oxidizing conditions over a broader range of points. The balance between oxidation and reduction reactions is strongly influenced by the fluid/rock ratio, where the fluid volume is sufficient to drive oxidation reactions without overwhelming the system with reduced species from mineral

dissolution. As a result, the pe remains elevated for a longer portion of the fluid path, reflectingsustained oxidizing conditions.

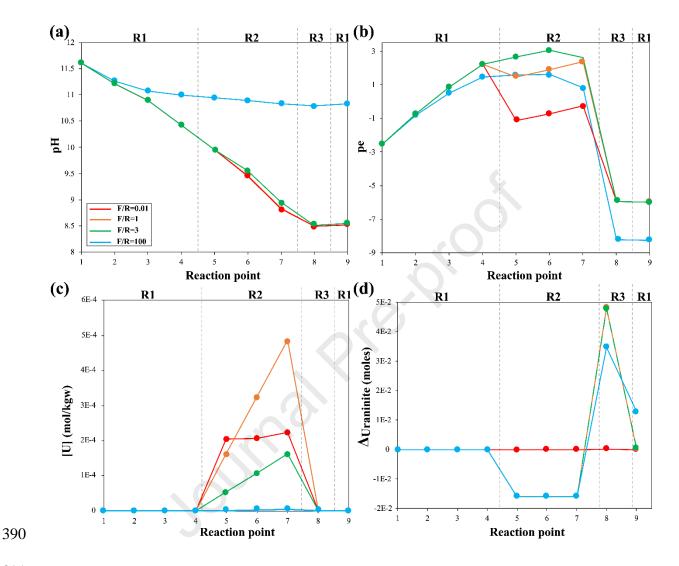


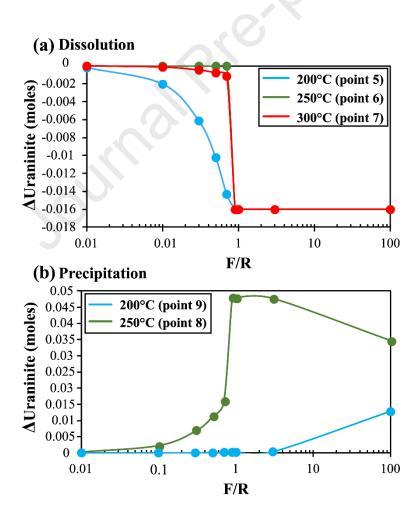
Figure 10: pH (a), pe (b), uranium concentration in the solution (c) and uraninite moles variation in the rock (d) along the reaction pathway (points 1 to 9) for various fluid/rock ratios. The red curve corresponds to the base model (it was presented on a larger scale in Figure 8).

The evolution of U concentration in solution (Fig. 10c) and the variation of uraninite amount in the rock (Fig. 10d) reveals a complex pattern. At point 5, an increase in the F/R ratio from 1 to 100 leads to a decrease in dissolved U due to a dilution effect. Points 6 and 7 show that the highest amount of dissolved U corresponds to F/R = 1 (Fig. 10c). The contents for F/R = 0.01and 3 are not so different. For the rock, uraninite dissolution is very low for F/R = 0.01 (base

model, Fig. 10d) compared to higher F/R ratios. Uraninite dissolution (points 5, 6 and 7) and
precipitation (points 8 and 9) are both more pronounced for F/R ratios of 1, 3 and 100 than for
the base model (Fig. 10d).

402

These observations suggest a correlation between pe variability with respect to F/R ratios and uraninite precipitation. Specifically, the lowest pe values at reaction points 8 and 9 correspond to significant uraninite precipitation. This correlation is less obvious for uraninite dissolution during which pe values vary more erratically and are less predictable. Nonetheless, the increase in uraninite dissolution observed for high F/R ratios corresponds to high pe values ($pe \ge 1$) (Fig. 10b).



409

Figure 11: Variations of the uraninite moles in infiltrated rocks as a function of fluid/rock (F/R) ratios. Negative
values (a) indicate uraninite dissolution and positive values (b) indicate uraninite precipitation.

412 In Reservoir 2, for F/R ratios lower than 0.9, uraninite dissolution is lower at elevated 413 temperatures (250°C-300°C) than at lower temperatures (200°C) (Fig. 11a). For F/R ratios 414 higher than 0.9, the dissolution rate remains constant, with uraninite entirely dissolved (Fig. 415 11a). This feature may be explained by the fact that at high F/R ratios, oxidizing conditions are 416 maintained in the uranium source, thereby sustaining the efficiency of uranium leaching. In 417 Reservoir 3 (Fig. 11b), there is an increase in uraninite precipitation for F/R ratios lower than 418 0.9, followed by a decrease in precipitation rate. This behavior contrasts with Reservoir 1 (point 419 9, Fig. 11b), where uraninite precipitation increases for F/R ratios higher than 3.

420

421 5.3 Influence of the initial redox state

422 To assess the impact of the reservoir redox state on pH, pe, variation of uraninite amount in the 423 rock and U concentration in solution along the fluid path, magnetite was introduced into 424 Reservoir 1 (Fig. 12; refer to section 4.4 for more details). These tests were conducted in the 425 conditions of the base model (F/R = 0.01).

First, addition of magnetite had minimal influence on the pH trend (Fig. 12a). On the other 426 427 hand, significant fluctuations in pe values are observed, consistently remaining negative and 428 reaching a pe value of -3 (maximum value for reaction point 7), indicative of the strong redox 429 buffering capacity of magnetite (Fig. 12b). These variations significantly influenced U 430 mobilization and subsequent precipitation, as evidenced by the patterns in U concentrations 431 and uraninite behavior along the fluid pathway (Fig. 12c and 12d). At points 5 and 6, uraninite 432 dissolution was low but slightly increased at point 7 (Fig. 12b and 12c). Similar patterns are 433 observed in U concentration in solution (Fig. 12c). No significant changes in pH, pe, U 434 concentration and uraninite quantities occurred when increasing the magnetite content from 435 0.5 to 1.6 wt.% in Reservoir 1.

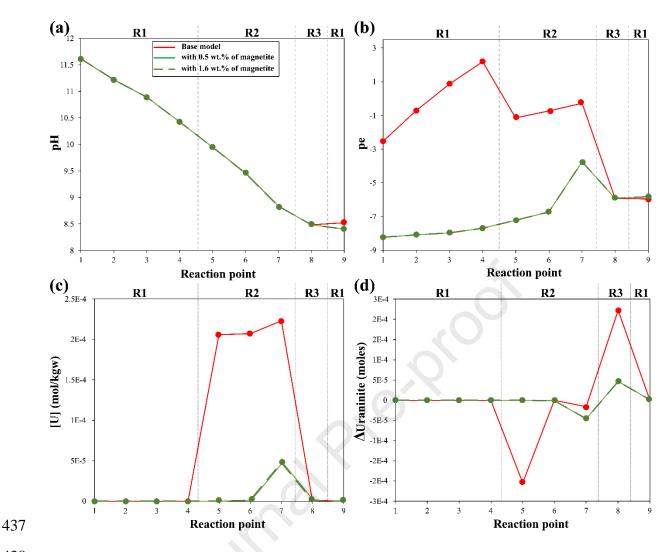


Figure 12: Effects of adding magnetite in Reservoir 1 on pH (a), pe (b), U concentration in solution (c) and
uraninite moles variations in the rock (d) along the fluid journey.

440

The reducing conditions due to the presence of magnetite also exert a significant influence on the speciation of U in the solution and the distribution of its oxidation states (Fig. 13). In contrast to experiments conducted without magnetite in Reservoir 1 (Fig. 9), U in solution is predominantly in the U(IV) state. U(VI) species represent only about 3% of the U species at point 7. U(IV) is primarily present as U(OH)₄, while the very low amount of U(VI) in the solution is mostly associated with carbonate species (Fig. 13).

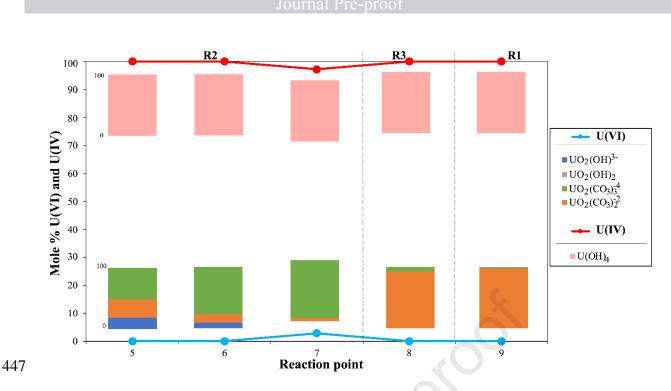


Figure 13: Evolution of U(VI) and U(IV) concentrations as percentages in the fluid for the model with 0.5 wt.%
magnetite in Reservoir 1. The uranium species are indicated for both valences.

- 450
- 451

452 6. Discussion

453 **6.1 Oxidation state of U**

Direct comparisons using precise pe or Eh values between our results and other research findings are challenging due to the unique numerical approach we employed and the limited number of studies addressing this issue. However, comparisons can be made considering general trends in the oxidation state of U.

In our base model (F/R ratio of 0.01), pe values of -1.14, -0.73, and -0.27 were calculated at 200°C, 250°C, and 300°C, respectively, in Reservoir 2 (Fig. 6), indicating moderately reducing conditions that promote the dissolution of primary magmatic uraninite (Fig. 8). Despite a trend towards less reducing conditions with increasing temperature, the fraction of U(VI) in the aqueous phase decreases from 200°C to 300°C (points 5 to 7, Fig. 9). This appears

463 counterintuitive since uraninite is more stable under reducing conditions (Langmuir, 1978),
464 and U(VI) typically dominates in oxidizing environments (Langmuir, 1978; Janeczek and
465 Ewing, 1992; Artinger et al., 2002).

However, this conventional understanding has been challenged by several studies. For 466 example, Timofeev et al. (2018) demonstrated that uranium can remain mobile under reducing 467 conditions in chloride-rich brines via the formation of UCl₄° complexes, particularly at Cl 468 469 concentrations of 0.1–1 mol/kg, pH 1.5–2.6 (at 25°C), and temperatures of 250–350°C. These 470 conditions favor uranium transport through chloride complexation. In contrast, our model fluid contains much lower Cl concentrations $(1.13 \times 10^{-5} \text{ mol/kg})$, higher pH (8.5–11.6), and lower 471 472 temperature ranges (25–300°C), which do not support U-Cl complexation. As Timofeev et al. 473 (2018) highlighted, "the ideal fluid for moving uranium is hot, chloride-rich, and highly acidic", whereas our conditions, being closer to the opposite end of the spectrum, explain why 474 475 uranium mobility in our study is not driven by chloride complexation. Another complexation 476 that could play a crucial role in uranium mobility is calcium-uranyl-carbonate (Ca-U(VI)-CO₃) 477 complexes. Previous studies have demonstrated that ternary complexes such as CaUO₂(CO₃)_{3²⁻} 478 and Ca₂UO₂(CO₃)₃(aq) dominate uranium(VI) speciation in calcium-rich environments, enhancing uranium solubility and mobility under neutral to alkaline pH conditions and 479 480 temperatures that varies from 20°C to 80°C (Fox et al., 2005; Maia et al., 2021).

Although CaUO₂(CO₃)₃²⁻ typically exhibits a peak in uranium(VI) speciation around pH 8 at 25°C (Fig. 5c), no significant concentrations of Ca-U complexes were detected in our solutions (Fig. 9). This absence can be attributed to the lack of abundant calcium in our granitic system (Fig. 4), coupled with the high temperatures (200–300°C) encountered in our experiments. Such elevated temperatures inhibit the formation of CaUO₂(CO₃)₃²⁻, as previously reported by Maia et al. (2021).

487 Additionally, Janeczek and Ewing (1992) observed that uraninite dissolution can occur under 488 hydrothermal reducing conditions at sites such as Oklo (Gabon) and Cigar Lake (Canada), even 489 at moderate temperatures (~200°C) in the presence of saline, moderately acidic solutions. Their 490 study also showed that uraninite can crystallize incorporating both U(IV) and U(VI) states, 491 challenging the assumption that post-formational oxidation is always necessary. On the other 492 hand, uraninite precipitation can occur without the typical reduction step from U(VI) to U(IV), 493 particularly in environments rich in silica (Pan et al., 2021). This non-reductive precipitation involves the formation of uranyl silicate complexes, where U binds directly as uranyl (UO_2^{2+}) 494 495 in the presence of silica. Therefore, these studies provide some clues to explain the moderate 496 reducing state we observed during U leaching from the pluton apical zone (Reservoir 2). Such 497 moderate reducing conditions encountered with a F/R ratio of 0.01, disappear with a higher 498 F/R ratio (≥ 1) which imposed oxidizing conditions (Fig. 10b). Following the fluid pathway, by 499 the time the fluid reaches Reservoir 3 (point 8), reducing conditions controlled by pyrite are calculated, inducing a classical behavior of U aligning with the oxidation state: uraninite 500 501 precipitates and U(VI) concentration decreases in solution (almost reaching zero), with the 502 remaining aqueous U being predominantly in the U(IV) state (Fig. 6 and Fig. 9).

The introduction of magnetite in Reservoir 1 significantly decreases the oxidative potential, shifting from mildly reducing conditions in the base model to moderately to strongly reducing conditions all along the fluid pathway (Fig. 12b). This alteration strongly influences U speciation, promoting a predominance of U(IV) in the aqueous phase within Reservoir 2 (Fig. 13).

508 The contrast in oxidation states between the base model (without magnetite in Reservoir 1) and 509 the experiments with magnetite in Reservoir 1 (Fig. 12) can be discussed in relation to THCC 510 (Thermo-Hydro-Chemical Coupling) results from Carnahan (1986). This author used two

29

511 different fluid sources to study how the redox state of the environment affects the behavior of 512 U in the solution. For an oxidized fluid, with a pH of 6 and an Eh of 0.0V at 90°C, Carnahan 513 (1986) showed that U species include both U(VI) and U(IV) complexes. The predominant species are U(VI) carbonate complexes such as UO₂CO₃ and UO₂(CO₃)2²⁻, with low 514 515 concentrations of U(IV) hydroxide. In contrast, in his scenario using a reduced fluid, with a pH 516 of 10 and an Eh of -0.4 V at 90°C, he showed that the dominant U species of U(IV) is U(OH)4. 517 This indicates that under reducing conditions and high pH, U(IV) species like uraninite tend to 518 dissolve but the soluble U remains predominantly in the U(IV) state. Even though pH and 519 temperature conditions are different, our results accord with the ones of Carnahan (1986). 520 Indeed, in the base model, which features mildly reducing conditions (not far from Eh of 0.0 521 V used by Carnahan (1986)), both U(VI) and U(IV) coexist, with higher proportion of U(VI) 522 in Reservoir 2 and a predominance of carbonate species (Fig. 9). Conversely, in the model with 523 magnetite in Reservoir 1, U(IV) is the predominant species, represented by U(OH)₄ (Fig. 13), 524 similarly to the Carnahan (1986) reduced source model.

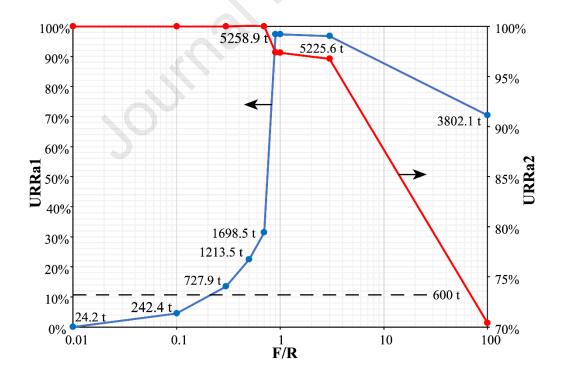
525 Uranium leaching from Reservoir 2 is more efficient in the base model than in the test with 526 magnetite in Reservoir 1 (Fig. 12d). Conditions in the base model favor the formation of U 527 complexes in solution, enhancing U mobility (Fig. 12c). Conversely, magnetite in Reservoir 1 528 leads to the formation of less soluble U species, limiting U leaching from Reservoir 2 (Fig. 12c 529 and 12d). This observation is also consistent with Carnahan (1986), who highlighted high U 530 mobility for oxidizing fluids.

531 6.2 Fluid/Rock ratio and uranium recovery rate: insight into natural systems

532 To visualize the efficiency of the fluid/rock interaction system modeled here, we defined the 533 Uranium Recovery Rate (URRa), with two types. URRa1 compares the mass of uranium

precipitated with the total mass of uranium in the source, whereas URRa2 compares the uranium precipitated with the uranium leached from the source. Thus, URRa1 provides information on the efficiency of the whole system, whereas URRa2 informs on the efficiency of the entrapment only.

In Figure 14 we observe that the URRa1 and URRa2 are dependent on the F/R ratio. For F/R 538 539 ratios lower than 0.9, the horizontal red line shows that nearly all the dissolved uraninite from 540 Reservoir 2 is precipitated in Reservoir 3 (URRa2 = 100%). For F/R ratio higher than 0.9, the 541 efficiency of uraninite precipitation decreases (slope of the red curve in Fig. 14). The abrupt 542 increase of URRa1 around the F/R ratio of 0.9 (blue curve in Fig. 14) is controlled by the 543 efficiency of uraninite dissolution in the source rather than the uraninite precipitation rate in the trap. At a F/R of 0.9, URRa1 is maximal around 97.5%. The remaining uranium is 544 545 transported away in the solution and may precipitate further, e.g., at reaction point 9 (Fig. 11b).



546

547 Figure 14: Uranium Recovery Rates (URRa1, left y-axis, blue curve and URRa2, right y-axis, red curve) as a 548 function of F/R ratio: (i) URRa1 represents the mass of uranium precipitated at point 8 divided by the sum of the 549 initial uranium mass at points 5, 6 and 7; (ii) URRa2 represents the mass of uranium precipitated at point 8 divided

by the sum of the dissolved uranium mass from points 5, 6 and 7. The mass in tons plotted along the blue curve corresponds to the calculated mass of uranium precipitated at point 8 (deposit) considering an initial content of 5400 tons of uranium (contained in primary magmatic uraninite) in the source (see text for details).

553 Our calculations regarding uranium recovery can be compared with the estimates of Ballouard et al. (2017) on the Guérande U metallogenic model. According to these authors, the total mass 554 555 of uranium leachable from the uraninite-bearing apical zone of the pluton is 5400 tons. Around 556 600 tons of U were actually mined at the Pen Ar Ran mine (Fig. 1d). The U mined represents 557 about 11% of the available U. This value of 11% corresponds to a theoretical F/R ratio of 0.2 558 (obtained by simple reading on the blue curve in Figure 14). Obviously, such value of 11% is 559 lower than the actual URRa1 value of the Guérande system given that the total amount of uranium deposited is higher than the uranium mined. To estimate the URRa1 of the Guérande 560 561 system, one has first to estimate the F/R ratio, for example using isotopic data. Dusséaux et al. 562 (2019) and Ballouard et al. (2015) provide such stable isotope data, respectively in the 563 hydrogen and the oxygen systems. Both systems show isotopic alteration in the granite-564 deformed cupola, indicative of rather high F/R ratios, likely above 0.5, despite no precise quantification. The fact that the oxygen isotope values are not buffered to constant values 565 566 indicates that the F/R ratio in the granite cupola is lower than 3 (e.g., Boulvais et al., 1998). A 567 reasonable range of F/R ratios for the Guérande system is then between 0.5 and 3. Reporting 568 these values in Figure 14 indicates a range of URRa1 values between 22% and 97% (reading 569 on the blue curve). In the end, one can estimate that between 1213 tons and 5225 tons of 570 uranium may have precipitated in the Guérande system. This crude calculation based on the comparison between our URRa1 and data from the Guérande systems shows that the uranium 571 572 actually mined at Guérande represents a small fraction of the uranium that was likely deposited. 573 At first sight, it could be good news for uranium prospection. However, our reasoning provides 574 no information on the morphology of the potential deposit, highly concentrated in a small zone

- 575 (high concentration, low volume) or diluted in a large zone (low concentration, high volume).
- 576 It has thus to be complemented by geological constraints.

577 6.3 Application of the TH-C approach to other U mineralized systems

578 Our modeling provides insights into U mobilization and precipitation mechanisms within a 579 detachment-related mineralization system associated with the emplacement of granitic melts. 580 However, it is crucial to acknowledge the limitations of these models in accurately representing 581 the complexity and scale of natural geological settings. First, the temperature range of the 582 LLNL chemical database used in our model is limited to below 300°C, whereas some mineralization has been documented to occur up to 350°C for the South Armorican case 583 584 (Ballouard et al., 2017). Furthermore, the LLNL database does not allow independent adjustment of pressure. Instead, it assumes a constant pressure of 1 bar for temperatures up to 585 586 100°C and saturation pressure for temperatures up to 300°C. This simplification may not fully 587 capture the complex pressure dynamics in natural systems, although the difference between 588 this assumed pressure and the actual fluid pressures indicated in the hydrodynamic model 589 appears to be minimal (Fig. 2b).

Notwithstanding these constraints, the TH-C approach presented here offers time efficiency and a more refined chemical analysis compared to the methods that fully coupled transport equations with chemical reactions (Steefel et al., 2005). Additionally, our study extends the existing knowledge base by conducting numerical modeling on U mobility across a wide temperature range from 25°C to 300°C. This aspect of our research addresses a gap in the literature, which has predominantly focused on U geochemistry at low temperatures.

596 Our TH-C modeling has the potential to investigate a wide spectrum of U deposits, particularly 597 those where the trapping temperatures of the mineralized fluids are below 300°C. This includes 598 the high-grade unconformity-related U deposits, which are situated at, above, or below a major

599 unconformity. In the Athabasca system (Canada), this boundary separates the Archean to 600 Paleoproterozoic basement and Proterozoic sedimentary sequences (Ruzicka, 1995; Jefferson 601 et al., 2007; Dahlkamp, 2010). Studies have consistently indicated that the formation 602 temperatures of these unconformity-related U deposits remain under 300°C. For example, 603 Cuney (2010) and Polito et al. (2011) point to formation temperatures around 200°C in the Alligator Rivers Uranium Field. Likewise, Jaireth et al. (2016) reported temperature ranges of 604 605 180°C to 250°C during the peak diagenesis of sandstone units. Cloutier et al. (2009) and 606 Kojima et al. (1994) identified similar temperatures up to 250°C, associated with fluid 607 interactions during muscovite alteration and within Canadian deposits, respectively. Richard et 608 al. (2013) detailed trapping temperatures for U mineralizing brines in the Athabasca Basin 609 between 100°C and 150°C for NaCl-rich brines and 80°C to 140°C for CaCl₂-rich brines. 610 Collectively, these findings support a formation temperature in the range of 80-250°C for 611 unconformity-related high-grade uranium mineralization, well within the applicable scope of our TH-C approach. 612

613 Another type of U mineralization is vein-type deposits. As described by Ruzicka (1993), vein-614 type deposits are identified as epigenetic concentrations of U, predominantly as pitchblende and coffinite, situated within fractures, shear zones and stockworks. These deposits are 615 616 typically hosted by granitic or sygnitic rocks and can also be found in sheared or mylonitized 617 rocks, metamorphosed sedimentary complexes. The formation of these deposits is generally 618 associated with the late phases of orogenic cycles, where changes in fluid pH, pe, pressure and 619 temperature play pivotal roles (Ruzicka, 1993). For example, in the Jáchymov deposits, 620 deposition of pitchblende occurred at temperatures between 370°C and 470°C. In contrast, the 621 Beaverlodge U district in northern Saskatchewan formed at temperatures between 100°C and 622 250°C (Liang et al., 2017). These temperature ranges highlight the diversity in conditions under

623 which vein-type uranium mineralization can occur, reflecting variations in geological settings

and fluid/rock interactions, and challenging the application of our TH-C numerical modeling.

625 7. Conclusions

The thermo-hydro-chemical (TH-C) numerical modeling approach employed in this study 626 627 appears effective in simulating uranium mobilization associated with syn-kinematic granite 628 emplacement in detachment zones. A key finding is that uranium mobility is not solely driven 629 by the oxidizing characteristics of percolating surface-derived fluids. Our TH-C modeling reveals significant changes in the redox potential of these fluids as they traverse the crust. By 630 the time these surface-derived fluids reach uranium-rich source rocks, their pe adjusts towards 631 632 more neutral or slightly reducing conditions. Remarkably, even after this evolution, the fluids retain the capacity to dissolve uranium, subsequently precipitating it in more reducing 633 634 environments. Furthermore, our calculations indicate persistent uranium dissolution in the 635 presence of magnetite, which enhances fluid reducing properties, resulting in distinct species, notably U(IV) in the aqueous phase. 636

Our results highlight the complexity of uranium mobilization, indicating that factors beyond simple oxidation-reduction dynamics play major roles. Temperature, pH, and fluid/rock (F/R) ratios emerge as critical determinants of this process. Particularly, the fluid/rock (F/R) ratio significantly influences uranium leaching, with high ratios enhancing uranium extraction from source rocks. Interestingly, an optimal F/R ratio of approximately 1 maximizes both leaching efficiency from the source and precipitation efficiency in the traps. Below this F/R ratio, dissolution efficiency decreases, whereas above it, precipitation efficiency decreases.

644 Our TH-C approach is compatible with geologically-based conceptual models and allows for the quantification of uranium mobilities, such as those seen in granite-related uranium deposits 645 (e.g., the Guérande U-bearing system in the Armorican Massif, West European Variscan 646 647 chain). Furthermore, this approach appears to be robust for up to 300°C uranium-mineralizing systems. While these findings are promising, extend this methodology to higher temperatures, 648 649 depends on the availability and accuracy of thermodynamic data. Therefore, expanding 650 thermodynamic databases through targeted laboratory experiments is crucial to improve the 651 robustness of the modeling approach. reignoc

652 **CRediT authorship contribution statement**

Khaled Bock: Writing – review and editing, Writing – original draft, Visualization,
Methodology, Investigation, Data curation, Conceptualization. Yannick Branquet: Writing –
review and editing, Supervision, Investigation, Validation, Funding acquisition,
Conceptualization. Olivier Pourret: Writing – review and editing, Formal analysis,
Conceptualization. Philippe Boulvais: Writing – review and editing, Supervision,
Investigation, Validation, Funding acquisition, Conceptualization.

659

660 Declaration of competing interest

661 The authors declare that they have no known competing financial interests or personal662 relationships that could have appeared to influence the work reported in this paper.

663 Data availability

664 Datasets related to this article are available on request from the corresponding author.

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Highlights :

- Developed a thermo-hydro-chemical (TH-C) model to investigate uranium mobility in granite-related mineralization within detachment zones.
- Found that uranium can dissolve under reducing conditions with U(IV) as the predominant aqueous species.
- Identified temperature, pH, pe, and an optimal fluid/rock ratio around 1 as critical factors for efficient uranium leaching and precipitation.
- Applied the TH-C model to the Variscan South Armorican Domain, enhancing understanding of uranium mineralization and suggesting applicability to other deposits formed below 300°C.

Declaration of interests

□ The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

☑ The authors declare the following financial interests/personal relationships which may be considered as potential competing interests:

Khaled BOCK reports financial support was provided by CNRS. If there are other authors, they declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.